Drainage Report for I-25: Mobility Hub (Sky Ridge @ Lone Tree) Project

Final

August 30, 2024

4582 South Ulster Street, Suite 1100 Denver, CO 80237 (303) 409-9700

Project No.: 24278 RS&H No.: 1248876019

Prepared by RS&H, Inc. at the direction of CDOT Region 1



TABLE OF CONTENTS

1.	Inti	roduction	.1
A	۸.	Location of Improvements	.1
E	3.	Description of Improvements	.2
C	-	Discussion of Drainage Investigation	.3
2.	Hy	drology	.4
A	۸.	Existing Basins	.4
E	8.	Proposed basins	.4
C	-	Precipitation Data	.5
3.	Exi	sting Structure	.6
A	۸.	Drainageways and Floodplains	.6
E	3.	Irrigation Crossings	.6
C	-	Water Quality	.6
4.	De	sign Discussion	.7
A	٨.	Hydraulic Structures	.7
	i)	Inlet/Catch Basin Design	.7
	ii)	Storm Drain Design	.8
	iii)	Roadside Ditch and Channel Design	.9
	iv)	Erosion Control Design	.9
а)	Irrigation Crossings	.9
k))	Drainageways and Floodplains	.9
C)	Water Quality 1	0
	i)	Allowable Release Rates1	0
	ii)	Water Quality Facilities 1	0
5.	Co	nclusion1	2
Ref	eren	ces1	3

LIST OF TABLES

Table 1: Intensity-Duration-Frequency	5
Table 2: Roadway Design Storm and Flow Spread Criteria	7
Table 3: Maintenance Access Spacing	8

LIST OF FIGURES

igure 1: Project location2

APPENDIX

Appendix A – Hydrologic Computations
Appendix A.1 – Soil Survey
Appendix A.2 – Proposed Hydrology
Appendix A.3 – Proposed Basin Map
Appendix A.4 – Existing Basin Maps

Appendix B – Hydraulic Computations

Appendix B.1 – Inlet/Spread Calculations
Appendix B.2 – Storm Sewer Capacity, HGL, and EGL

Appendix B.3 – Channel Calculations

Appendix B.4 – Erosion Control

Appendix C – Water Quality Enhancements BMPs Appendix C.1 – Design and Sizing Appendix C.2 – Permanent Water Quality Form

Appendix D – Pipe Selection Memo

1. INTRODUCTION

The purpose of this I-25 – Mobility Hub (Sky Ridge @ Lone Tree) Project is to provide Northbound (NB) and Southbound (SB) mobility hubs between Lincoln Avenue and Sky Ridge Avenue allowing the Bustang transit service minimal delay for departure and re-entry along the I-25 corridor while improving safety, mobility and operations. The I-25 – Mobility Hub (Sky Ridge @ Lone Tree) Project is hereafter referred to as "project" in this report. The purpose will be achieved by constructing two bus stops and a pedestrian bridge connection across I-25 for access between mobility hubs. The project will include widening of the Lincoln Ave NB Off-Ramp and Lincoln Ave SB On-Ramp with bus stop pull outs on either side as well as sidewalk and trail connections on the west side of the project to connect to the adjacent RTD light rail station at Sky Ridge and north to Lincoln Ave. The project is limited to improvements along I-25 between Lincoln Avenue and Sky Ridge Avenue that includes roadway improvements, traffic signing and striping, roadway lighting, bus platform and sidewalk installation, environmental restoration of areas disturbed by construction, and associated drainage and permanent water quality improvements.

A. LOCATION OF IMPROVEMENTS

The project is located along I-25 between Sky Ridge Ave and Lincoln Ave in the City of Lone Tree within Douglas County, Colorado. The site is in Section 15, Township 6 South, Range 67 West of the 6th Principal Meridian. The project location is shown on a Google Earth image in **Figure 1**. The project is entirely within the Cottonwood Creek watershed, which is a tributary to the Cherry Creek Reservoir.

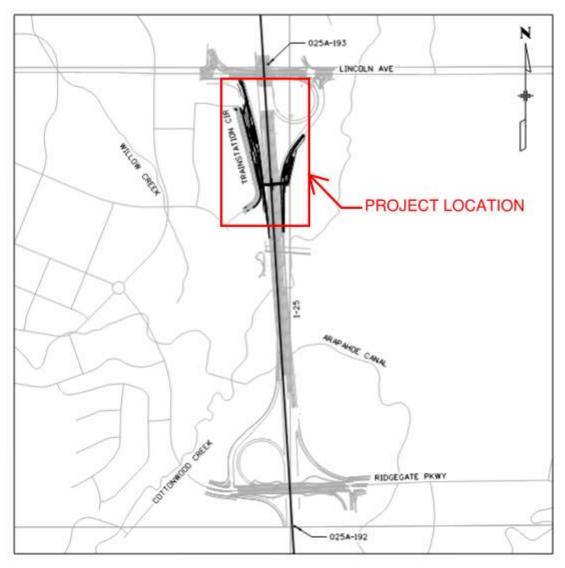


FIGURE 1: PROJECT LOCATION

B. DESCRIPTION OF IMPROVEMENTS

This project will construct transit stops with bus pullouts on the southbound and northbound ramps to Lincoln Ave along I-25 for use by Bustang as well as a pedestrian bridge connection between bus stops. The project is also constructing sidewalks trail connections to Sky Ridge Light Rail station and Lincoln Ave on the west side. The east side of the project is currently undeveloped and is planned to be a future city center. This pedestrian ramp and transit stop are designed to maximize flexibility for tie in by upcoming projects. There is also another adjacent project currently in preliminary design phase called Advancing Lincoln Avenue that will reconfigure Lincoln Ave from Park Meadows Drive to Oswego St. The project limits for this Mobility Hub do not overlap with the recommended alternative from Advancing Lincoln Ave, however this project has coordinated design to ensure that the two projects work together to create a safe environment for both pedestrians and vehicles through this interchange. The drainage design will incorporate a new network of open channels/roadside ditches, storm sewer pipes, manholes, and inlets to capture and convey storm runoff generated by the proposed roadway, sidewalk, and pullout bus stop improvements. The project has one outfall location to an existing water quality pond located in the Lincoln Ave NB On-Loop Ramp that outfalls into Cottonwood Creek. All added impervious areas are being captured by and routed through this existing water quality facility for treatment prior to being released to Cottonwood Creek.

C. DISCUSSION OF DRAINAGE INVESTIGATION

The drainage conditions investigation uses aerial images, land survey, review of as-built drawings, review of drainage reports, and site field investigations. As-built information for the Ridgegate Parkway/I-25 interchange project in 2007 and an I-25 widening project in 2011 (revised 2014) form the basis of analysis for the existing drainage patterns and facilities. The area adjacent to the project limits on the west side has undergone significant development in the last ten years that have altered drainage patterns within the area. The drainage report from the construction of Kiewit Ridgegate Campus facilitated the analysis of the drainage along the west side of the project including the existing conditions of Trainstation Circle.

A field investigation was conducted focusing on areas along the west side of the southbound lane of I-25 between Sky Ridge Avenue and Lincoln Avenue to supplement as-built information related to existing drainage patterns. The site visit validated the information from the Kiewit Drainage report that runoff from areas located along Trainstation Circle are captured into a storm system and flow into an existing water quality feature prior to discharging into CDOT ROW. The flows are ultimately conveyed into a double-barrel culvert section that crosses the I-25 corridor to the east side of the interstate and into an existing extended detention basin (EDB). For more information, see **Appendix A.4 Existing Basin Maps** for basin maps obtained from existing drainage reports in the project area. Hampton Inn & Suites is located to the north at a highpoint where runoff generally flows to the west and off-site for this area. The investigation of the drainage system for the Charles Schwab building and parking area showed two existing inlets that discharge to the west. No outlets were identified that would suggest runoff from this site discharges to the project area.

The I-25 Widening project report includes design calculations for the existing water quality pond located in the loop ramp, called "A" in the original report. The tributary area for this pond has been affected by subsequent development, most notably the installation of Trainstation Circle and the Kiewit Campus.

Historic flow patterns are maintained where possible. The proposed condition flows are discussed further in Section 4. Efforts were made to reuse existing facilities to the maximum extent practicable and to limit the impacts to existing pavement area.

2. HYDROLOGY

Hydrologic analyses for the project were performed using the Rational Method for drainage areas less than 90 acres. Parameters for the Rational Method include drainage area size (A) (acres), a dimensionless runoff coefficient (C), and rainfall intensity (I) (inches/hour) for a selected storm frequency, for a duration equal to the time of concentration (Tc). A detailed description and in-depth discussion of the Rational Method can be found in the Mile High Flood District (MHFD) *Urban Strom Drainage Criteria Manual (USDCM)*.

Runoff coefficient is a fractional portion of the precipitation that appears as runoff and is expressed as a constant between zero and one as a function of the impervious land cover and the hydrologic soil group. The runoff coefficients for the roadway sub-basins were calculated using the equations found in Table 6-4 of MHFD's USDCM Volume 1, Chapter 6 Runoff.

Tc is estimated using the hydraulically longest flow path within a drainage basin. It is calculated by using the accumulated travel time for sheet flow, shallow concentrated flow, and concentrated flow in ditches and pipes. The time of concentration is calculated using Equations 6-2, 6-3, 6-4, and 6-5 from MHFD's *USDCM Volume 1, Chapter 6 Runoff.* The minimum value for the initial Tc reading the design point is 5 minutes for any urban basin and 10 minutes for non-urban basins. Tc values for each basin are delineated to the upstream element, ditch or inlet, where the basin is attached.

A. EXISTING BASINS

In existing conditions runoff generally flows from south to north along I-25. Flows along NB I-25 are intercepted and conveyed as shallow concentrated flow adjacent to barrier and in curb and gutter sections along the east side of the highway and off ramp. Flows along SB I-25 sheet flows into grass-lined roadside ditches. Runoff generated along Trainstation Cir are captured in curb and gutter and flow from one high point located to the north at the east entrance to Hampton Inn & Suites near station 52+50 and from a second high point located to the south from the entrance to Charles Schwab near station 40+00 to a low point along Trainstation Circle. This runoff is intercepted by two inlets, located near station 48+50, that outlet into the project site through an orifice plate in the landscape wall which provides water quality. These flows combine with highway water in ditches that flows towards a low point near station 21+50 into a double barrel crossing under I-25 into the exisitng water quality pond in the loop ramp, called Pond L within this project and report. Existing on-site basins generally consist of impervious roadway and grass/lawn roadside ditch areas.

B. PROPOSED BASINS

The proposed drainage system improvements for the I-25 southbound lane and proposed ramps between Lincoln Avenue and Ridgegate Parkway will follow the same flow patterns as the existing condition.

However, due to increases in impervious area associated with the project improvements, peak runoff rates will increase. Proposed basin maps are located in **Appendix A.3**.

Basin L

The entire project limits are within basin L and drain into the existing water quality pond in the loop ramp, EDB L. The project site captures 8.56 acres with an impervious percentage of 56%, however the overall tributary area to the pond with the proposed improvements is 31.50 acres with an impervious percentage of 71%. General flow patterns within the basin are from south to north with flow concentrating in ditches and gutters along the ramps to be captured by inlets that route the water northeast to the pond for water quality treatment. The flow patterns within Basin L are predominantly the same in proposed conditions as existing conditions, however proposed utilizes more closed pipe systems than existing.

C. PRECIPITATION DATA

Intensity-duration-frequency (IDF) data was obtained utilizing the Douglas County Storm Drainage Design and Technical Criteria Manual. 1-hour point rainfall values for Douglas County, Zone 1 were used to generate the storm event precipitation data for the 10-year, 50-year, and 100-year storm events.

		Storm Event			
Duration	10-Year	50-Year	100-Year		
5 min	5.63	7.67	8.82		
10 min	4.49	6.11	7.03		
15 min	3.77	5.13	5.90		
30 min	2.60	3.55	4.08		
60 min	1.68	2.28	2.63		

TABLE 1: INTENSITY-DURATION-FREQUENCY

3. EXISTING STRUCTURE

Survey data was the primary source used for identifying existing hydraulic feature information. In addition to survey work, previous project as-builts, field visits, and photographs were used to provide information about the existing hydraulic features.

A. DRAINAGEWAYS AND FLOODPLAINS

There is one major drainageway within the vicinity of the project: Cottonwood Creek. Cottonwood Creek crosses under I-25 in a 7.75'x8' box culvert, CDOT minor structure number 025A192540BL, just south of the project limits. Cottonwood Creek is designated a Special Flood Hazard Area (SFHA) with regulatory floodway under the National Flood Insurance Program (NFIP). The 100-year floodplain boundary and regulatory floodway limits are located on the east side of I-25 and outside of the project limits therefore, this project will not impact the regulatory floodplain.

B. IRRIGATION CROSSINGS

There are no existing irrigation crossings within the limits of this project.

C. WATER QUALITY

There are two existing permanent water quality control measures within the project area. The first is located on the east side of Trainstation circle and provides water quality treatment for Trainstation Circle runoff before it enters CDOT ROW. The second provides treatment of runoff from I-25, Extended Detention Basin (EDB) L, located within the Lincoln Ave NB on-ramp loop infield. A water quality facility was installed on the east side of Trainstation Circle as part of the construction of the Trainstation Circle Roadway to treat the impervious area generated by the roadway. This facility provides water quality treatment for the portion of Trainstation Circle that runs adjacent to I-25, approximately 1.57 acres of pavement, prior to release to CDOT ROW where it combines with I-25 water and is routed through the extended detention basin located in the loop ramp. EDB L, which is understood to be owned and maintained by CDOT, is a full-spectrum facility, designed for the Excess Urban Runoff Volume (EURV). It is currently sized for a watershed area of 40.67 acres with an imperviousness of 30.2% which yields an EURV of 1.155 acre-feet.

The first facility, along Trainstation Circle, will be removed and decommissioned as part of this project and the runoff previously treated here will combine with CDOT generated runoff and receive treatment in Pond L, removing the in-series treatment. Pond L will be utilized to treat all of the additional impervious area added with this project.

4. DESIGN DISCUSSION

The proposed roadway drainage improvements include inlets, manholes, pipes, and roadside ditches. Inlets are placed along barriers and curb to adhere to project spread criteria. In accordance with the CDOT *Drainage Design Manual (DDM)* and drainage best practices, existing drainage patterns are maintained where possible and peak discharges will continue to be limited to pre-project discharge rates, where possible.

A. HYDRAULIC STRUCTURES

The inlet types and uses proposed for this project are:

- » CDOT Type C Inlets Area drains
- » Special Type D Inlet Area drain
- » CDOT Type 16 Valley Inlet In pedestrian walk area
- » CDOT Type R Inlets Curb and gutter sections
- » Single Vane Grate Inlet Along Type 9 barriers
- » Deck Drain Inlets On pedestrian ramp

i) Inlet/Catch Basin Design

The placement and design of inlets is dependent on the roadway horizontal and vertical geometry. CDOT *DDM*, FHWA *HEC-22*, MHFD's *USDCM*, methods and calculations within MHFD's Street Capacity and Inlet Sizing (version 5.03) spreadsheet were used to analyze gutter flow and calculate spread widths and bypass flows. For this project, allowable spreads are shown in **Table 2**, below.

Road Classification	Design Storm	Flow Spread				
I-25	10-year	Shoulder				
Ramps	10-year	Shoulder * + 3 ft				
Sag Point	50-year	Shoulder * + 3 ft				
Pedestrian Trail	10-year	1⁄2 Trail				

TABLE 2: ROADWAY DESIGN STORM AND FLOW SPREAD CRITERIA

* Where shoulder widths are less than 4 feet, a minimum shoulder width of 4 feet was used.

Clogging factors for inlets have been applied in accordance with the CDOT *DDM*. Detailed inlet hydraulic calculations for comparison of the proposed spread to allowable are included in **Appendix B.1** of this report. Allowable depths at area inlets are confirmed by adhering to ditch capacity criteria. For the northbound lanes that are adjacent to Cottonwood Creek this depth criteria is also applied in the 100-year storm event. Since there are no channels that would capture any water that leaves the roadway in this area the project designed the storm system to capture all of the roadway water in order to ensure all impervious area is treated and not released directly into Cottonwood Creek. The deck drain inlets, located

along the uncovered pedestrian ramps, utilize Neenah R-3924 grates and were designed to be bicycle safe and to not protrude into the limits of the trail to minimize impacts to users. The water collected will be piped via 6" pipe down the pier or wall to outfall onto a 5'x5' riprap pad. Small swales are provided to direct the concentrated flow from the ramp to outfall locations.

In addition to meeting design criteria for allowable spread and bypass, and according to the CDOT *DDM*, inlets are also located in the following locations:

- » Sag vertical curve or sump areas;
- Flanking inlets on each side of sump inlets (these are designed in accordance with Section 4.4.6.3 of the FHWA HEC-22 Urban Drainage Design Manual) to function if the sump inlet becomes clogged;
- » Upstream of pedestrian ramps (only placed if the flow would exceed the gutter);
- » As required to meet maintenance access spacing criteria of Section 13.3.7 of the CDOT DDM.

The pedestrian bridge is covered with a crowned roof that drains on either side into a rectangular gutter plate. The gutter matches the profile of the bridge at 0.5% from the center pier to either end where it drains into a 6" pipe down the pier to outlet to outfall onto a 5'x5' riprap pad. Calculations showing gutter capacity are provided in **Appendix B.2**. Small swales are provided to direct the concentrated flow from the bridge to outfall locations. No concentrated water from either the bridge or ramp will outfall into a pedestrian area.

In addition, manholes for the Project are also spaced in accordance with the maintenance access spacing criteria outlined in Section 13.3.7 of the CDOT *DDM* and shown in **Table 3**. Some of the existing pipes do not meet this spacing criteria, and manholes were not added to bring them up to criteria.

TABLE 3: MAINTENANCE ACCESS SPACING

Size of Pipe, inches	Maximum Distance, ft
≤ 48	300
> 48	600

ii) Storm Drain Design

The hydraulic design for storm drainpipes follow MHFD, CDOT *DDM*, and *HEC-22* guidelines. The calculations were performed with the Bentley OpenRoads Designer (ORD) computer program. Within ORD the calculations are completed using Bentley Storm and Sanitary Analysis.

In accordance with CDOT Standard Specifications for Road and Bridge Construction, Section 624, soil conditions were evaluated, and a pipe material selection memo was prepared, included in **Appendix D**. For this project two pipe materials have been identified – reinforced concrete pipe (RCP) and Class 7 which permits RCP, PP, SRPE, or PVC. Class 7 is used except in locations where there is insufficient cover which require the use of RCP.

The minor design storm event for all on-site facilities is the 10-year return frequency and the major storm event is the 100-year storm. The proposed storm drainpipes are designed to maintain a minimum velocity of 3 feet per second for the 10-year return frequency peak discharge and to not exceed a maximum velocity of 22 feet per second for the 100-year return frequency storm discharge. One pipe is unable to meet velocity criteria for the 10-year storm event, P-L-84-2, is just under 3 ft/s due to the flat slope required to connect into an existing pipe crossing under the ramp.

Hydraulic Grade Line (HGL) and Energy Grade Line (EGL) calculations are included for both the 10-year and 100-year storm events. The storm drain systems are designed with HGL kept at or below the crown of pipe for the 10-year frequency peak discharge. The storm drainage systems are also designed such that the EGL at or below the surface of pavement and inlet grates for the 100-year storm event. HGL and EGL calculations were performed using ORD and can be found in **Appendix B.2** of this report.

iii) Roadside Ditch and Channel Design

All ditches will be designed to convey the 100-year storm event without the water surface exceeding the edge of pavement. Ditches are also designed to maintain a minimum of 1 foot of freeboard from the edge of pavement adjacent to I-25 during the 10-year storm event. Channel geometry is in accordance with the AASHTO *Roadside Design Guide*.

Channel linings were designed in accordance with FHWA *HEC-15 Design of Roadside Channels with Flexible Linings*. Vegetated ditch linings were calculated by assuming a standard height of vegetation of 0.33 ft, fair condition of vegetation, and a mixed growth form of vegetation. These assumptions are based on the standard values recommended in *HEC-15*. Ditch calculations for flexible linings follow the iterative process found in *HEC-15* and were calculated in Excel Spreadsheets. Manning's n values vary between ditch segments based on variables used in *HEC-15* and are not specific to lining type. Channel calculations are provided in **Appendix B.3**.

iv) Erosion Control Design

Riprap outlet protection is provided at all storm drain outfalls. Riprap aprons were designed in accordance with FHWA *HEC-14 Hydraulic Design of Energy Dissipaters for Culverts and Channels*. Outlet protection calculations are provided in **Appendix B.4**.

A) IRRIGATION CROSSINGS

There are no proposed irrigation crossings within the limits of this project.

B) DRAINAGEWAYS AND FLOODPLAINS

The Cottonwood Creek floodway is not impacted by this project. See Floodplain Evaluation memo for more information.

C) WATER QUALITY

Permanent water quality treatment is sized to provide water quality treatment for 100% of the increased impervious area per Colorado Discharge Permit System (CDPS) Permit No. C0S000005.

Under CDOT's Municipal Separate Storm Sewer System (MS4) Permit, onsite permanent water quality (PWQ) treatment is required for this project based on the permanent water quality form, seen in **Appendix C.2**. This project increases the impervious area by 54%, discharges to the Cherry Creek Reservoir basin, is part of the South I-25 Corridor and US 85 Corridor Final Environmental Impact Statement (FEIS), and discharges to a 303(d) impaired stream therefore water quality treatment is required.

i) Allowable Release Rates

The Pond was designed for a tributary area of 40.67 acres with an impervious percentage of 30.24%. RS&H delineated the tributary area for the pond to account for all of the recent offsite development. Factoring in the offsite development on the west side of I-25, the current tributary area is 29.92 acres with 68.38% imperviousness flows into EDB L. The original pond design has a 100-year release flowrate of 40.7 cfs., however the existing release rate is 34.4 with the current tributary area. Flows released from the pond travel east to outfall into Cottonwood Creek.

The proposed project increases the tributary area to 31.50 acres with 71.2% imperviousness. The pond volume has been confirmed to be able to handle the additional impervious area from the project and adjacent development. The pond outlet structure was also determined to provide the required 40 hour drain time for the proposed conditions tributary area with no required modifications. The proposed 100-year release rate is 35.8 cfs which is lower than the original design and therefore this project does not cause any adverse effects downstream.

ii) Water Quality Facilities

This project proposes to remove the existing water quality treatment facility along Trainstation Circle and would provide treatment for Trainstation Circle impervious area in the CDOT loop EDB facility.

Pond calculations are included in **Appendix C.1** and contain the design and the calculations for the permanent water quality pond for the project. Detention and sizing was calculated using MHFD's spreadsheet UD-Detention version 4.06. The major features of the pond are forebay, outlet structure with micropool and trash rack, and emergency overflow inlet none of which are being impacted by this project which does not propose any construction with the pond limits.

Advancing Lincoln Ave project is proposing to modify the tributary area to EDB L, therefore it is anticipated that the project will have to modify the facility in order to accommodate the change. With this upcoming future project in the works this project has determined not to do any physical improvements or upgrades to the exisitng facility since the calculations show that it will function properly for water quality using the exiting outlet structure configuration. Some of the noted features that do not meet current design standards include lack of a concrete trickle channel, no seal around the orifice plate,

northeast inlet does not have sufficient residence time prior to discharge, and no stamped as built plan or O&M manual. These will need to be addressed when the pond is modified in the future.

5. CONCLUSION

The drainage design for the I-25 Mobility Hub (Sky Ridge @ Lone Tree) Project is performed in accordance with the CDOT *DDM*, MHFD *USDCM*, and FHWA *HEC-22* guidelines. The new storm sewer systems convey initial storm (10-year) and major storm (100-year) runoff from redeveloped roadway and ramp areas. All added impervious area will be treated prior to release offsite. The existing water quality pond has sufficient capacity to provide treatment and detention of roadway runoff resulting from the increase in impervious area.

REFERENCES

Colorado Department of Transportation. Drainage Design Manual; 2019.

Douglas County, June 2019, "Storm Drainage Design and Technical Criteria Manual"

FEMA, FIRM Panel 08035C0063H

- Federal Highway Administration. September 2005. *Hydraulic Engineering Circular No. 15*, Third Edition, Design of Roadside Channels with Flexible Linings.
- Federal Highway Administration. August 2013. *Hydraulic Engineering Circular No. 22*, Third Edition, Urban Drainage Design Manual.
- Felsburg Holt & Ullevig. April 2014. *Hydrology & Hydraulics Report for Interstate 25 Widening from Ridgegate Parkway to County Line Road.*

Martin/Martin, Inc. June 2019. Phase III Drainage Report for Kiewit Ridgegate Campus.

Mile High Flood District. September 2017. Urban Storm Drainage Criteria Manuals, Volume 1.

Mile High Flood District. September 2017. Urban Storm Drainage Criteria Manuals, Volume 2.

Mile High Flood District. November 2015. Urban Storm Drainage Criteria Manuals, Volume 3.

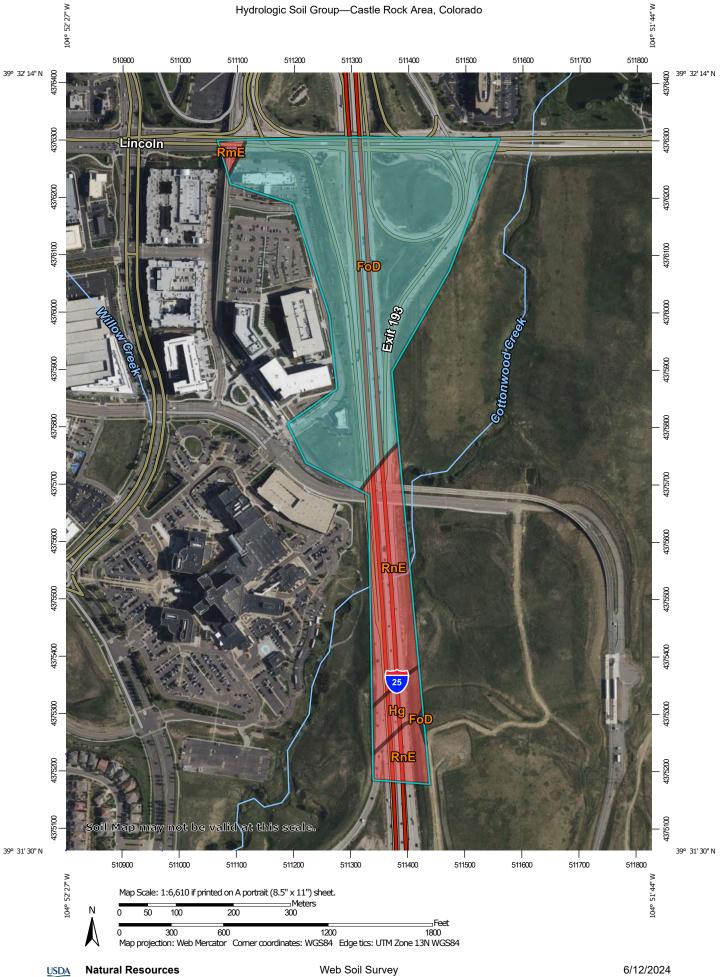
RS&H. June 2024. Floodplain Evaluation Memo.

United States Department of Agriculture, Natural Resources Conservation Service. Web Soil Survey; https://websoilsurvey.sc.egov.usda.gov/.

U.S. Department of Transportation, Federal Highway Administration & Colorado Department of Transportation. April 2001. South I-25 Corridor and US 85 Corridor Final Environmental Impact Statement Section 4(f) Evaluation.

APPENDIX A – HYDROLOGIC COMPUTATIONS

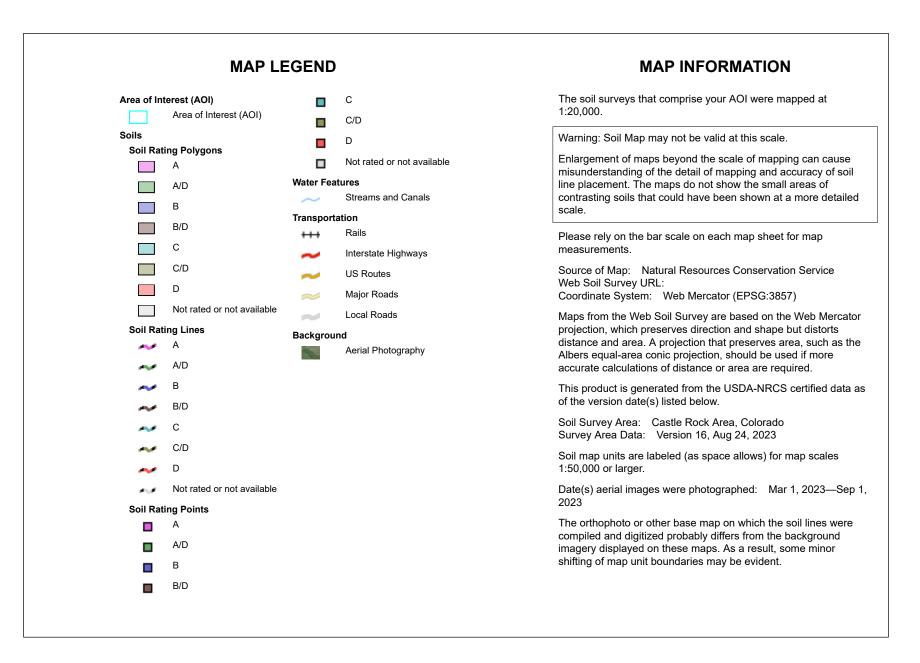
APPENDIX A.1 – SOIL SURVEY



6/12/2024 Page 1 of 4

Conservation Service

Web Soil Survey National Cooperative Soil Survey



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Rating Acres in AOI			
FoD	Fondis clay loam, 3 to 9 percent slopes	С	33.9	75.2%		
Hg	Hilly gravelly land	D	1.8	3.9%		
RmE	Renohill-Buick complex, 5 to 25 percent slopes	D	0.4	0.9%		
RnE	Renohill-Manzanola clay loams, 3 to 20 percent slopes		9.0	20.0%		
Totals for Area of Inter	rest		45.1	100.0%		

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



APPENDIX A.2 – PROPOSED HYDROLOGY

COMPOSITE C CALCULATIONS - SYSTEM SB LANES

PROJECT: I-25 Mobility Hub (Lone Tree) FOR DESIGNED BY: NAG DATE: 6/7/2024

NRCS Soil Group		Storm Return Period												
NRCS SOIL GLOUP	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year								
А	$C_A = 0.84i^{1.302}$	C _A = 0.86i ^{1.276}	$C_A = 0.87i^{1.232}$	$C_A = 0.88i^{1.124}$	C _A = 0.85i+.025	C _A = 0.78i+0.110								
В	$C_B = 0.84i^{1.169}$	C _B = 0.86i ^{1.088}	C _B = 0.81i+0.057	C _B = 0.63i+0.249	C _B = 0.56i+0.328	C _B = 0.47i+0.426								
C/D	C _{C/D} = 0.83i ^{1.122}	C _{C/D} = 0.82i+0.035	C _{C/D} = 0.74i+0.132	C _{C/D} = 0.56i+0.319	C _{C/D} = 0.49i+0.393	C _{C/D} = 0.41i+0.484								

			Land Use a	nd Impervious	Percentage			T		<u> </u>							
Basin ID	Paved	Open	Gravel (Packed)	Gravel	Roof	Ponds	Drive and Walks	Total Area	Percentage Imperviousness	NRCS Soil		F	Runoff C	oefficier	nt		
	100%	2%	40%	13%	90%	100%	90%		(%)	Group	С	С	С	С	С	С	
	area (ft ²)	(ft ²)	(acres)			02 yr	05 yr	10 yr	25 yr	50 yr	100 yr						
A-L-12	78,761	64,119	0	496	0	0	0	3.29	56%	C/D	0.43	0.49	0.55	0.63	0.67	0.71	
A-L-14	17,226	0	0	0	0	0	0	0.40	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-15	7	5,567	0	0	0	0	0	0.13	2%	C/D	0.01	0.05	0.15	0.33	0.40	0.49	
A-L-16	13,353	206	0	0	0	0	0	0.31	99%	C/D	0.82	0.84	0.86	0.87	0.88	0.89	
A-L-17-1	5,109	538	0	0	0	0	0	0.13	91%	C/D	0.74	0.78	0.80	0.83	0.84	0.86	
A-L-17-2	140	5,681	0	0	0	0	0	0.13	4%	C/D	0.02	0.07	0.16	0.34	0.41	0.50	
A-L-17-3	6,877	483	0	0	0	0	0	0.17	94%	C/D	0.77	0.80	0.82	0.84	0.85	0.87	
A-L-20	12,812	6,434	0	0	0	0	0	0.44	67%	C/D	0.53	0.59	0.63	0.70	0.72	0.76	
A-L-20-1	5,493	2,495	0	0	0	0	0	0.18	69%	C/D	0.55	0.60	0.65	0.71	0.73	0.77	
A-L-20-2	8,464	8,238	0	0	0	0	0	0.38	52%	C/D	0.40	0.46	0.51	0.61	0.65	0.70	
A-L-20-3	3,272	0	0	0	0	0	0	0.08	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-21-1	5,739	0	0	0	0	0	0	0.13	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-21-2	5,144	0	0	0	0	0	0	0.12	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
EX-A-L-21-5	36,714	8,337	0	0	0	0	0	1.03	82%	C/D	0.66	0.71	0.74	0.78	0.79	0.82	
A-L-23	8,455	0	0	0	0	0	0	0.19	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-24	1,835	17,053	0	0	0	0	0	0.43	12%	C/D	0.07	0.13	0.22	0.38	0.45	0.53	
A-L-24-1	8,767	0	0	0	0	0	0	0.20	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-25	6,357	37,459	0	0	0	0	0	1.01	16%	C/D	0.11	0.17	0.25	0.41	0.47	0.55	
A-L-42	7,407	1,917	0	0	0	0	0	0.21	80%	C/D	0.64	0.69	0.72	0.77	0.78	0.81	
A-L-45	8,696	931	0	0	0	0	0	0.22	91%	C/D	0.74	0.78	0.80	0.83	0.84	0.86	
A-L-48-1N	7,844	0	0	0	0	0	0	0.18	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
EX-A-L-48-1S	10,113	801	0	0	0	0	0	0.25	93%	C/D	0.76	0.80	0.82	0.84	0.85	0.86	
EX-A-L-48-2	10,235	2,183	0	0	0	0	0	0.29	83%	C/D	0.67	0.71	0.74	0.78	0.80	0.82	
EX-A-L-48-3	22,515	4,524	0	0	0	0	0	0.62	84%	C/D	0.68	0.72	0.75	0.79	0.80	0.83	
A-L-102	1,775	0	0	0	0	0	0	0.04	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-103	1,845	0	0	0	0	0	0	0.04	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-105	0	0	0	0	1,827	0	0	0.04	90%	C/D	0.74	0.77	0.80	0.82	0.83	0.85	
DESIGN POINT 1	1,985	5,681	0	0	1,827	0	0	0.22	39%	C/D	0.29	0.36	0.42	0.54	0.59	0.65	

DESIGN POINT 1 INCLUDES THE FOLLOWING BASINS: A-L-17-2, A-L-103, A-L-105

PROJECT #: 24278 CHECKED BY: MED

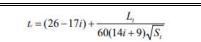
RS&H

TIME OF CONCENTRATION - SYSTEM SB LANES

PROJECT: I-25 Mobility Hub (Lone Tree) FOR DESIGNED BY: NAG DATE: 6/7/2024

 $t_c = t_i + t_i$

 $t_{t} = \frac{L_{t}}{60K\sqrt{S_{o}}} \qquad t_{i} = \frac{0.395(1.1 - C_{5})\sqrt{L_{i}}}{S_{o}^{0.33}}$





	SUB-BASIN			INITIAL	OVERLAN	ID TIME	TRAVEL TIME							t _c URBAN	FINAL
	DATA			1	(t _i)		1	01	(t _t)	1			t _i + t _t	CHECK	t_c USED
Basin ID	Basin Type	Area	С	Length (L _i)	Slope (S _i)	ti	Length (L _t)	Slope (S _t)	Type of	Conveyance	Velocity	t	t _c	t _{reg}	t _c
	Laon Spo	(acres)	05 yr	(ft)	%	(min)	(ft)	%	Land Surface	Factor, K	(ft/sec)	(min)	(min)	(min)	(min)
A-L-12	URBAN	3.29	0.49	234.58	6.21%	9.27	1117.72	1.33%	GRASSED WATERWAY	15.00	1.73	10.77	20.04	26.10	20.04
A-L-14	URBAN	0.40	0.86	95.05	2.91%	3.07	185.85	0.82%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	1.81	1.71	4.78	10.49	5.00
A-L-15	URBAN	0.13	0.05	58.37	11.94%	6.42	127.81	1.28%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.27	0.94	7.36	27.66	7.36
A-L-16	URBAN	0.31	0.84	119.95	2.76%	3.68	135.37	1.41%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.38	0.95	4.63	10.09	5.00
A-L-17-1	URBAN	0.13	0.78	148.78	5.02%	4.20	46.69	1.57%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.51	0.31	4.51	10.87	5.00
A-L-17-2	URBAN	0.13	0.07	17.00	32.59%	2.44	166.76	2.89%	GRASSED WATERWAY	15.00	2.55	1.09	3.53	26.96	5.00
A-L-17-3	URBAN	0.17	0.80	148.78	5.02%	3.89	142.79	1.94%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.79	0.85	4.74	10.87	5.00
A-L-20	URBAN	0.44	0.59	64.78	3.03%	5.24	208.37	1.81%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.69	1.29	6.53	15.97	6.53
A-L-20-1	URBAN	0.18	0.60	58.01	3.34%	4.63	29.21	0.58%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	1.53	0.32	4.95	14.54	5.00
A-L-20-2	URBAN	0.38	0.46	26.91	3.49%	4.02	94.08	0.60%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	1.54	1.02	5.04	18.47	5.04
A-L-20-3	URBAN	0.08	0.86	35.39	3.36%	1.78	70.04	0.37%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	1.22	0.96	2.74	9.83	5.00
A-L-21-1	URBAN	0.13	0.86	45.93	3.74%	1.96	110.40	1.54%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.48	0.74	2.70	9.64	5.00
A-L-21-2	URBAN	0.12	0.86	83.04	3.53%	2.69	95.99	2.05%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.87	0.56	3.25	9.49	5.00
EX-A-L-21-5	URBAN	1.03	0.71	104.37	4.16%	4.59	466.26	1.91%	GRASSED WATERWAY	15.00	2.07	3.75	8.33	14.83	8.33
A-L-23	URBAN	0.19	0.86	113.53	3.36%	3.19	117.98	2.90%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	3.41	0.58	3.77	9.50	5.00
A-L-24	NON-URBAN	0.43	0.13	44.31	4.72%	7.06	135.10	6.84%	GRASSED WATERWAY	15.00	3.92	0.57	7.64	N/A	10.00
A-L-24-1	URBAN	0.20	0.86	28.05	2.28%	1.81	332.49	2.41%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	3.10	1.79	3.59	10.55	5.00
A-L-25	NON-URBAN	1.01	0.17	98.53	4.86%	10.01	504.41	0.56%	GRASSED WATERWAY	15.00	1.12	7.50	17.51	N/A	17.51
A-L-42	URBAN	0.21	0.69	17.14	1.40%	2.78	307.56	1.70%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.61	1.97	4.75	14.37	5.00
A-L-45	URBAN	0.22	0.78	70.19	2.35%	3.73	303.04	1.91%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.76	1.83	5.56	12.30	5.56
A-L-48-1N	URBAN	0.18	0.86	17.24	0.41%	2.52	433.88	0.91%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	1.90	3.80	6.32	12.30	6.32

PROJECT #: 24278 CHECKED BY: MED

TIME OF CONCENTRATION - SYSTEM SB LANES

PROJECT: DESIGNED BY: DATE:	I-25 Mobility Hub (Lone Tree) FOR NAG 6/7/2024							OJECT #: CKED BY:	24278 MED	
		$t_c = t_i + t_t$	$t_i = 0$	$\frac{L_t}{60K\sqrt{S_o}}$	$t_i = \frac{0.395(1.1 - 1)}{S_o^0}$	$-C_5)\sqrt{L_i}$	$t_c = (26 - 17i) + \frac{L_t}{60(14i + 9)\sqrt{2}}$	$\overline{\overline{S_t}}$	RSa	SH
SU	B-BASIN	INITIAL/OVERLA			TR	AVEL TIME			t _c URBAN	FINAL

	UD-DASIN			INTIAL	OVERLAN		TRAVEL TIME								FINAL
	DATA				(t _i)				(t _t)		t _i + t _t	CHECK	t _c USED		
Basin ID	Basin Type	Area	С	Length (L _i)	Slope (S _i)	ti	Length (L _t)	Slope (S _t)	Type of Land Surface	Conveyance Factor, K	Velocity	t,	t _c	t _{reg}	t _c
		(acres)	05 yr	(ft)	%	(min)	(ft)	%	Land Surface	Tactor, R	(ft/sec)	(min)	(min)	(min)	(min)
EX-A-L-48-1S	URBAN	0.25	0.80	58.22	1.53%	3.69	256.42	1.81%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.69	1.59	5.28	11.67	5.28
EX-A-L-48-2	URBAN	0.29	0.71	23.06	1.73%	2.83	379.13	1.13%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.12	2.97	5.80	14.82	5.80
EX-A-L-48-3	URBAN	0.62	0.72	18.09	2.21%	2.27	828.20	1.95%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.79	4.94	7.22	16.56	7.22
A-L-102	URBAN	0.04	0.86	46.83	5.89%	1.70	113.45	6.98%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	5.28	0.36	2.06	9.31	5.00
A-L-103	URBAN	0.04	0.86	18.00	1.72%	1.59	135.00	7.10%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	5.33	0.42	2.01	9.37	5.00
A-L-105	URBAN	0.04	0.77	0.00	0.00%	0.00	0.00	0.00%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	0.00	0.00	0.00	10.70	5.00
DESIGN POINT 1	URBAN	0.22	0.36	17.00	32.59%	1.76	166.76	2.89%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	3.40	0.82	2.57	27.82	5.00

DESIGN POINT 1 INCLUDES THE FOLLOWING BASINS: A-L-17-2, A-L-103, A-L-105

RUNOFF CALCULATIONS - SYSTEM SB LANES

PROJECT: DESIGNED BY: DATE: I-25 Mobility Hub (Lone Tree) FOR NAG 6/7/2024 PROJECT #: 24278 CHECKED BY: MED



Basin	Area (ac.)	'c'	cA	t _c (min)	intensity (in/hr)	Q (cfs)	Storm Event	Attached To
		0.55	1.80		3.26	5.86	10 YR	
A-L-12	3.29	0.67	2.19	20.04	4.44	9.75	50 YR	IN-L-12
		0.71	2.35		5.11	11.99	100 YR	
A-L-14	0.40	0.87	0.34 0.35	5.00	5.63 7.67	1.94 2.68	10 YR 50 YR	IN-L-14
	0.40	0.89	0.35	0.00	8.82	3.12	100 YR	
		0.15	0.02		5.09	0.10	10 YR	
A-L-15	0.13	0.40	0.05	7.36	6.93	0.36	50 YR	IN-L-15
		0.49	0.06		7.98	0.50	100 YR	
		0.86	0.27		5.63	1.51	10 YR	
A-L-16	0.31	0.88	0.27	5.00	7.67	2.09	50 YR	IN-L-16
		0.89	0.28		8.82	2.44	100 YR	
	0.40	0.80	0.10		5.63	0.59	10 YR	
A-L-17-1	0.13	0.84	0.11	5.00	7.67	0.83	50 YR	IN-L-17-1
		0.86	0.11	-	8.82	0.98	100 YR	
A-L-17-2	0.13	0.16 0.41	0.02	5.00	5.63 7.67	0.12	10 YR 50 YR	
A-L-17-2	0.15	0.41	0.00	5.00	8.82	0.42	100 YR	IN-L-17-2
		0.82	0.07		5.63	0.78	10 YR	
A-L-17-3	0.17	0.85	0.14	5.00	7.67	1.10	50 YR	IN-L-17-3
	••••	0.87	0.15		8.82	1.29	100 YR	
		0.63	0.28		5.28	1.47	10 YR	
A-L-20	0.44	0.72	0.32	6.53	7.19	2.30	50 YR	IN-L-20
		0.76	0.34		8.27	2.78	100 YR	
	0.18	0.65	0.12		5.63	0.67	10 YR	
A-L-20-1		0.73	0.13	5.00	7.67	1.03	50 YR	IN-L-20-1
		0.77	0.14		8.82	1.24	100 YR	
		0.51	0.20		5.62	1.11	10 YR	
A-L-20-2	0.38	0.65	0.25	5.04	7.65	1.90	50 YR	IN-L-20-2
		0.70	0.27	-	8.81	2.35	100 YR	
A-L-20-3	0.08	0.87	0.07	5.00	5.63	0.37	10 YR	IN-L-20-3
A-L-20-3	0.00	0.88	0.07	5.00	7.67 8.82	0.51	50 YR 100 YR	IIN-L-20-3
		0.87	0.07		5.63	0.65	10 YR	
A-L-21-1	0.13	0.88	0.11	5.00	7.67	0.89	50 YR	IN-L-21-1
	0.10	0.89	0.12		8.82	1.04	100 YR	
		0.87	0.10		5.63	0.58	10 YR	
A-L-21-2	0.12	0.88	0.10	5.00	7.67	0.80	50 YR	IN-L-21-2
		0.89	0.11		8.82	0.93	100 YR	1
		0.74	0.76		4.87	3.72	10 YR	
EX-A-L-21-5	1.03	0.79	0.82	8.33	6.63	5.45	50 YR	EX-IN-L-21-
		0.82	0.85		7.63	6.47	100 YR	
		0.87	0.17		5.63	0.95	10 YR	
A-L-23	0.19	0.88	0.17	5.00	7.67	1.31	50 YR	IN-L-23
		0.89	0.17	-	8.82	1.53	100 YR	
A-L-24	0.43	0.22	0.09	10.00	4.49	0.42	10 YR	IN-L-24
A-L-24	0.43	0.45	0.19 0.23	10.00	6.11 7.03	1.19 1.62	50 YR 100 YR	IIN-L-24
		0.55	0.23		5.63	0.99	10 YR	
A-L-24-1	0.20	0.88	0.10	5.00	7.67	1.36	50 YR	IN-L-24-1
	0.20	0.89	0.18		8.82	1.59	100 YR	1
		0.25	0.25		3.52	0.89	10 YR	
A-L-25	1.01	0.47	0.48	17.51	4.79	2.27	50 YR	IN-L-25
		0.55	0.55		5.51	3.05	100 YR	
		0.72	0.15		5.63	0.87	10 YR	
A-L-42	0.21	0.78	0.17	5.00	7.67	1.29	50 YR	IN-L-42
		0.81	0.17		8.82	1.53	100 YR	1

RUNOFF CALCULATIONS - SYSTEM SB LANES

PROJECT: DESIGNED BY: DATE: I-25 Mobility Hub (Lone Tree) FOR NAG 6/7/2024



Basin	Area (ac.)	'c'	cA	t _c (min)	intensity (in/hr)	Q (cfs)	Storm Event	Attached To
		0.80	0.18		5.50	0.98	10 YR	
A-L-45	0.22	0.84	0.18	5.56	7.49	1.39	50 YR	IN-L-45
		0.86	0.19		8.62	1.63	100 YR	
		0.87	0.16		5.33	0.84	10 YR	
A-L-48-1N	0.18	0.88	0.16	6.32	7.26	1.15	50 YR	IN-L-48-1N
		0.89	0.16		8.35	1.34	100 YR	
		0.82	0.21		5.57	1.14	10 YR	
EX-A-L-48-1S	0.25	0.85	0.21	5.28	7.58	1.61	50 YR	EX-IN-L-48-1S
		0.86	0.22		8.72	1.89	100 YR	
		0.74	0.21		5.45	1.16	10 YR	
EX-A-L-48-2	0.29	0.80	0.23	5.80	7.42	1.69	50 YR	EX-IN-L-48-2
		0.82	0.23		8.53	2.00	100 YR	
	0.62	0.75	0.47	7.22	5.13	2.39	10 YR	EX-IN-L-48-3
EX-A-L-48-3		0.80	0.50		6.98	3.48	50 YR	
		0.83	0.51		8.03	4.12	100 YR	
		0.87	0.04		5.63	0.20	10 YR	
A-L-102	0.04	0.88	0.04	5.00	7.67	0.28	50 YR	IN-L-102
		0.89	0.04		8.82	0.32	100 YR	
		0.87	0.04		5.63	0.21	10 YR	
A-L-103	0.04	0.88	0.04	5.00	7.67	0.29	50 YR	IN-L-103
		0.89	0.04		8.82	0.33	100 YR	
	1	0.80	0.03		5.63	0.19	10 YR	
A-L-105	0.04	0.83	0.03	5.00	7.67	0.27	50 YR	N/A
		0.85	0.04]	8.82	0.32	100 YR	
	1	0.42	0.09		5.63	0.52	10 YR	
DESIGN POINT 1	0.22	0.59	0.13	5.00	7.67	0.98	50 YR	IN-L-17-2
		0.65	0.14		8.82	1.24	100 YR	1

DESIGN POINT 1 INCLUDES THE FOLLOWING BASINS: A-L-17-2, A-L-103, A-L-105

COMPOSITE C CALCULATIONS - SYSTEM NB LANES

PROJECT: I-25 Mobility Hub (Lone Tree) DESIGNED BY: NAG

DATE: 6/7/2024

NRCS Soil Group		Storm Return Period												
	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year								
А	$C_A = 0.84i^{1.302}$	C _A = 0.86i ^{1.276}	C _A = 0.87i ^{1.232}	$C_A = 0.88i^{1.124}$	C _A = 0.85i+.025	C _A = 0.78i+0.110								
В	$C_B = 0.84i^{1.169}$	C _B = 0.86i ^{1.088}	C _B = 0.81i+0.057	C _B = 0.63i+0.249	C _B = 0.56i+0.328	C _B = 0.47i+0.426								
C/D	C _{C/D} = 0.83i ^{1.122}	C _{C/D} = 0.82i+0.035	C _{C/D} = 0.74i+0.132	C _{C/D} = 0.56i+0.319	C _{C/D} = 0.49i+0.393	C _{C/D} = 0.41i+0.484								

CHECKED BY:	MED	

PROJECT #:



24278

			Land Use ar	nd Impervious													
Basin ID	Paved	Open	Gravel (Packed)	Gravel	Roof	Ponds	Drive and walks	Total Area	Percentage Imperviousness	NRCS Soil		R	unoff C	oefficier	nt		
	100%	2%	40%	13%	90%	100%	90%		(%)	. (%)	Group	С	С	С	С	С	С
	area (ft ²)	(acres)			02 yr	05 yr	10 yr	25 yr	50 yr	100 yr							
A-L-108	0	0	0	0	3,024	0	0	0.07	90%	C/D	0.74	0.77	0.80	0.82	0.83	0.85	
A-L-109	3,149	0	0	0	0	0	0	0.07	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-111	2,215	0	0	0	0	0	0	0.05	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-76	15,787	0	0	0	0	0	0	0.36	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-79	33,964	1,322	0	0	0	0	0	0.81	96%	C/D	0.80	0.82	0.84	0.86	0.87	0.88	
A-L-80	6,307	479	0	0	0	0	0	0.16	93%	C/D	0.77	0.80	0.82	0.84	0.85	0.87	
A-L-83-1	7,847	0	0	0	0	0	0	0.18	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-83-2	8,396	0	0	0	0	0	0	0.19	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-84-1	6,175	0	0	0	0	0	0	0.14	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-84-2	1,453	40,219	0	0	0	0	0	0.96	5%	C/D	0.03	0.08	0.17	0.35	0.42	0.51	
A-L-85	5,876	0	0	0	0	0	0	0.13	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
A-L-87	7,192	0	0	0	0	0	0	0.17	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
EX-A-L-75	7,333	0	0	0	0	0	0	0.17	100%	C/D	0.83	0.86	0.87	0.88	0.88	0.89	
DESIGN POINT 2	6,816	40,219	0	0	3,024	0	0	1.15	21%	C/D	0.14	0.20	0.28	0.43	0.49	0.57	

DESIGN POINT 2 INCLUDES THE FOLLOWING BASINS: A-L-84-2, A-L-108, A-L-109, A-L-111

TIME OF CONCENTRATION - SYSTEM NB LANES

I-25 Mobility Hub (Lone Tree) PROJECT: DESIGNED BY: NAG 6/7/2024 DATE:

 $t_c = t_i + t_t$ $t_t = \frac{L_t}{60K\sqrt{S_o}}$ $t_i = \frac{0.395(1.1 - C_s)\sqrt{L_i}}{S_o^{0.33}}$

 $t_{r} = (26 - 17i) + \frac{L_{t}}{60(14i + 9)\sqrt{S_{t}}}$

PROJECT #:

CHECKED BY: MED



24278

	INITIAL	INITIAL/OVERLAND TIME TRAVEL TIME									t _c URBAN	FINAL			
	DATA						(t _i) (t _t)						t _i + t _t	CHECK	t _c USED
Basin ID	Basin Type	Area	С	Length (L _i)	Slope (S _i)	ti	Length (L _t)	Slope (S _t)	Type of Land Surface	Conveyance Factor. K	Velocity	t _t	t _c	t _{reg}	t _c
		(acres)	05 yr	(ft)	%	(min)	(ft)	%	Land Sufface	Tactor, R	(ft/sec)	(min)	(min)	(min)	(min)
A-L-108	URBAN	0.07	0.77	155.97	1.00%	7.49	0.00	0.00%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	0.00	0.00	7.49	10.70	7.49
A-L-109	URBAN	0.07	0.86	75.47	6.60%	2.08	110.56	6.86%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	5.24	0.35	2.43	9.31	5.00
A-L-111	URBAN	0.05	0.86	76.07	6.72%	2.08	89.80	5.62%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	4.74	0.32	2.39	9.27	5.00
A-L-76	URBAN	0.36	0.86	98.83	1.75%	3.71	152.93	0.82%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	1.81	1.41	5.11	10.23	5.11
A-L-79	URBAN	0.81	0.82	111.41	2.02%	4.21	298.91	1.02%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.02	2.47	6.68	11.82	6.68
A-L-80	URBAN	0.16	0.80	138.99	1.63%	5.55	111.30	3.50%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	3.74	0.50	6.04	10.63	6.04
A-L-83-1	URBAN	0.18	0.86	38.25	7.29%	1.43	167.86	0.97%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	1.96	1.42	2.86	10.24	5.00
A-L-83-2	URBAN	0.19	0.86	59.80	5.87%	1.93	197.82	0.91%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	1.91	1.73	3.65	10.50	5.00
A-L-84-1	URBAN	0.14	0.86	64.96	6.43%	1.95	74.20	1.64%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.56	0.48	2.43	9.42	5.00
A-L-84-2	NON-URBAN	0.96	0.08	208.26	2.21%	20.72	447.98	1.91%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.76	2.70	23.42	N/A	23.42
A-L-85	URBAN	0.13	0.86	54.47	8.35%	1.63	104.50	0.33%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	1.16	1.50	3.14	10.31	5.00
A-L-87	URBAN	0.17	0.86	47.44	5.73%	1.73	181.40	1.42%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.38	1.27	3.00	10.10	5.00
EX-A-L-75	URBAN	0.17	0.86	99.09	1.84%	3.65	73.60	0.58%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	1.53	0.80	4.45	9.70	5.00
DESIGN POINT 2	NON-URBAN	1.15	0.20	208.26	2.21%	18.18	447.98	1.91%	PAVED AREAS AND SHALLOW PAVED SWALES	20.00	2.76	2.70	20.88	N/A	20.88

DESIGN POINT 2 INCLUDES THE FOLLOWING BASINS: A-L-84-2, A-L-108, A-L-109, A-L-111

RUNOFF CALCULATIONS - SYSTEM NB LANES

PROJECT: DESIGNED BY: DATE:

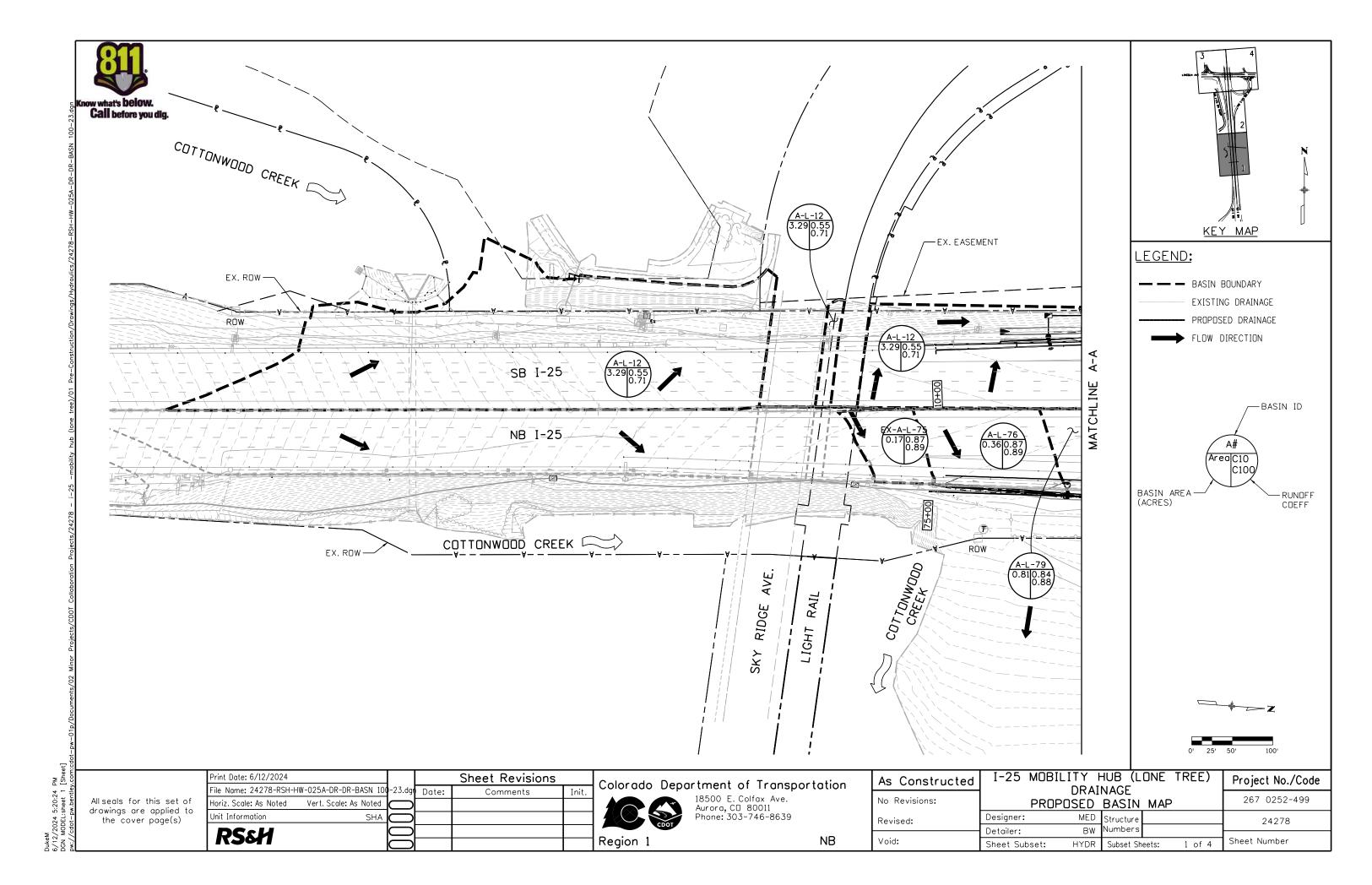
T: I-25 Mobility Hub (Lone Tree) Y: NAG E: 6/7/2024 PROJECT #: 24278 CHECKED BY: MED

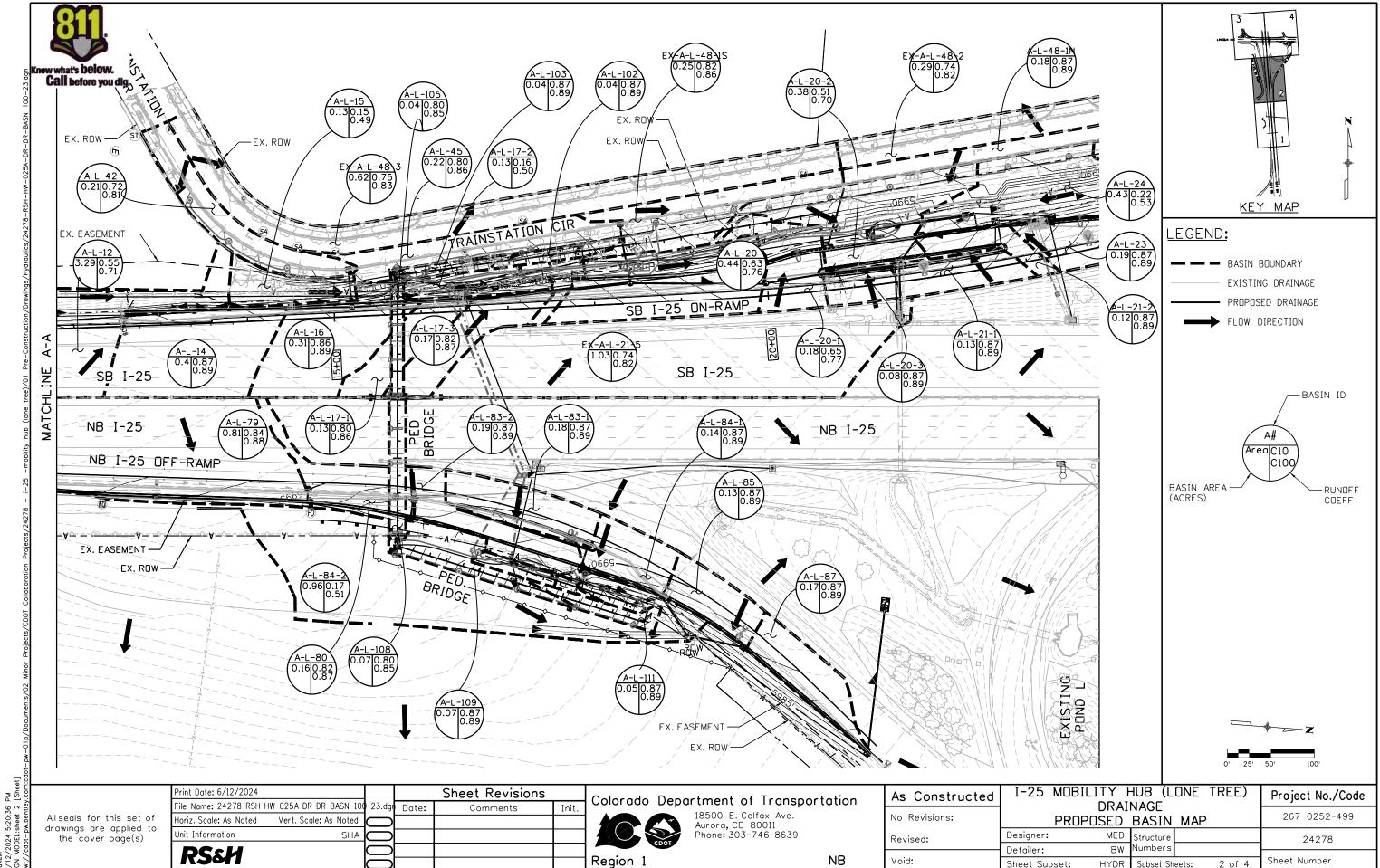
RS&H

Basin	Area (ac.)	'c'	cA	t _c (min)	intensity (in/hr)	Q (cfs)	Storm Event	Attached To
A-L-108	0.07	0.80	0.06	7.49	5.06 6.89	0.28	10 YR 50 YR	N/A
A-L-109	0.07	0.85 0.87 0.88	0.06 0.06 0.06	5.00	7.93 5.63 7.67	0.47 0.35 0.49	100 YR 10 YR 50 YR	IN-L-109
A-L-111	0.05	0.89 0.87 0.88	0.06 0.04 0.04	5.00	8.82 5.63 7.67	0.57 0.25 0.34	100 YR 10 YR 50 YR	IN-L-111
	0.26	0.89 0.87	0.05 0.32	- 	8.82 5.60	0.40	100 YR 10 YR	
A-L-76	0.36	0.88 0.89 0.84	0.32 0.32 0.68	5.11	7.63 8.78 5.25	2.44 2.84 3.59	50 YR 100 YR 10 YR	IN-L-76
A-L-79	0.81	0.87 0.88 0.82	0.70 0.71 0.13	6.68	7.14 8.22 5.39	5.01 5.85 0.69	50 YR 100 YR 10 YR	IN-L-79
A-L-80	0.16	0.85 0.87	0.13 0.13	6.04	7.34 8.45	0.89 0.97 1.14	50 YR 100 YR	IN-L-80
A-L-83-1	0.18	0.87 0.88 0.89	0.16 0.16 0.16	5.00	5.63 7.67 8.82	0.88 1.22 1.42	10 YR 50 YR 100 YR	IN-L-83-1
A-L-83-2	0.19	0.87 0.88 0.89	0.17 0.17 0.17 0.17	5.00	5.63 7.67 8.82	0.95 1.30 1.52	10 YR 50 YR 100 YR	IN-L-83-2
A-L-84-1	0.14	0.87 0.88 0.89	0.12 0.13 0.13	5.00	5.63 7.67 8.82	0.70 0.96 1.12	10 YR 50 YR 100 YR	IN-L-84-1
A-L-84-2	0.96	0.89 0.17 0.42 0.51	0.13 0.16 0.40 0.48	23.42	3.01 4.10 4.72	0.50 1.64 2.28	10 YR 50 YR 100 YR	IN-L-84-2
A-L-85	0.13	0.87 0.88 0.89	0.12 0.12 0.12 0.12	5.00	5.63 7.67 8.82	0.66 0.91 1.06	10 YR 50 YR 100 YR	IN-L-85
A-L-87	0.17	0.87 0.88 0.89	0.12 0.14 0.15 0.15	5.00	5.63 7.67 8.82	0.81 1.12 1.30	10 YR 50 YR 100 YR	IN-L-87
EX-A-L-75	0.17	0.87 0.88 0.89	0.15 0.15 0.15 0.15	5.00	5.63 7.67 8.82	0.83 1.14 1.33	10 YR 50 YR 100 YR	EX-IN-L-75
DESIGN POINT 2	1.15	0.89 0.28 0.49 0.57	0.13 0.33 0.57 0.65	20.88	3.20 4.36 5.01	1.05 2.47 3.28	10 YR 50 YR 100 YR	IN-L-84-2

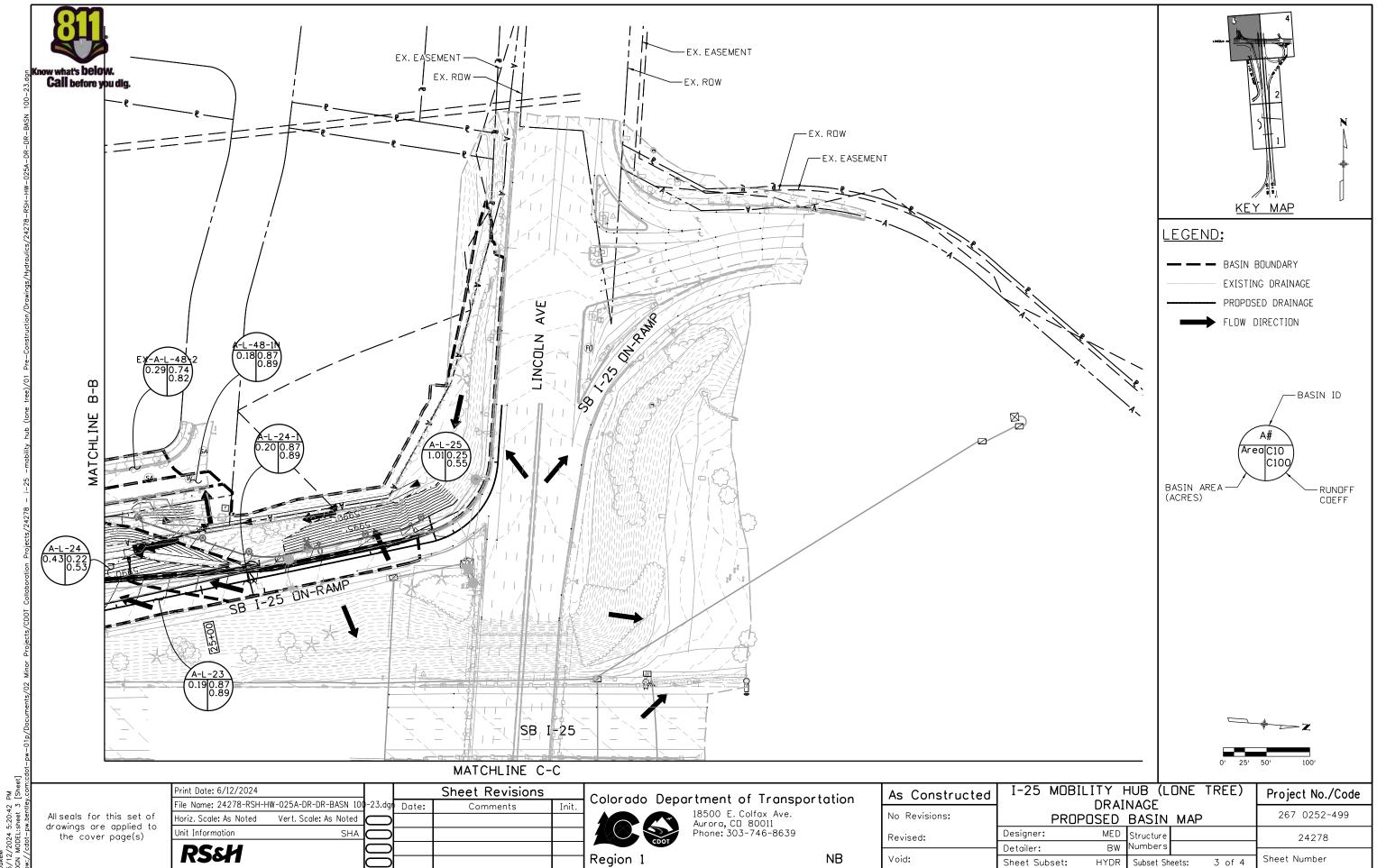
DESIGN POINT 2 INCLUDES THE FOLLOWING BASINS: A-L-84-2, A-L-108, A-L-109, A-L-111

APPENDIX A.3 – PROPOSED BASIN MAP

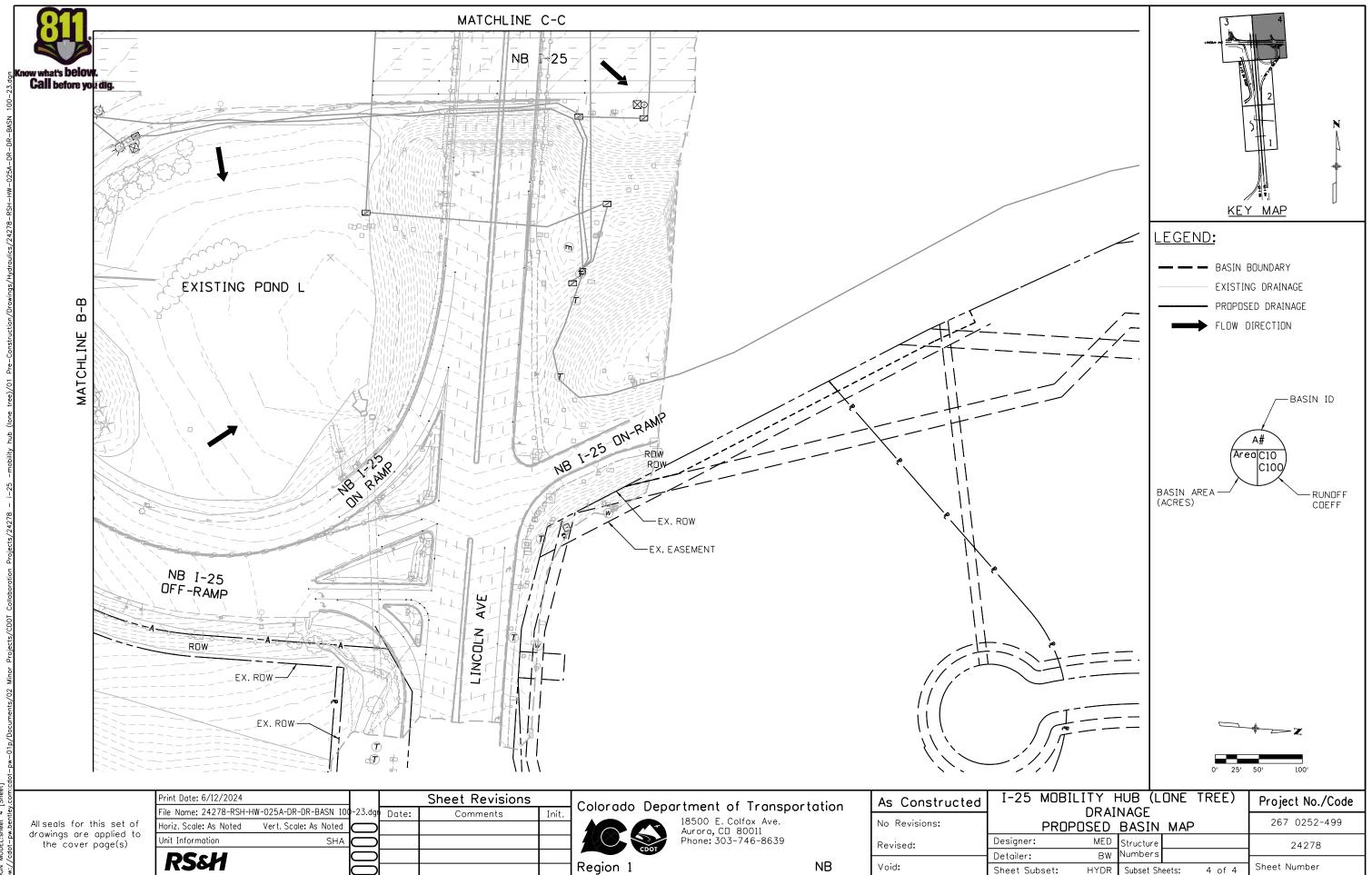




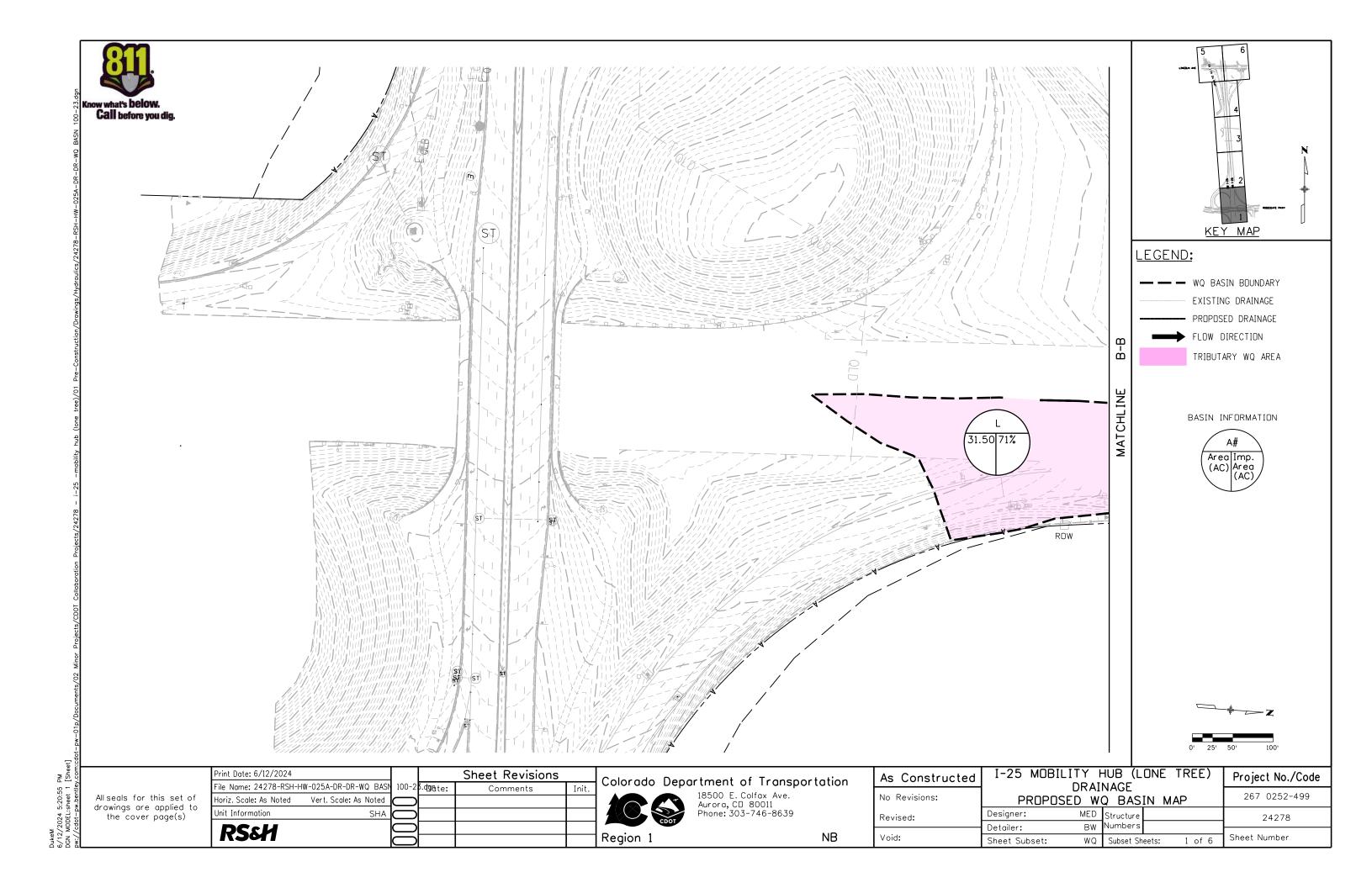
5:20:36 :sheet 2 /2024 MODEL DukeM 6/12/

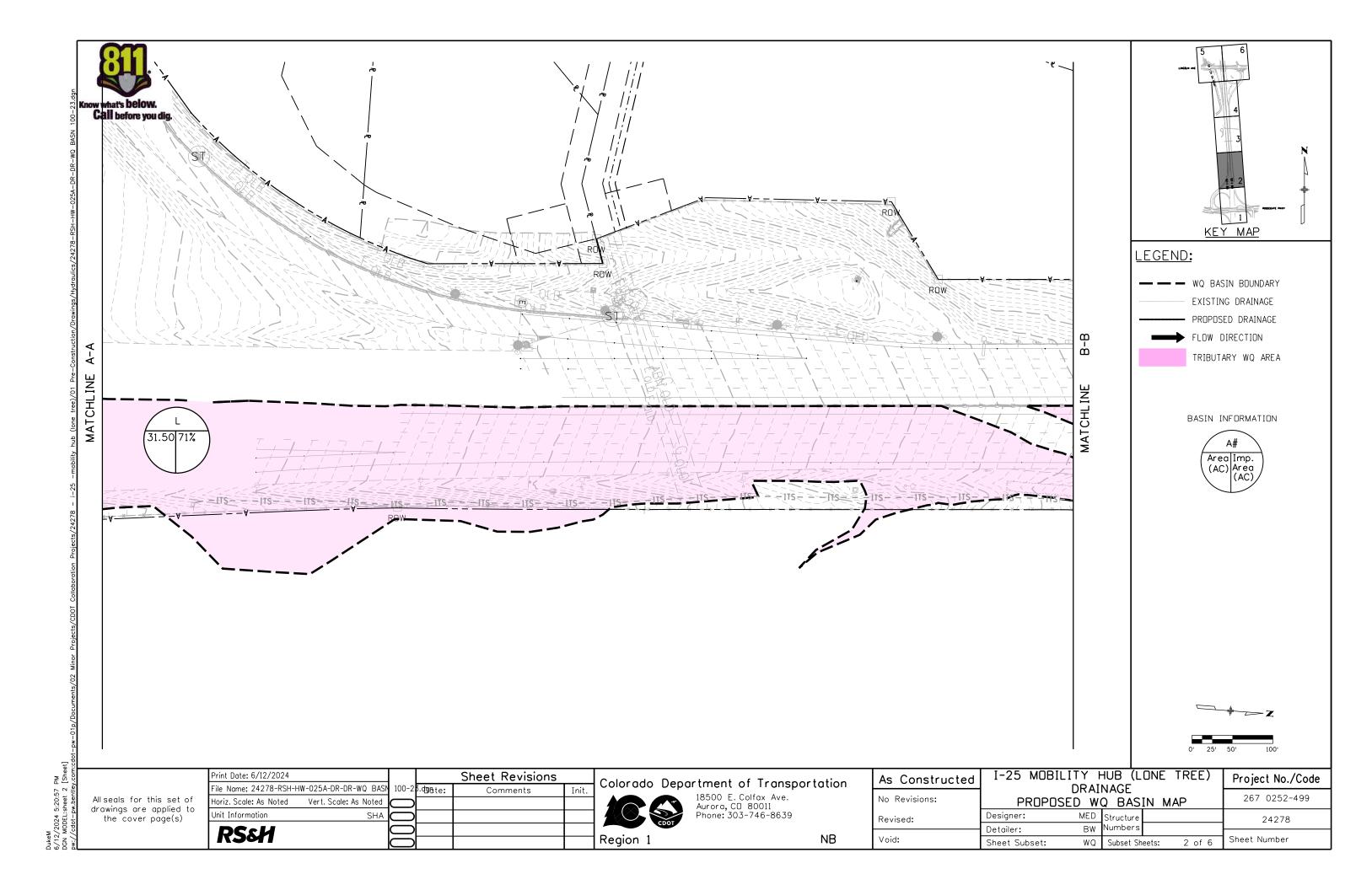


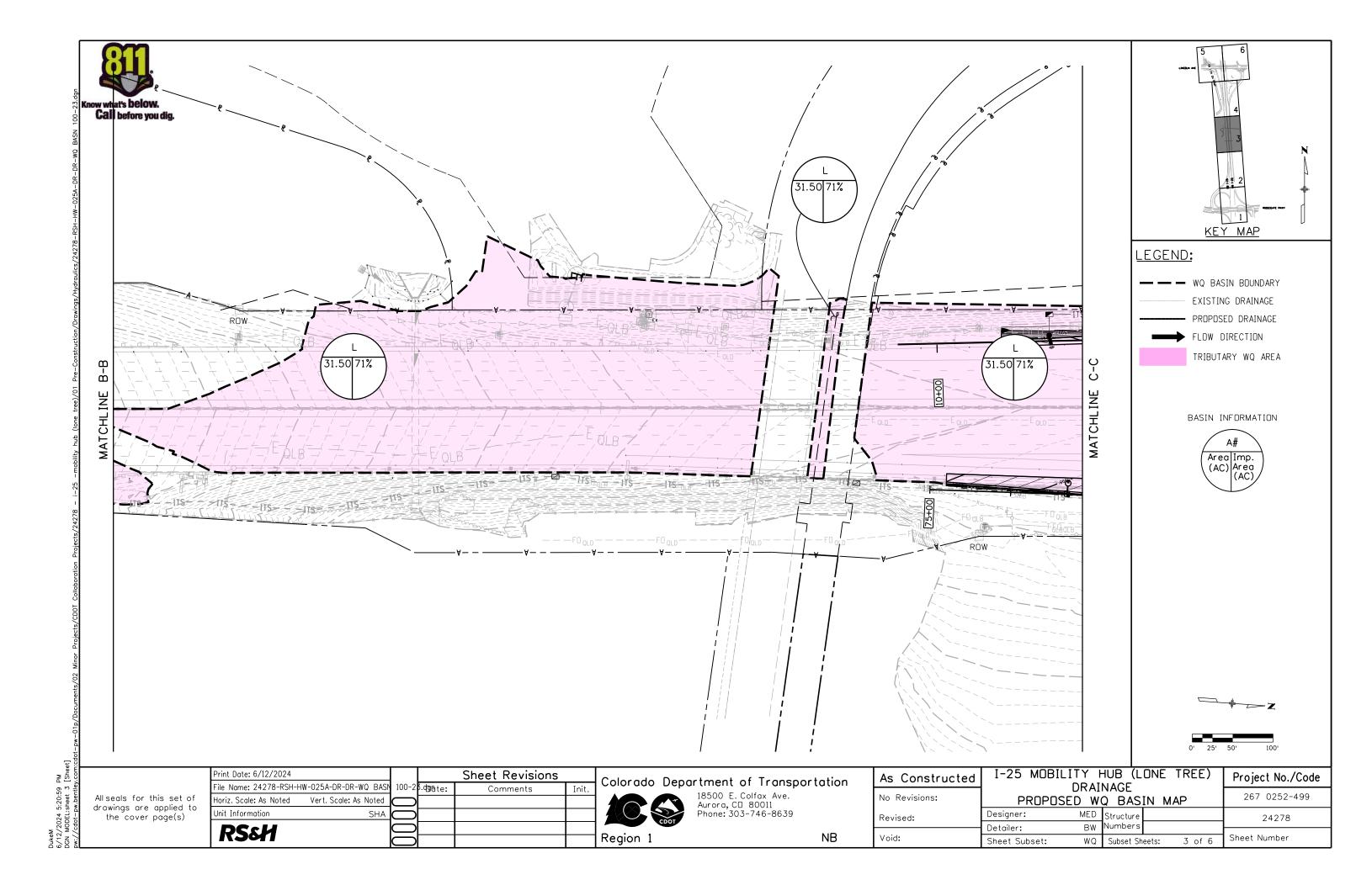
/2024 MODEL DukeM 6/12/: DGN_M

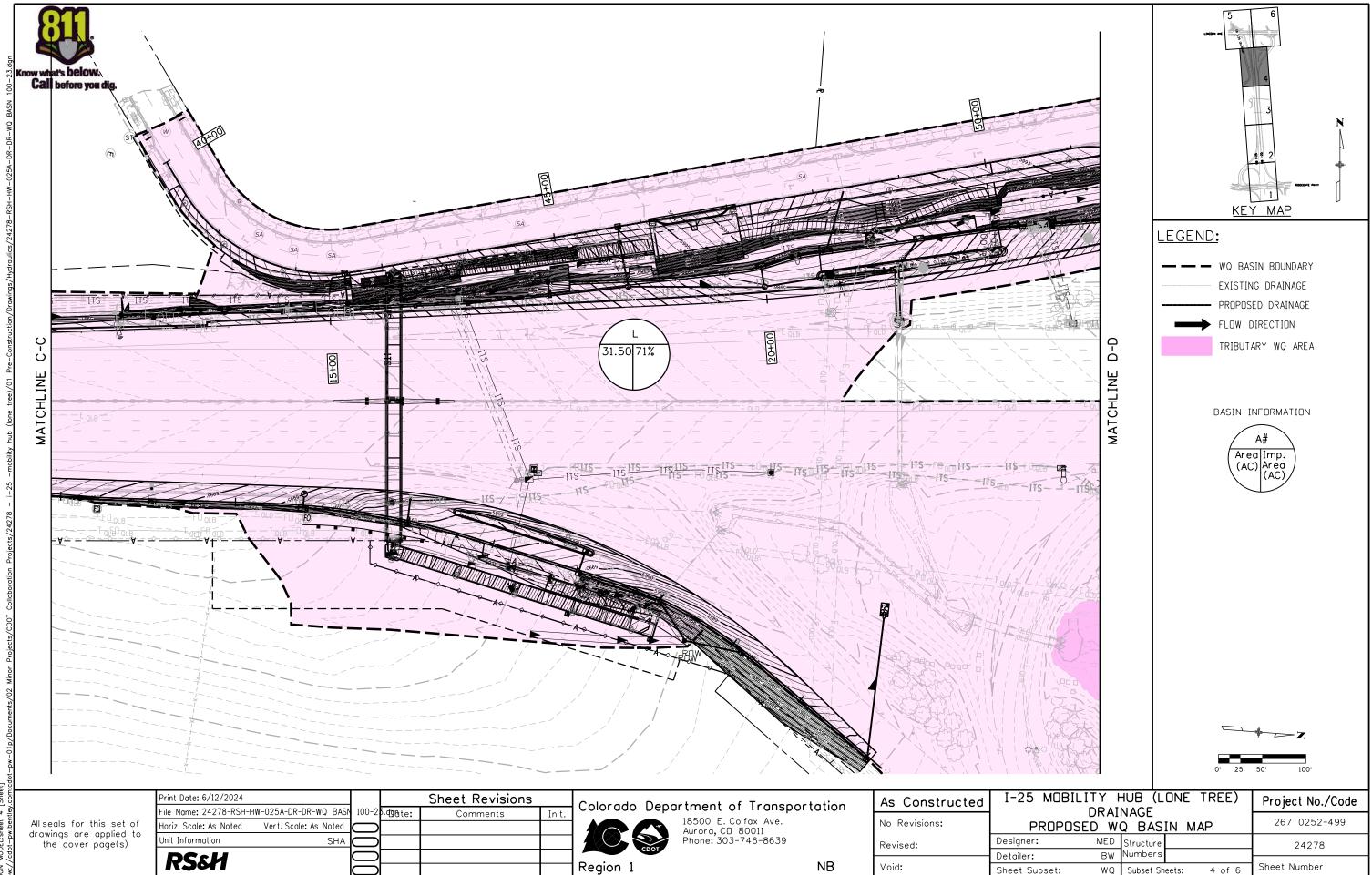


DukeM 6/12/2024 5:20:45 PM DGN MODEL:sheet 4 [Sheet]

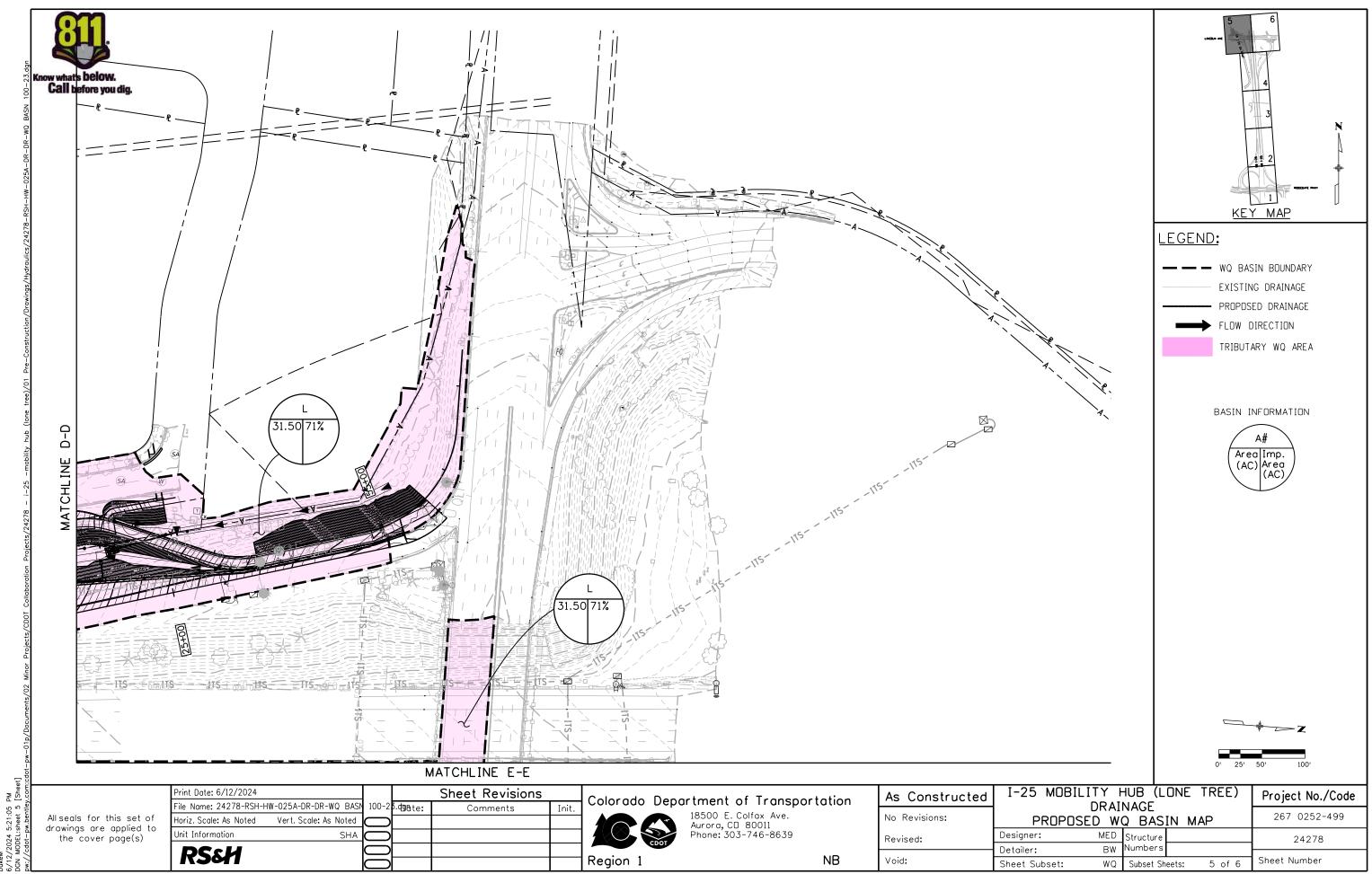




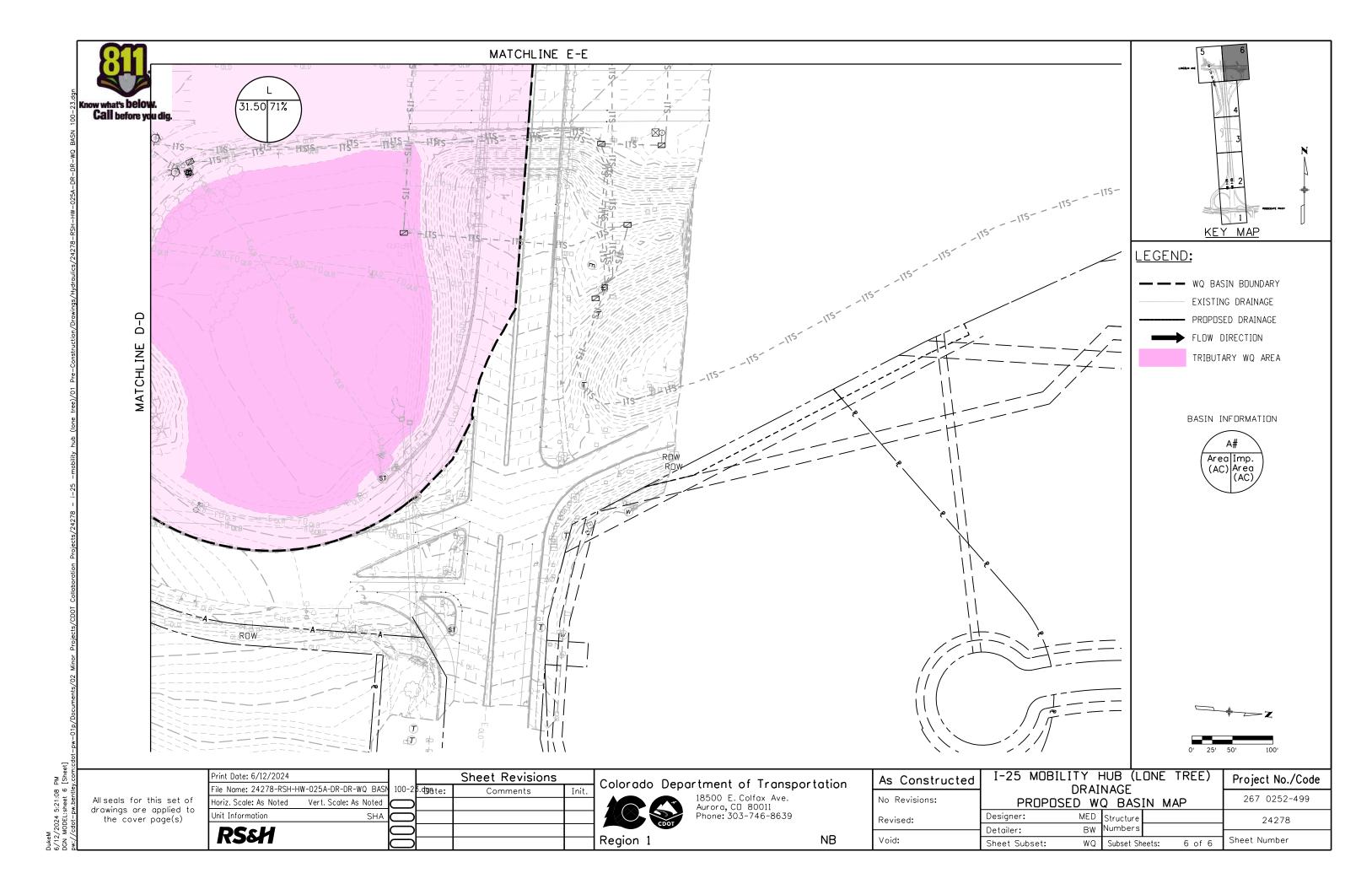




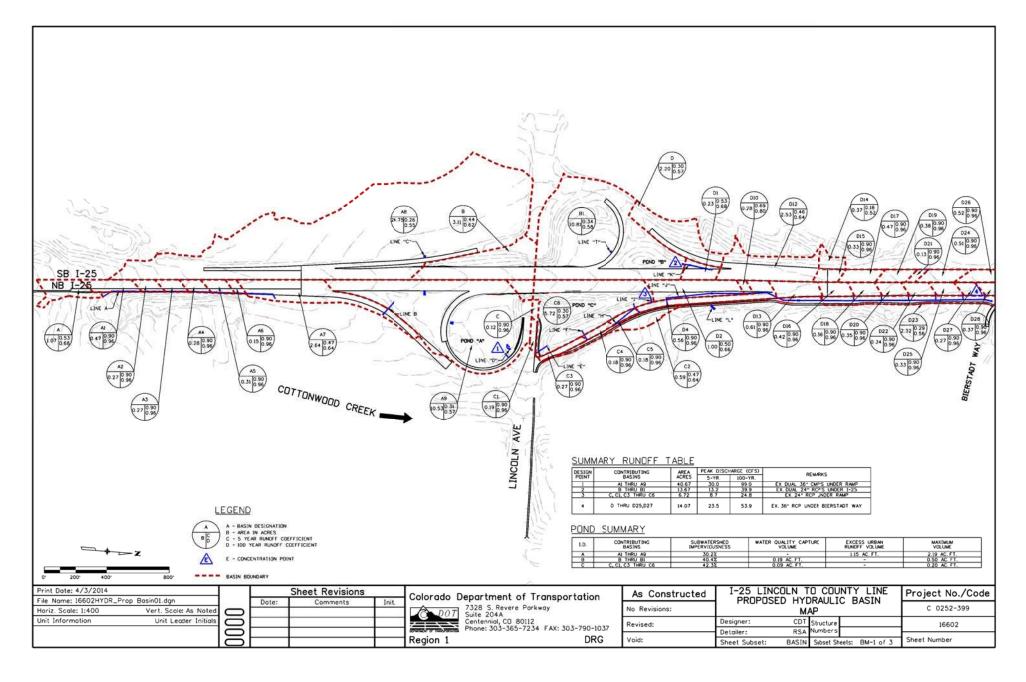
DukeM 6/12/2024 5:21:03 PM DGN MODEL:sheet 4 [Sheet]

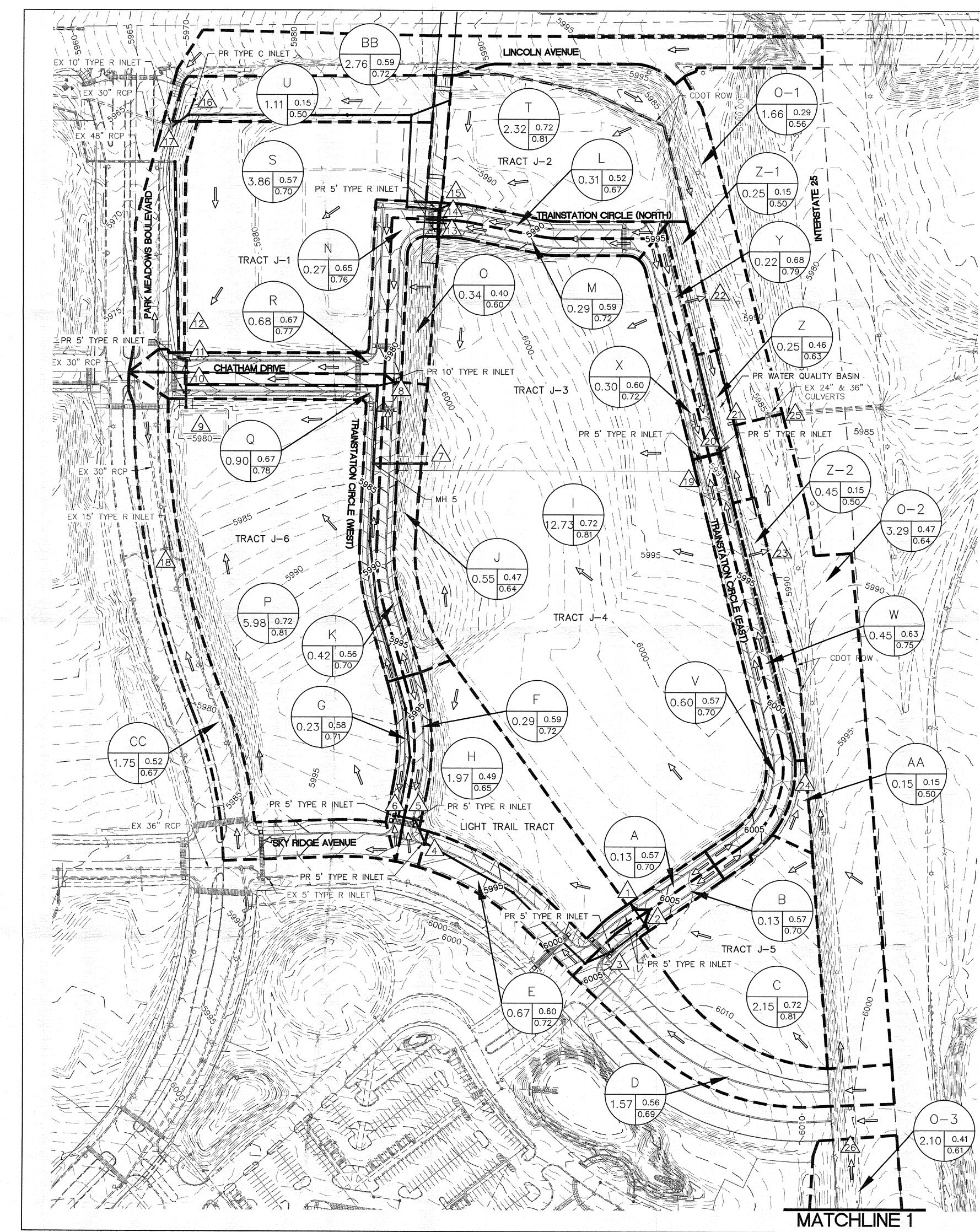


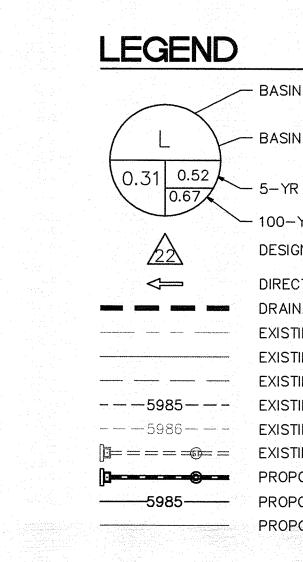
/2024 MODEL DukeM 6/12/



APPENDIX A.4 – EXISTING BASIN MAP



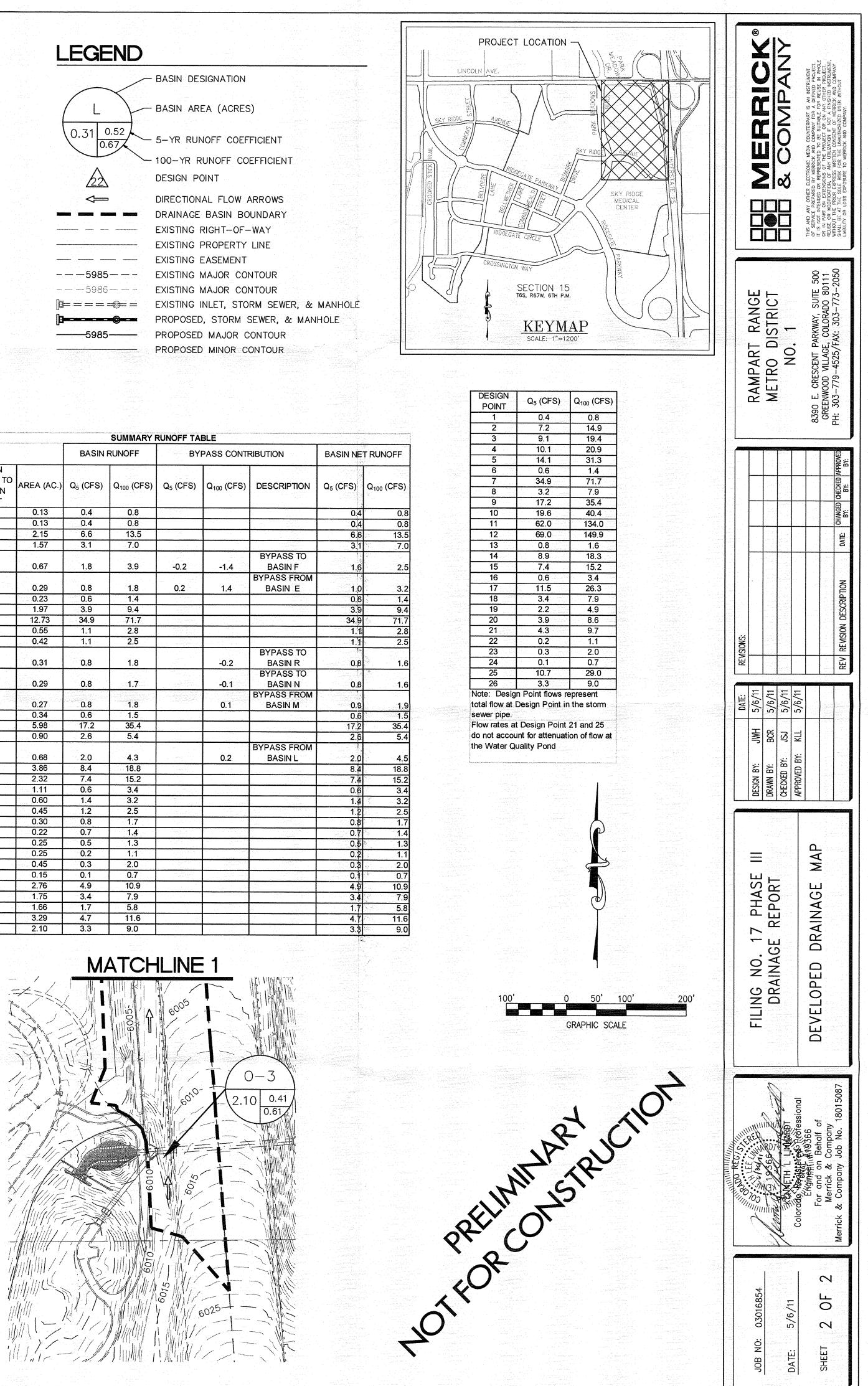




F	
2	
	5-YR RUNOFF CO
\sim	100-YR RUNOFF
	DESIGN POINT
	DIRECTIONAL FLO
	DRAINAGE BASIN
and the second	EXISTING RIGHT-
······································	EXISTING PROPER
	EXISTING EASEME
	EXISTING MAJOR
	EXISTING MAJOR
	EXISTING INLET, S
	PROPOSED, STOR
	PROPOSED MAJOR
	PROPOSED MINOR

، بر المادينية (مريد المريد (مادينية))، مريد المريدية (مريد المريدية))، مريد المريدية (مريد المريدية))، م	tere per la companya de la companya	annygi atala agan tarah tara manani miningan a manana mang		SUMMARY I	KUNOFF IA	BLE
			BASIN	RUNOFF	BY	PASS CON
BASIN ID	BASIN RUNOFF TO DESIGN POINT	AREA (AC.)	Q ₅ (CFS)	Q ₁₀₀ (CFS)	Q ₅ (CFS)	Q ₁₀₀ (CFS
А	1	0.13	0.4	0.8		
В	2	0.13	0.4	0.8		
C C	2	2.15	6.6	13.5	1 (w) 11	1
D	3	1.57	3.1	7.0		
E	4	0.67	1.8	3.9	-0.2	-1.4
F	5	0.29	0.8	1.8	0.2	1.4
G	6	0.23	0.6	1.4		
H	5	1.97	3.9	9.4		
	7	12.73	34.9	71.7		
J J	8	0.55	1.1	2.8		
К	8	0.42	1.1	2.5		
L	14	0.31	0.8	1.8		-0.2
M	13	0.29	0.8	1.7		-0.1
N	8	0.27	0.8	1.8		0.1
. 0,	8	0.34	0.6	1.5		
Р	9	5.98	17.2	35.4		
Q	10	0.90	2.6	5.4		، د می مرکز م
R	11	0.68	2.0	4.3		0.2
S	12	3.86	8.4	18.8		
Т	15	2.32	7.4	15.2		
U	16	1.11	0.6	3.4	and the second	
V t	19	0.60	1.4	3.2		
W	20	0.45	1.2	2.5		and a second sec
X	19	0.30	0.8	1.7	ingen en ser	
Y P	20	0.22	0.7	1.4		
Z	21	0.25	0.5	1.3		
Z-1	22	0.25	0.2	1.1		1
Z-2	23	0.45	0.3	2.0		
AA	24	0.15	0.1	0.7	1	
BB	17	2.76	4.9	10.9		
CC	18	1.75	3.4	7.9		1
0-1	25	1.66	1.7	5.8		
0-2	25	3.29	4.7	11.6	· · · · · ·	
O-3	26	2.10	3.3	9.0		





APPENDIX B – HYDRAULIC COMPUTATIONS

APPENDIX B.1 – INLET/SPREAD CALCULATIONS

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>IN-L-14</u>	<u>IN-L-15</u>	<u>IN-L-16</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	AREA	STREET
Hydraulic Condition	On Grade	Swale	On Grade
Inlet Type	Directional Cast Vane Grate	CDOT Type C	Directional Cast Vane Grate

USER-DEFINED INPUT

User-Defined Design Flows			
Minor Q _{Known} (cfs)	1.9	0.1	1.5
Major Q _{Known} (cfs)	3.1	0.5	2.4

Bypass (Carry-Over) Flow from Upstream Inlets must be organized from upstream (left) to downstream (right) in order for bypass flows to be linked.

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	IN-L-14
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.5
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0	1.2

Watershed Characteristics

Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		

Watershed Profile

Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		

Minor Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P_1 (inches)		

Major Storm Rainfall Input

One-Hour Precipitation, P ₁ (inches)	

Minor Total Design Peak Flow, Q (cfs)	1.9	0.1	2.1
Major Total Design Peak Flow, Q (cfs)	3.1	0.5	3.7
Minor Flow Bypassed Downstream, Q _b (cfs)	0.5	0.0	1.2
Major Flow Bypassed Downstream, Q _b (cfs)	1.2	0.0	2.3

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>IN-L-17-1</u>	<u>IN-L-17-3</u>	<u>IN-L-20</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	On Grade	On Grade	On Grade
Inlet Type	Directional Cast Vane Grate	Directional Cast Vane Grate	CDOT Type R Curb Opening

USER-DEFINED INPUT

Minor Q _{Known} (cfs)	0.6	0.8	1.5
Major Q _{Known} (cfs)	1.0	1.3	2.8

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	IN-L-16	IN-L-17-1	IN-L-17-3
Minor Bypass Flow Received, Q _b (cfs)	1.2	0.4	0.5
Major Bypass Flow Received, Q _b (cfs)	2.3	1.2	1.3

Watershed Characteristics

Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		

Watershed Profile

Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		

Minor Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P ₁ (inches)		

Major Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P_1 (inches)		

Minor Total Design Peak Flow, Q (cfs)	1.8	1.1	2.0
Major Total Design Peak Flow, Q (cfs)	3.3	2.5	4.1
Minor Flow Bypassed Downstream, Q _b (cfs)	0.4	0.5	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	1.2	1.3	0.0

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>IN-L-20-1</u>	<u>IN-L-24-1</u>	<u>IN-L-21-2</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	On Grade	On Grade
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening

USER-DEFINED INPUT

User-Defined Design Flows

Minor Q _{Known} (cfs)	0.7	1.0	0.6
Major Q _{Known} (cfs)	1.2	1.6	0.9

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	IN-L-20	No Bypass Flow Received	IN-L-24-1
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.1

Watershed Characteristics

Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		

Watershed Profile

Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		

Minor Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P_1 (inches)		

Major Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P_1 (inches)		

Minor Total Design Peak Flow, Q (cfs)	0.7	1.0	0.6
Major Total Design Peak Flow, Q (cfs)	1.3	1.6	1.0
Minor Flow Bypassed Downstream, Q _b (cfs)	N/A	0.0	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	N/A	0.1	0.0

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>IN-L-20-2</u>	<u>IN-L-20-3</u>	<u>IN-L-21-1</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	On Grade	On Grade	On Grade
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening

USER-DEFINED INPUT

User-Defined Design Flows			
Minor Q _{Known} (cfs)	1.1	0.4	0.7
Major Q _{Known} (cfs)	2.4	0.6	1.0

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	IN-L-21-2	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0

Watershed Characteristics

Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		

Watershed Profile

Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		

Minor Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P ₁ (inches)		

Major Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P_1 (inches)		

Minor Total Design Peak Flow, Q (cfs)	1.1	0.4	0.7
Major Total Design Peak Flow, Q (cfs)	2.4	0.6	1.0
Minor Flow Bypassed Downstream, Q _b (cfs)	0.0	0.0	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	0.0	0.0	0.0

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>IN-L-23</u>	<u>EX-IN-L-48-2</u>	<u>EX-IN-L-48-3</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	On Grade	In Sump	In Sump
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT/Denver 13 Valley Grate

USER-DEFINED INPUT

User-Defined Design Flows			
Minor Q _{Known} (cfs)	1.0	1.2	2.3
Major Q _{Known} (cfs)	1.5	2.0	4.0

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0

Watershed Characteristics

Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		

Watershed Profile

Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		

Minor Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P ₁ (inches)		

Major Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P_1 (inches)		

Minor Total Design Peak Flow, Q (cfs)	1.0	1.2	2.3
Major Total Design Peak Flow, Q (cfs)	1.5	2.0	4.0
Minor Flow Bypassed Downstream, Q _b (cfs)	0.0	N/A	N/A
Major Flow Bypassed Downstream, Q _b (cfs)	0.0	N/A	N/A

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>IN-L-12</u>	<u>IN-L-42</u>	<u>IN-L-45</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	AREA	STREET	STREET
Hydraulic Condition	Swale	On Grade	On Grade
Inlet Type	CDOT Type D (In Series)	CDOT Type R Curb Opening	CDOT Type R Curb Opening

USER-DEFINED INPUT

User-Defined Design Flows			
Minor Q _{Known} (cfs)	5.9	0.9	1.0
Major Q _{Known} (cfs)	12.0	1.5	1.6

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	IN-L-42
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.1

Watershed Characteristics

Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		

Watershed Profile

Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		

Minor Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P ₁ (inches)		

Major Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P_1 (inches)		

Minor Total Design Peak Flow, Q (cfs)	5.9	0.9	1.0
Major Total Design Peak Flow, Q (cfs)	12.0	1.5	1.7
Minor Flow Bypassed Downstream, Q _b (cfs)	0.0	0.0	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	0.0	0.1	0.3

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>EX-IN-L-48-1</u>	<u>EX-IN-L-21-5</u>	<u>IN-L-17-2</u>
Site Type (Urban or Rural)	URBAN	URBAN URBAN	
Inlet Application (Street or Area)	STREET	AREA	AREA
Hydraulic Condition	In Sump	Swale	Swale
Inlet Type	CDOT Type R Curb Opening	CDOT Type D (In Series & Depressed)	CDOT Type C

USER-DEFINED INPUT

User-Defined Design Flows						
Minor Q _{Known} (cfs)	2.0	3.7	0.1			
Major Q _{Known} (cfs)	3.2	6.5	0.6			

Bypass (Carry-Over) Flow from Upstream

Receive Bypass Flow from:	IN-L-45	No Bypass Flow Received	No Bypass Flow Received	
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0	
Major Bypass Flow Received, Q _b (cfs)	0.3	0.0	0.0	

Watershed Characteristics

Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		

Watershed Profile

Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		

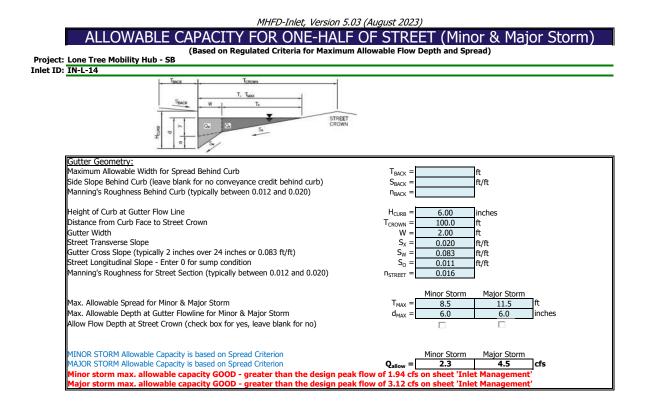
Minor Storm Rainfall Input

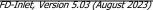
Design Storm Return Period, Tr (years)		
One-Hour Precipitation, P ₁ (inches)		

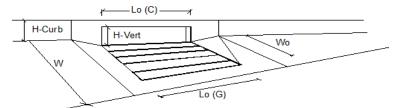
Major Storm Rainfall Input

· · · · · · · · · · · · · · · · · · ·		
Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P ₁ (inches)		

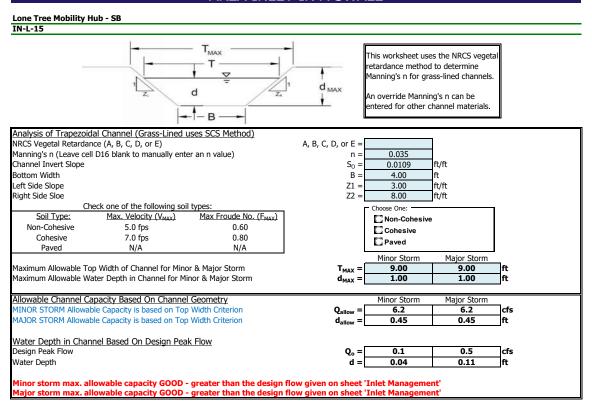
Minor Total Design Peak Flow, Q (cfs)	2.0	3.7	0.1
Major Total Design Peak Flow, Q (cfs)	3.5	6.5	0.6
Minor Flow Bypassed Downstream, Q _b (cfs)	N/A	0.0	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	N/A	0.0	0.0

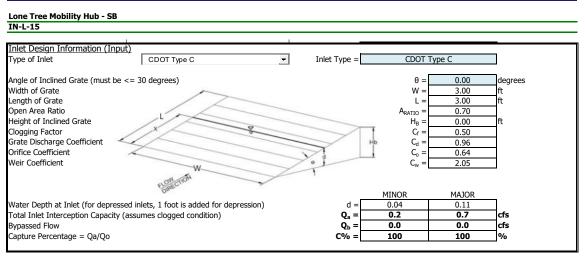


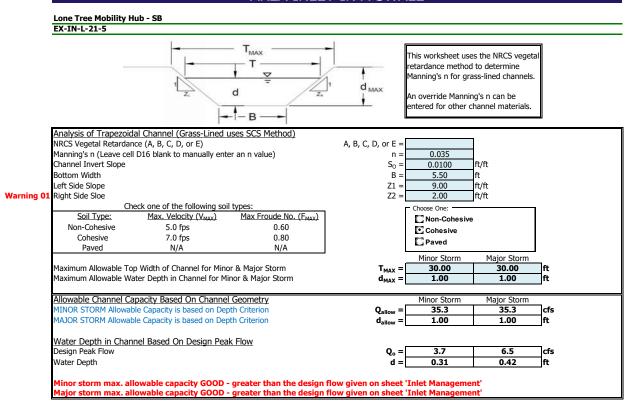


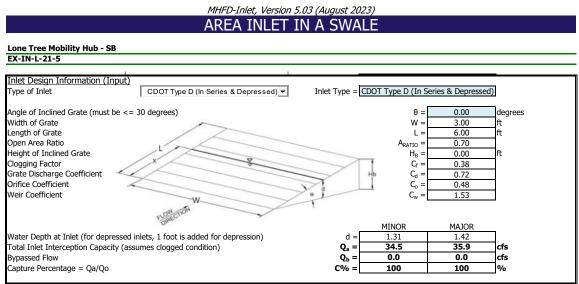


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =		ast Vane Grate	1
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	0.0	0.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	linches
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_0 =$	3.00	3.00	ft
5 5		2.00	2.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_{o} =$			π
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	0.50	0.50	-
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	N/A	N/A	
Street Hydraulics: OK - Q < Allowable Street Capacity'	- T	MINOR	MAJOR	٦.
Design Discharge for Half of Street (from Inlet Management)	Q _o =	1.9	3.1	cfs
Water Spread Width	T =	7.7	9.8	ft
Water Depth at Flowline (outside of local depression)	d =	3.4	3.9	inches
Water Depth at Street Crown (or at T _{MAX})	d _{CROWN} =	0.0	0.0	inches
Ratio of Gutter Flow to Design Flow	E ₀ =	0.701	0.586	
Discharge outside the Gutter Section W, carried in Section T_x	$Q_x =$	0.6	1.3	cfs
Discharge within the Gutter Section W	Q _w =	1.4	1.8	cfs
Discharge Behind the Curb Face	Q _{BACK} =	0.0	0.0	cfs
Flow Area within the Gutter Section W	A _W =	0.40	0.48	sq ft
Velocity within the Gutter Section W	V _w =	3.4	3.8	fps
Water Depth for Design Condition	d _{LOCAL} =	3.4	3.9	inches
Grate Analysis (Calculated)	110.0	MINOR	MAJOR	
Total Length of Inlet Grate Opening	L =	3.00	3.00	ft
Ratio of Grate Flow to Design Flow	E _{o-GRATE} =	0.701	0.586	
Under No-Clogging Condition	-0-GRATE	MINOR	MAJOR	
Minimum Velocity Where Grate Splash-Over Begins	V ₀ =	7.11	7.11	fps
Interception Rate of Frontal Flow	V ₀ – R _f =	1.00	1.00	ihe
				-
Interception Rate of Side Flow	$R_x =$	0.23	0.20	
Interception Capacity	$Q_i =$	1.5	2.1	cfs
Under Clogging Condition		MINOR	MAJOR	-
Clogging Coefficient for Multiple-unit Grate Inlet	GrateCoeff =	1.00	1.00	_
Clogging Factor for Multiple-unit Grate Inlet	GrateClog =	0.50	0.50	
Effective (unclogged) Length of Multiple-unit Grate Inlet	L _e =	1.50	1.50	ft
Minimum Velocity Where Grate Splash-Over Begins	V _o =	5.13	5.13	fps
Interception Rate of Frontal Flow	R _f =	1.00	1.00	
Interception Rate of Side Flow	R _x =	0.06	0.05	
Actual Interception Capacity	Q _a =	1.4	1.9	cfs
Carry-Over Flow = $Q_0 - Q_a$ (to be applied to curb opening or next d/s inlet)	$Q_{\rm b} =$	0.5	1.2	cfs
Curb Opening or Slotted Inlet Analysis (Calculated)		MINOR	MAJOR	
Equivalent Slope S _e	S _e =	N/A	N/A	ft/ft
Required Length L_{T} to Have 100% Interception	L _T =	N/A	N/A	ft
Under No-Clogging Condition	-, [MINOR	MAJOR	
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L_T)	L =	N/A	N/A	ft
Interception Capacity	$Q_i =$	N/A	N/A	cfs
Under Clogging Condition	Qi –	MINOR	MAJOR	0.5
Clogging Coefficient	CurbCoeff =	N/A	MAJOR N/A	7
				-
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet	CurbClog =	N/A	N/A	
Effective (Unclogged) Length	L _e =	N/A	N/A	ft
Actual Interception Capacity	$Q_a =$	N/A	N/A	cfs
Carry-Over Flow = $Q_{b(GRATF)}$ - Q_a	Q _b =	N/A	N/A	cfs
Summary	F	MINOR	MAJOR	٦.
Total Inlet Interception Capacity	Q =	1.4	1.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.5	1.2	cfs
Capture Percentage = Q_a/Q_a	C% =	72	61	%

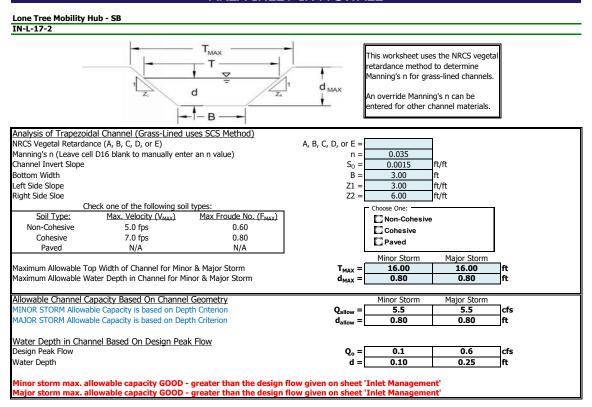




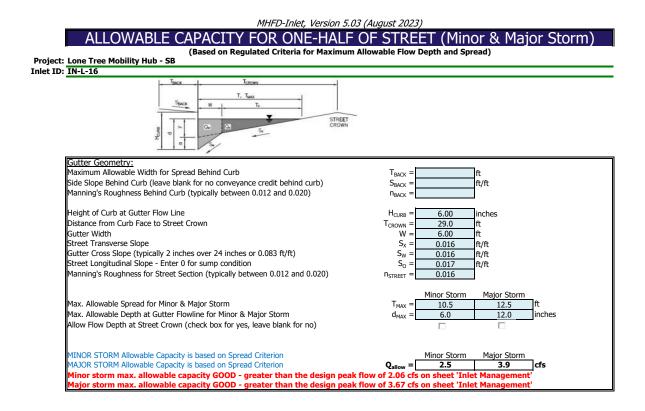


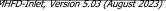


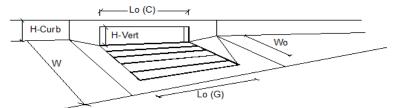




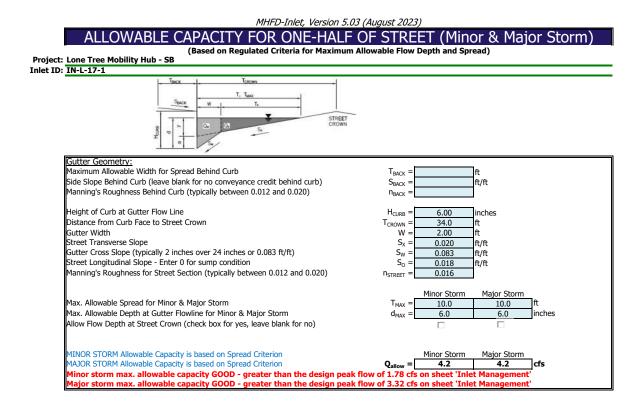
Lone Tree Mobility Hub - SB IN-L-17-2 Inlet Design Information (Input) CDOT Type C CDOT Type C -Inlet Type = Type of Inlet Angle of Inclined Grate (must be <= 30 degrees) θ= 0.00 degrees Width of Grate W = 3.00 ft Length of Grate L 3.00 ft Open Area Ratio Height of Inclined Grate Clogging Factor Grate Discharge Coefficient Orifice Coefficient A_{RATIO} 0.70 HB 0.00 ft Cf 0.50 C_d 0.96 C_o 0.64 Weir Coefficient C_w 2.05 W FLON DIRECTION MAJOR MINOR Water Depth at Inlet (for depressed inlets, 1 foot is added for depression) Total Inlet Interception Capacity (assumes clogged condition) d : 0.10 **0.6** 0.25 **2.4** Q_a = cfs Bypassed Flow **Q**_b = 0.0 0.0 cfs Capture Percentage = Qa/Qo C% 100 % 100

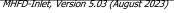


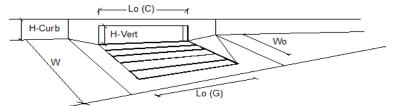




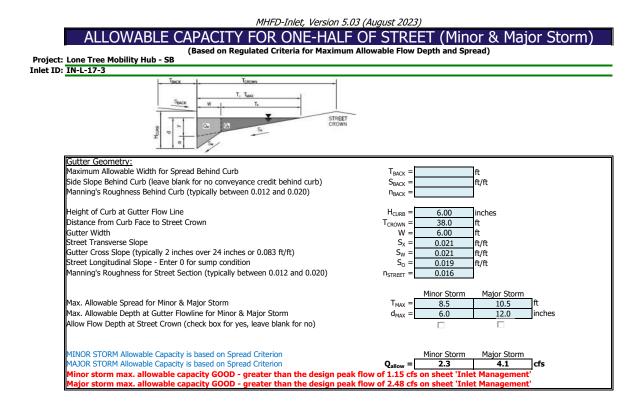
Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	Directional Ca	ast Vane Grate	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	0.0	0.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	3.00	3.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	2.00	2.00	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	N/A	N/A	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.9	1.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	1.2	2.3	cfs
Capture Percentage = Q_a/Q_o	C% =	42	36	%

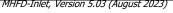


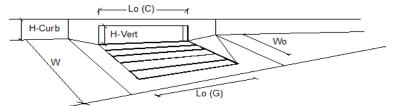




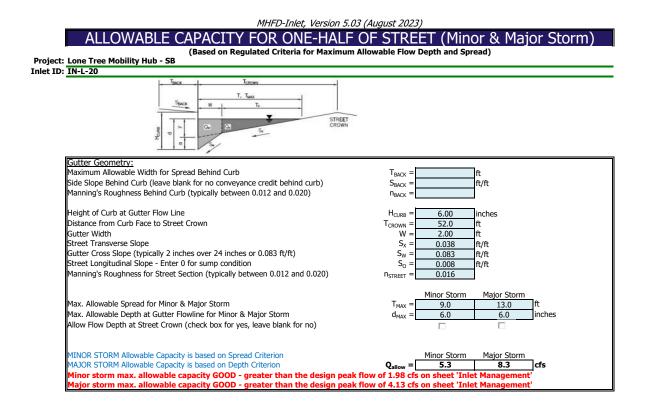
Design Information (Input)	1	MINOR	MAJOR	_
Type of Inlet	Type =	Directional Ca	ast Vane Grate	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	0.0	0.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	3.00	3.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	2.00	2.00	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	N/A	N/A	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.4	2.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.4	1.2	cfs
Capture Percentage = Q_a/Q_o	C% =	79	64	%

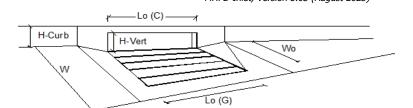




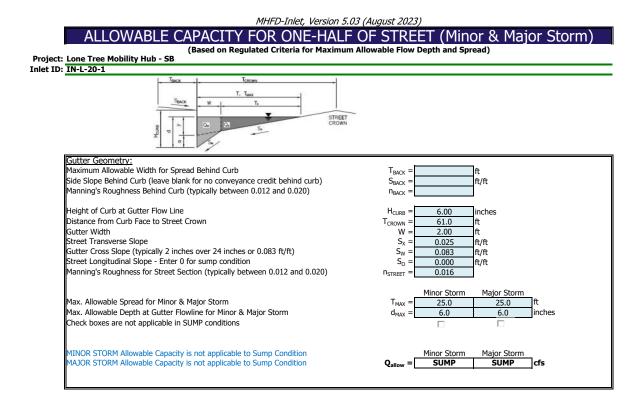


Design Information (Input)	-	MINOR	MAJOR	
Type of Inlet	Type =	Directional Ca	ast Vane Grate	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	0.0	0.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	3.00	3.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	2.00	2.00	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	N/A	N/A	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.6	1.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.5	1.3	cfs
Capture Percentage = Q_a/Q_o	C% =	55	46	%

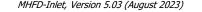


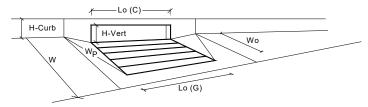


Design Information (Input)	1	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.0	4.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.0	cfs
Capture Percentage = Q_a/Q_o	C% =	100	100	%

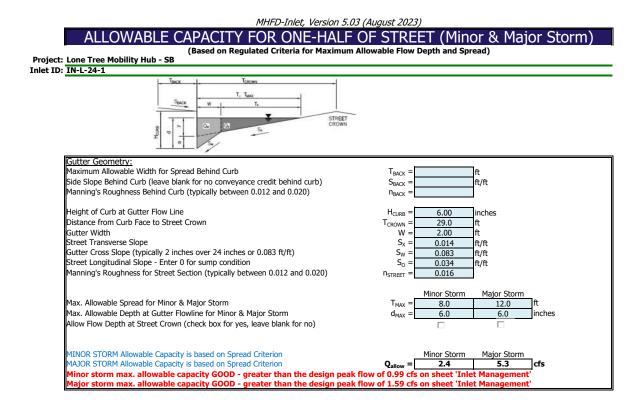


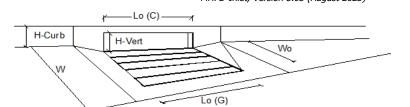
INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.03 (August 2023)



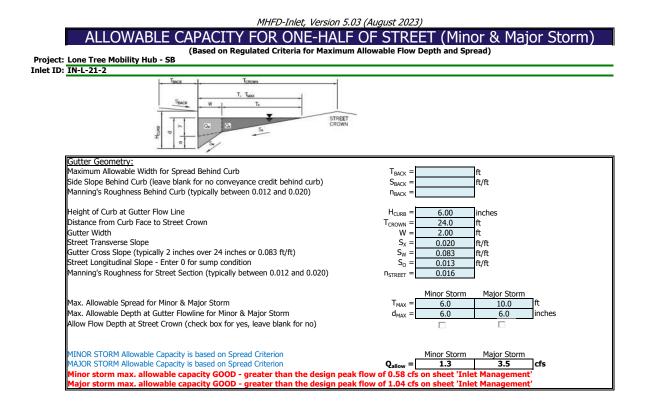


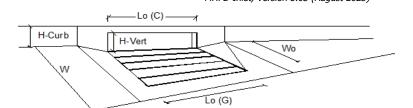
Type of InletCDOT Type R Curb OpeningLocal Depression (additional to continuous gutter depression 'a' from above)Type =CDOT Type R Curb OpeningNumber of Unit Inlets (Grate or Curb Opening)No 3.00 3.00 Water Depth at Flowline (outside of local depression)Ponding Depth = 6.0 6.0 Grate Information $No =$ 11Length of a Unit GrateNINORMAIOROverride DepthsVigth of a Unit Grate N_0 N_0 $ReatOpen Area Ratio for a Grate (typical values 0.15-0.90)C_0 (G) =N/AN/AClogging Factor for a Single Grate (typical value 0.50 - 0.70)C_0 (G) =N/AN/AGrate Orifice Coefficient (typical value 0.60 - 0.80)C_w (G) =N/AN/ACurb Opening InformationMiNORMAIORMAIORLength of a Unit Curb OpeningH_{wett} =6.006.00Height of Vertical Curb Opening In InchesH_{wett} =6.006.00Height of Curb Opening (typical value 0.60 - 0.70)C_v (C) =0.100.10Curb Opening Weir Coefficient (typical value 0.60 - 0.70)C_v (C) =0.670.67Curb Opening Weir Coefficient (typical value 0.60 - 0.70)C_v (C) =0.670.67Curb Opening Weir Coefficient (typical value 0.60 - 0.70)C_v (C) =0.670.67Low Head Performance Reduction Factor for Long InletsRF_{curb} =0.003.03ftCurb Opening Weir Coefficient (typical value 0.60 - 0.70)$	Design Information (Input)		MINOR	MAJOR	
Local Depression (additional to continuous gutter depression 'a' from above) Number of Unit Inlets (Grate or Curb Opening) Water Depth of a Unit Grate Open Area Ratio for a Grate (typical values 0.15-0.90) Clogging Factor for a Single Grate (typical values 0.15-0.90) Clogging Factor for a Single Grate (typical value 0.50 - 0.70) Grate Orffice Coefficient (typical value 0.50 - 0.70) Grate Orffice Coefficient (typical value 0.60 - 0.80) Length of a Unit Curb Opening Information Length of a Unit Curb Opening Information Length of Depression Pan (typically the gutter width of 2 feet) Clogging Factor for a Single Curb Opening (typical value 0.10) Curb Opening Weir Coefficient (typical value 0.60 - 0.70) Curb Opening Weir Coefficient (typical value 0.60 - 0.70) Curb Opening Information Length of a Unit Curb Opening in Inches Height of Vertical Curb Opening (typical value 0.10) Curb Opening Weir Coefficient (typical value 0.60 - 0.70) Curb Opening Meir Equat		Type -			٦
Number of Unit Inlets (Grate or Curb Opening)No11Water Depth at Flowline (outside of local depression) Grate Information Length of a Unit GrateNo11Width of a Unit Grate Width of a Unit GratePonding Depth =6.06.0inchesWidth of a Unit Grate Open Area Ratio for a Grate (typical value 0.15-0.90) Clogging Factor for a Single Grate (typical value 0.50 - 0.70) Grate Orifice Coefficient (typical value 0.50 - 0.80) Curb Opening Information Length of a Unit Curb Opening Information Length of a Unit Curb Opening Information Length of a Unit Orub Opening Information Length of a Unit Curb Opening Inches Height of Vertical Curb Opening Inches Angle of Throat Side Width for Depression Pan (typical value 0.10) Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_{v} (G) = N/A N/A Curb Opening Weir Coefficient (typical value 0.60 - 0.70) Curb Opening Weir Coefficient (typical value 0.10) Curb Opening Weir Coefficient (typical value 0.10) Curb Opening Weir Coefficient (typical value 0.10) Curb Opening Weir Equation Grate Midwidth Depth for Curb Opening Weir Equation Grate Inlet Performance Reduction Factor for Long InletsMINOR MAJOR MAJOR MAJOR Curb Opening Weir Equation Grate Inlet Performance Reduction Factor for Long InletsMINOR MAJOR MAJOR Curb Opening Neir Equation Grate Midwidth Depth for Curb Opening Weir Equation Grate Inlet Performance Reduction Factor for Long InletsMINOR ReformateMINOR MAJOR MAJOR Curb Opening Weir Equation Grate Inlet Performance Reduction Factor for Long InletsMINOR ReformateMAJOR MAJOR Curb Opening Major MAJORTotal Inlet Interception Capacity (assumes		· · ·			inches
Water Depth at Flowline (outside of local depression) Grate Linformation Length of a Unit GratePonding Depth =6.06.0inchesMINORMAIOROverride DepthsWidth of a Unit Grate L_0 (G) =N/AN/AFeetWidth of a Unit Grate W_0 =N/AN/AFeetOpen Area Ratio for a Grate (typical values 0.15-0.90) C_r (G) =N/AN/AFeetClogging Factor for a Single Grate (typical value 2.15 - 3.60) C_w (G) =N/AN/AFeetGrate Wer Coefficient (typical value 2.15 - 3.60) C_w (G) =N/AN/AFeetGrate Wer Coefficient (typical value 2.15 - 3.60) C_w (G) =N/AN/AFeetCurb Opening Information C_v (G) =N/AN/AFeetLength of a Unit Curb Opening L_0 (C) = C_0 (G) =N/AN/AHeight of Vertical Curb Opening Information H_{vert} = 6.00 6.00 inchesHeight of Depression Pan (typically the gutter width of 2 feet) W_p = 2.00 2.00 feetClogging Factor for a Single Curb Opening (typical value 2.13-7) C_v (C) = 0.60 3.60 3.60 Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_v (C) = 0.67 0.67 0.67 Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_v (C) = 0.60 3.60 3.60 Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_v (C) = 0.67 0.67 Low Head Performance Reduction Factor for Long Inlets				1	inches
Grate InformationMINORMAJOROverride DepthsLength of a Unit Grate V_0 a Unit Grate V_0 a Unit Grate V_0 a V_0 N/A V_0 feetOpen Area Ratio for a Grate (typical value 0.15 - 0.90) A_{ratio} = N/A N/A N/A Clogging Factor for a Single Grate (typical value 0.50 - 0.70) C_1 (G) = N/A N/A N/A Grate Weir Coefficient (typical value 0.60 - 0.80) C_0 (G) = N/A N/A N/A Curb Opening Information $MINOR$ $MAJOR$ $MAJOR$ Length of a Unit Curb Opening in Inches H_{wett} = 6.00 6.00 Height of Vertical Curb Opening in Inches H_{wett} = 6.00 6.00 Angle of Throat $MINOR$ $MAJOR$ $G3.40$ $degrees$ Side Width for Depression Pan (typically the gutter width of 2 feet) W_p = 2.00 2.00 Curb Opening Weir Coefficient (typical value 2.3-3.7) C_v (C) = 3.60 3.60 Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_v (C) = 0.33 0.33 ftDepth for Grate Midwidth B_{curb} = 0.33 0.33 ftDepth for Grate Midwidth R_{fourbe} = 1.00 1.00 Depth for Grate Midwidth R_{fourbe} = N/A N/A Depth for Grate Midwidth <td></td> <td>-</td> <td>-</td> <td>6.0</td> <td>inchos</td>		-	-	6.0	inchos
Length of a Unit Grate L_{o} (G) = N/A N/A Width of a Unit Grate W_{o} = N/A N/A Open Area Ratio for a Grate (typical value 0.50 - 0.70) C_{c} (G) = N/A N/A Grate Weir Coefficient (typical value 2.15 - 3.60) C_{c} (G) = N/A N/A Grate Orifice Coefficient (typical value 2.15 - 3.60) C_{c} (G) = N/A N/A Grate Orifice Coefficient (typical value 2.15 - 3.60) C_{c} (G) = N/A N/A Grate Orifice Coefficient (typical value 2.15 - 3.60) C_{c} (G) = N/A N/A Grate Orifice Coefficient (typical value 0.60 - 0.80) C_{c} (G) = N/A N/A Length of a Unit Curb Opening In Inches H_{corth} E_{c} (C) = $S.00$ Height of Curb Orifice Throat in Inches H_{wroat} E_{c} (C) = $S.00$ Side Width for Depression Pan (typical value 0.10) C_{c} (C) = 0.10 0.10 Curb Opening Weir Coefficient (typical value 0.10) C_{c} (C) = 0.10 0.10 Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_{c} (C) = 0.57 0.67 Low Head Performance Reduction (Calculated) M_{corth} N/A N/A N/A Depth for Grate Midwidth d_{crate} N/A N/A N/A Depth for Grate Midwidth C_{corth} $C_{oothination}$ N/A N/A Depth for Grate Midwidth R_{Fcorth} N/A N/A N/A Depth for Grate Midwidth R_{Fcorth} N/A N/A N/A		Fonding Depth =			
Width of a Unit Grate Open Area Ratio for a Grate (typical values 0.15-0.90) $W_o =$ N/A N/A N/A Clogging Factor for a Single Grate (typical value 0.50 - 0.70) Grate Weir Coefficient (typical value 0.15 - 3.60) C_r (G) = N/A N/A Grate Veir Coefficient (typical value 0.60 - 0.80) C_w (G) = N/A N/A Curb Opening Information Length of a Unit Curb Opening in Inches $H_{ort} =$ 6.00 6.00 Height of Vertical Curb Opening in Inches $H_{ort} =$ 6.00 6.00 Height of Curb Orifice Throat in Inches $H_{ort} =$ 6.00 6.00 Side Width for Depression Pan (typically the gutter width of 2 feet) $W_p =$ 2.00 2.00 Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_v (C) = 3.60 3.60 Curb Opening Weir Coefficient (typical value 0.10) C_v (C) = 0.10 0.10 Curb Opening Weir Equation Grated Inlet Performance Reduction Factor for Long Inlets $RF_{Gate} =$ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $RF_{combination} =$ N/A N/A Curb Opening Inlet Performance Reduction Factor for Long Inlets $RF_{combination} =$ N/A N/A Curb Inlet Interception Capacity (assumes clogged condition) $Q_a =$ $\overline{5.4}$ $\overline{5.4}$ $\overline{5.4}$		(G) =			
Open Area Ratio for a Grate (typical values 0.15-0.90) $A_{ratio} = \frac{N/A}{A}$ N/A N/A Clogging Factor for a Single Grate (typical value 0.50 - 0.70) C_r (G) = N/A N/A Grate Veir Coefficient (typical value 2.15 - 3.60) C_v (G) = N/A N/A Grate Orifice Coefficient (typical value 0.60 - 0.80) C_v (G) = N/A N/A Curb Opening Information C_v (G) = N/A N/A Length of a Unit Curb Opening in Inches H_{edit} 6.00 6.00 Height of Vertical Curb Opening in Inches H_{rect} 6.00 6.00 Angle of Throat N/A N/A N/A Side Width for Depression Pan (typical value 0.10) C_v (C) = 0.10 0.10 Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_v (C) = 0.67 0.67 Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_v (C) = 0.33 0.33 0.33 Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_v (C) = 0.33 0.33 0.33 Curb Opening Weir Equation $C_{curb} = \frac{N/A}{A}$ N/A N/A Depth for Grate Midwidth $d_{Grate} = \frac{N/A}{A}$ N/A N/A Depth for Grate Midwidth $R_{Curb} = \frac{N/A}{A}$ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $R_{FGrate} = \frac{N/A}{A}$ N/A Curb Opening Performance Reduction Factor for Long Inlets $R_{FGrate} = \frac{N/A}{A}$ N/A Curb Opening Performance Reduction Factor for Long Inlets $R_{FGrate} = $,	1	
Clogging Factor for a Single Grate (typical value $0.50^{\circ} - 0.70$) Grate Weir Coefficient (typical value $2.15 - 3.60$) Grate Veir Coefficient (typical value $0.60 - 0.80$) Curb Opening Information Length of a Unit Curb Opening Height of Vertical Curb Opening in Inches Height of Vertical Curb Opening in Inches Height of Curb Orifice Throat in Inches Angle of Throat Side Width for Depression Pan (typical value 0.10) Curb Opening Weir Coefficient (typical value $0.3.77$) Curb Opening Orifice Coefficient (typical value $0.3.77$) Curb Opening Orifice Coefficient (typical value $0.3.77$) Curb Opening Weir Coefficient (typical value $0.50 - 0.70$) Low Head Performance Reduction Factor for Long Inlets Curb Opening Coefficient (assumes clogged condition) Total Inlet Interception Capacity (assumes clogged condition)		0			leet
Grate Weir Coefficient (typical value 2.15 - 3.60) C_w (G) = N/A N/A Grate Orifice Coefficient (typical value 0.60 - 0.80) C_o (G) = N/A N/A Curb Opening InformationLength of a Unit Curb Opening $MINOR$ MAJORLength of a Unit Curb Opening in Inches H_{vert} 6.00 6.00 Height of Curb Orifice Throat in Inches H_{vert} 6.00 6.00 Angle of ThroatSide Width for Depression Pan (typical value 0.10) C_r (C) = 0.10 0.10 Curb Opening Weir Coefficient (typical value 2.3-3.7) W_p = 2.00 2.00 Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_o (C) = 0.67 0.67 Low Head Performance Reduction (Calculated)MINORMAJORDepth for Grate Midwidth d_{curb} = 0.33 0.33 Depth for Grate Midwidth d_{curb} = 1.00 1.00 Curb Opening Veir Equation RF_{core} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $RF_{combination}$ = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $RF_{combination}$ = N/A N/A Curb Opening Chiper Coefficient (upper Coefficient for Long Inlets $RF_{combination}$ = N/A N/A Curb Opening Veir Equation $RF_{combination}$ = N/A N/A N/A Curb Opening Veir Equation Factor for Long Inlets $RF_{combination}$ = N/A N/A Curb Opening Coefficient (upper Coefficient for Long Inlets RF_{co				1	
Grate Orifice Coefficient (typical value 0.60 - 0.80) C_o (G) = N/A N/A Curb Opening Information Length of a Unit Curb Opening in Inches $MINOR$ $MAIOR$ Height of Vertical Curb Opening in Inches L_o (C) = 5.00 5.00 Height of Curb Orifice Throat in Inches H_{tert} = 6.00 6.00 Angle of Throat C_o (G) = 0.10 0.10 Side Width for Depression Pan (typical value 0.10) C_c (C) = 0.10 0.10 Curb Opening Orifice Coefficient (typical value 2.3-3.7) C_w (C) = 3.60 3.60 Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_o (C) = 0.67 0.67 Low Head Performance Reduction (Calculated) $MINOR$ $MAJOR$ Depth for Grate Midwidth d_{Grate} = N/A N/A N/A Depth for Curb Opening Weir Equation Grated Inlet Performance Reduction Factor for Long Inlets Curb Opening Performance Reduction Factor for Long Inlets RF_{Grate} = N/A N/A Curb Opening Veir Equation Grated Inlet Performance Reduction Factor for Long Inlets Curb Opening Veir Equation Factor for Long Inlets RF_{Crurb} = N/A N/A Total Inlet Interception Capacity (assumes clogged condition) Q_a = 5.4 5.4 5.4					-
MINORMAJORLength of a Unit Curb OpeningInchesHeight of Vertical Curb Opening in Inches $L_o (C) = 5.00$ Height of Curb Orifice Throat in Inches $H_{wett} = 6.00$ Angle of Throat $H_{wett} = 6.00$ Side Width for Depression Pan (typically the gutter width of 2 feet) $W_p = 2.00$ Curb Opening Weir Coefficient (typical value 0.10) $C_r (C) = 0.10$ Curb Opening Weir Coefficient (typical value 2.3-3.7) $C_w (C) = 3.60$ Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) $C_o (C) = 0.67$ Low Head Performance Reduction (Calculated)MINORDepth for Grate Midwidth $d_{Grate} = N/A$ Depth for Grate Midwidth $d_{Grate} = N/A$ Curb Opening Veir Equation $d_{Grate} = N/A$ Grated Inlet Performance Reduction Factor for Long Inlets $RF_{Grate} = N/A$ Curb Opening Performance Reduction Factor for Long Inlets $RF_{Corrbination} = N/A$ Curb Opening Veir Coefficient (typical value 0.60 - 0.70) $R_{Curb} = 1.00$ Low Head Performance Reduction Factor for Long Inlets $RF_{Grate} = N/A$ Curb Opening Veir Equation $R_{Curb} = N/A$ Grated Inlet Performance Reduction Factor for Long Inlets $R_{Curb} = N/A$ Curb Opening Combination Inlet Performance Reduction Factor for Long Inlets $R_{Curb} = N/A$ Curb Opening Combination Inlet Interception Capacity (assumes clogged condition) $R_{Curb} = 0.33$ Curb Opening Combination Capacity (assumes clogged condition) $R_{Curb} = 0.64$,	1	
Length of a Unit Curb OpeningLoSince<		00 (0) -	,	1	
Height of Vertical Curb Opening in Inches H_{vert} 6.006.00inchesHeight of Curb Orifice Throat in Inches H_{vert} 6.006.00inchesAngle of ThroatInches H_{throat} 6.006.00inchesSide Width for Depression Pan (typically the gutter width of 2 feet) W_p 2.002.00feetClogging Factor for a Single Curb Opening (typical value 0.10) C_r (C)0.100.10feetCurb Opening Weir Coefficient (typical value 2.3-3.7) C_w (C)3.603.603.60Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_o (C)0.670.670.67Low Head Performance Reduction (Calculated)MINORMAJORftDepth for Grate Midwidth d_{crate} N/AN/AftCurb Opening Veir EquationRF _{Grate} N/AN/AftCurb Opening Performance Reduction Factor for Long InletsRF _{Grate} N/AN/ACurb Opening Performance Reduction Factor for Long InletsRF _{combination} N/AN/ACurb Opening Combination Inlet Performance Reduction Factor for Long InletsRF _{combination} N/AN/ACurb Opening Combination Inlet Reformance Reduction Factor for Long InletsRF _{combination} N/AN/ATotal Inlet Interception Capacity (assumes clogged condition) $Q_a = $ 5.45.4cfs		L (C) =			feet
Height of Curb Orifice Throat in Inches H_{throat} 6.006.00inchesAngle of ThroatG3.40G3.40degreesSide Width for Depression Pan (typically the gutter width of 2 feet) $W_p = 2.00$ 2.00feetClogging Factor for a Single Curb Opening (typical value 0.10) C_r (C) =0.100.10feetCurb Opening Weir Coefficient (typical value 2.3-3.7) C_w (C) =3.603.60feetCurb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_o (C) =0.570.67Low Head Performance Reduction (Calculated)MINOR M_{curb} =N/AN/ADepth for Grate Midwidth d_{curb} =N/AN/AftDepth for Curb Opening Weir Equation d_{curb} =N/AN/AftGrated Inlet Performance Reduction Factor for Long Inlets RF_{Grate} =N/AN/ACurb Opening Performance Reduction Factor for Long Inlets RF_{Curb} =N/AN/ACombination Inlet Performance Reduction Factor for Long Inlets RF_{Curb} =N/AN/ACorb Inlet Interception Capacity (assumes clogged condition) $Q_a = $ 5.4 5.4 $6fs$					
Angle of ThroatTheta = 63.40 63.40 degreesSide Width for Depression Pan (typically the gutter width of 2 feet)Theta = 63.40 63.40 degreesClogging Factor for a Single Curb Opening (typical value 0.10) C_r (C) = 2.00 2.00 feetCurb Opening Weir Coefficient (typical value 0.60 - 0.70) C_r (C) = 3.60 3.60 C_o (C) =Low Head Performance Reduction (Calculated) $MiNOR$ $MajOR$ d_{Grate} N/A N/A Depth for Carb Opening Weir Equation Grated Inlet Performance Reduction Factor for Long Inlets RF_{Grate} N/A N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{Curb} N/A N/A N/A Curb Opening Veir Equation Grate of Long Inlets RF_{Curb} N/A N/A N/A Curb Opening Veir Formance Reduction Factor for Long Inlets RF_{Curb} N/A N/A Curb Opening Veir Grate Neduction Factor for Long Inlets RF_{Curb} N/A N/A Curb Opening Veir Formance Reduction Factor for Long Inlets RF_{Curb} N/A N/A Curb Opening Veir Grate Inlet Interception Capacity (assumes clogged condition) Q_n 5.4 5.4 5.4					
Side Width for Depression Pan (typically the gutter width of 2 feet) $W_p =$ 2.00 2.00 Clogging Factor for a Single Curb Opening (typical value 0.10) $C_r (C) =$ 0.10 0.10 Curb Opening Weir Coefficient (typical value 0.60 - 0.70) $C_w (C) =$ 3.60 3.60 Low Head Performance Reduction (Calculated)MINORMAJORDepth for Grate Midwidth $d_{Grate} =$ N/A N/A Depth for Grate Midwidth $d_{Grate} =$ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $RF_{Grate} =$ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} =$ 1.00 1.00 Curb Opening Veriformance Reduction Factor for Long Inlets $RF_{Curb} =$ N/A N/A Curb Opening Veriformance Reduction Factor for Long Inlets $RF_{Curb} =$ N/A N/A Curb Opening Veriformance Reduction Factor for Long Inlets $RF_{Curb} =$ N/A N/A Curb Opening Veriformance Reduction Factor for Long Inlets $RF_{Curb} =$ N/A N/A Curb Opening Veriformance Reduction Factor for Long Inlets $RF_{Curb} =$ N/A N/A Curb Opening Veriformance Reduction Factor for Long Inlets $RF_{Curb} =$ N/A N/A Curb Opening Veriformance Reduction Factor for Long Inlets $RF_{Curb} =$ $R_{Curb} =$ N/A N/A Curb Opening Veriformance Reduction Factor for Long Inlets $RF_{Curb} =$ R/A N/A R/A Curb Opening Veriformance Reduction Factor for Long Inlets RF_{C	- 5				
Clogging Factor for a Single Curb Opening (typical value 0.10) C_r (C) = 0.10 0.10 Curb Opening Weir Coefficient (typical value 2.3-3.7) C_w (C) = 3.60 3.60 Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_o (C) = 0.67 0.67 Low Head Performance Reduction (Calculated) MINOR MAJOR Depth for Grate Midwidth d_{Curb} = 0.33 0.33 Curb Opening Weir Equation d_{Curb} = N/A N/A Grated Inlet Performance Reduction Factor for Long Inlets RF _{Grate} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF _{combination} = N/A N/A Total Inlet Interception Capacity (assumes clogged condition) Qa = 5.4 5.4 64	5				
Curb Opening Weir Coefficient (typical value 2.3-3.7) $C_w (C) = 3.60$ 3.60 Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) $C_w (C) = 3.60$ 3.60 Low Head Performance Reduction (Calculated) $MINOR$ MAIOR Depth for Grate Midwidth $d_{Grate} = N/A$ N/A Depth for Curb Opening Weir Equation $d_{Grate} = N/A$ N/A Grated Inlet Performance Reduction Factor for Long Inlets $RF_{Grate} = N/A$ N/A Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} = 1.00$ 1.00 Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} = 1.00$ 1.00 Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} = 1.00$ 1.00 Curb Opening Veir Equation $RF_{Curb} = 3.60$ R_{A} N/A Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} = 1.00$ 1.00 1.00 Combination Inlet Performance Reduction Factor for Long Inlets $RF_{Curb} = 3.4$ $S.4$					
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_o^2 (C) = 0.67 Low Head Performance Reduction (Calculated) MINOR Depth for Grate Midwidth $d_{Grate} = N/A N/A$ Depth for Curb Opening Weir Equation $d_{Curb} = 0.33$ Grated Inlet Performance Reduction Factor for Long Inlets RF _{Grate} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF _{Grate} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF _{Curb} = 1.00 Combination Inlet Performance Reduction Factor for Long Inlets RF _{Combination} = N/A N/A Total Inlet Interception Capacity (assumes clogged condition) Q _a = <u>5.4</u> <u>5.4</u> <u>6.4</u>					
Low Head Performance Reduction (Calculated) MINOR MAJOR Depth for Grate Midwidth $d_{Grate} = N/A$ N/A N/A ft Depth for Curb Opening Weir Equation $d_{Curb} = 0.33$ 0.33 ft Grated Inlet Performance Reduction Factor for Long Inlets RF _{Grate} = N/A N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF _{Curb} = 1.00 1.00 1.00 Combination Inlet Performance Reduction Factor for Long Inlets RF _{Combination} = N/A N/A N/A Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 5.4$ 5.4 5.4 cfs					-
Depth for Grate Midwidth $d_{Grate} =$ N/A N/A ft Depth for Curb Opening Weir Equation $d_{Curb} =$ 0.33 0.33 ft Grated Inlet Performance Reduction Factor for Long Inlets RF _{Grate} = N/A N/A ft Curb Opening Performance Reduction Factor for Long Inlets RF _{Curb} = 1.00 1.00 ft Combination Inlet Performance Reduction Factor for Long Inlets RF _{Combination} = N/A N/A Total Inlet Interception Capacity (assumes clogged condition) Qa = 5.4 5.4 cfs		-0(-)			
Depth for Curb Opening Weir Equation $d_{Curb} =$ 0.33 0.33 ft Grated Inlet Performance Reduction Factor for Long Inlets $RF_{Grate} =$ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} =$ 1.00 1.00 Combination Inlet Performance Reduction Factor for Long Inlets $RF_{Curb} =$ N/A N/A Total Inlet Interception Capacity (assumes clogged condition) $Q_n =$ 5.4 5.4 cfs	Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Grated Inlet Performance Reduction Factor for Long Inlets $RF_{Grate}^{Grate} = $ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} = $ 1.00 1.00 Combination Inlet Performance Reduction Factor for Long Inlets $RF_{Curb} = $ N/A N/A Total Inlet Interception Capacity (assumes clogged condition) $Q_a = $ 5.4 5.4 cfs	Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} = 1.00$ 1.00 Combination Inlet Performance Reduction Factor for Long Inlets $RF_{Curb} = N/A$ N/A Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 5.4$ 5.4 cfs	Depth for Curb Opening Weir Equation	d _{curb} =	0.33	0.33	ft
Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} = 1.00$ 1.00 Combination Inlet Performance Reduction Factor for Long Inlets $RF_{Curb} = N/A$ N/A Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 5.4$ 5.4 cfs	Grated Inlet Performance Reduction Factor for Long Inlets		N/A	N/A	
Combination Inlet Performance Reduction Factor for Long Inlets RF _{Combination} = N/A N/A MINOR MAJOR Total Inlet Interception Capacity (assumes clogged condition) Qa = 5.4 5.4 cfs	Curb Opening Performance Reduction Factor for Long Inlets		1.00	1.00	
Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 5.4$ 5.4 cfs	Combination Inlet Performance Reduction Factor for Long Inlets		N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 5.4 5.4$ cfs		2.5mbinddon		•	-
			MINOR	MAJOR	
Inlet Capacity IS GOOD for Minor and Major Storms (>O Peak) Q PEAK REQUIRED = 0.7 1.3 Cfs	Total Inlet Interception Capacity (assumes clogged condition)	Q _a =			cfs
	Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	Q PEAK REQUIRED =	0.7	1.3	cfs



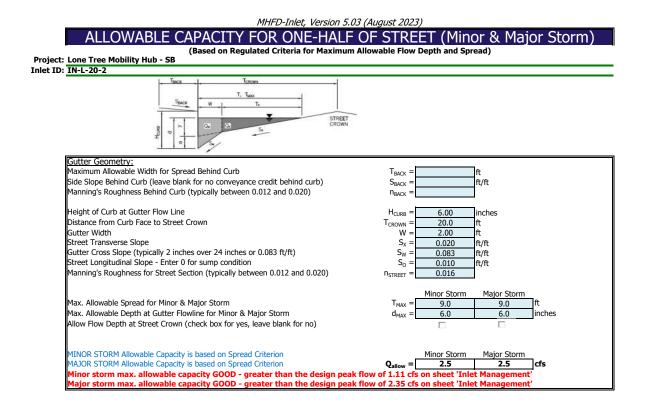


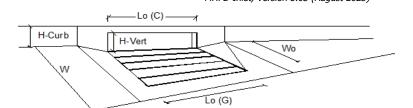
Design Information (Input) CDOT Type R Curb Opening	•	MINOR	MAJOR	1
Type of Inlet	Type =	СБОТ Туре К	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.0	1.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_{b} =$	0.0	0.1	cfs
Capture Percentage = Q_a/Q_o	C% =	100	93	%



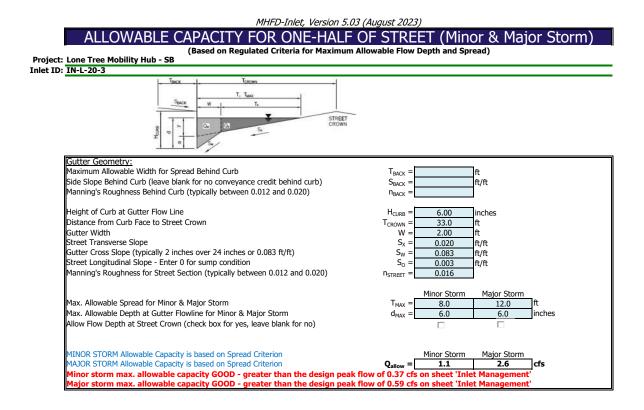


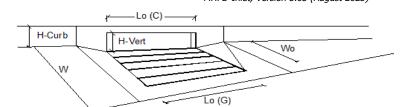
Design Information (Input)	1	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.6	1.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.0	cfs
Capture Percentage = Q_a/Q_o	C% =	100	100	%



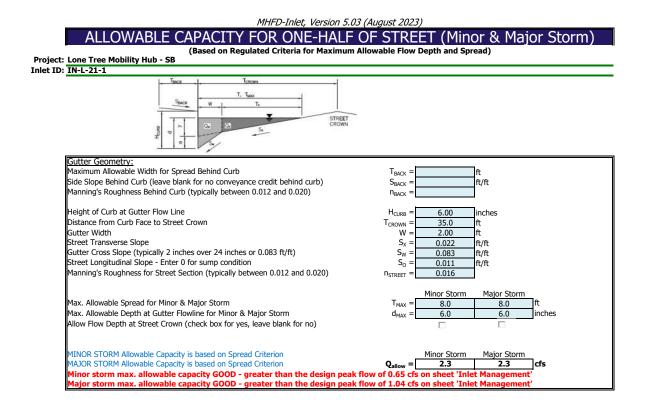


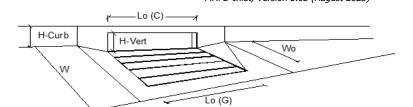
Design Information (Input)	1	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.1	2.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.0	cfs
Capture Percentage = Q_a/Q_o	C% =	100	100	%



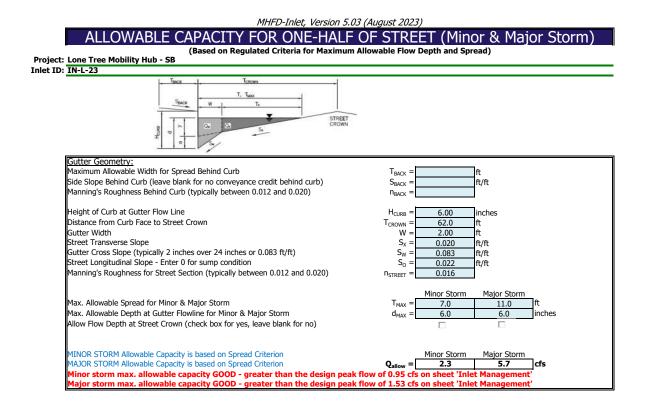


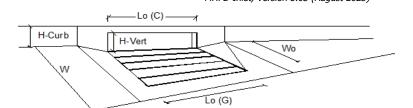
Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.4	0.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.0	cfs
Capture Percentage = Q_a/Q_o	C% =	100	100	%



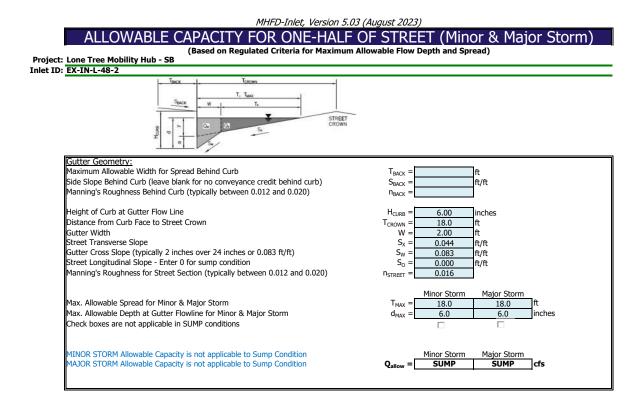


Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.7	1.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.0	cfs
Capture Percentage = Q_a/Q_o	C% =	100	100	%

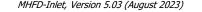


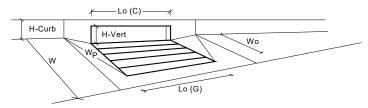


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.0	1.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q_a/Q_o	C% =	100	100	%

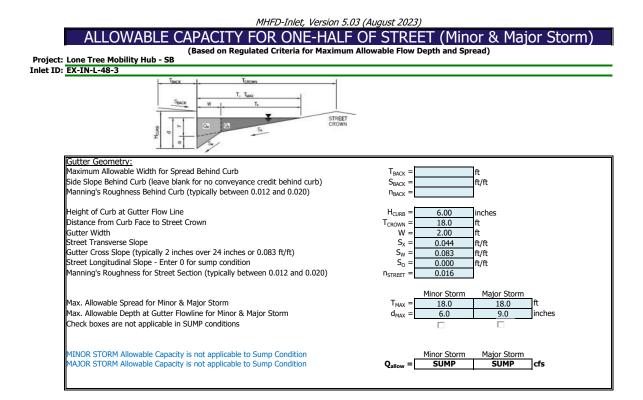


INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.03 (August 2023)

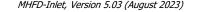


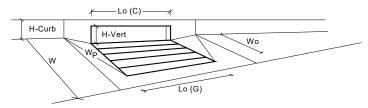


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R		1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	6.0	inches
Grate Information	· •······	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W ₀ =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_{w}(G) =$	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{o}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.33	0.33	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	-
	Combination	,	,	_
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	5.4	5.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{PEAK REQUIRED} =$	1.2	2.0	cfs



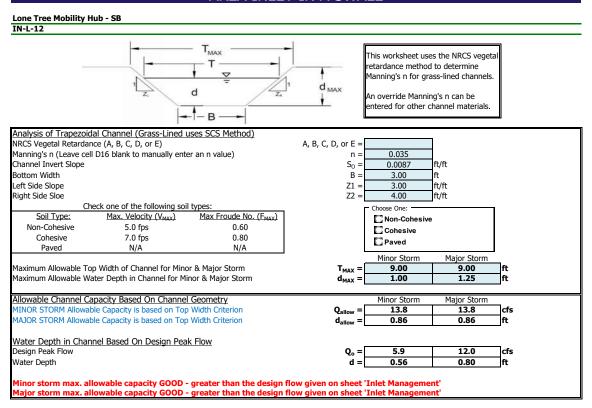
INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.03 (August 2023)





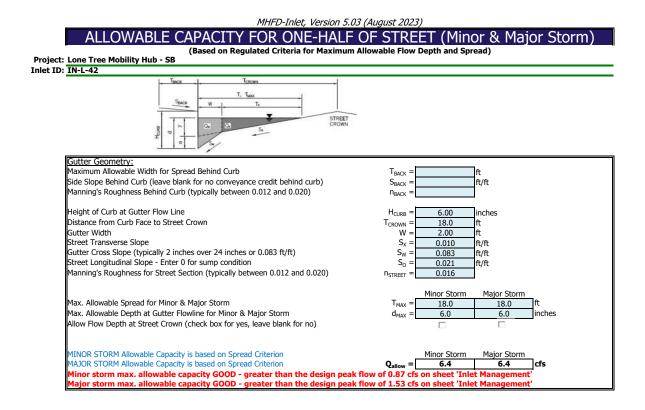
Clogging Factor for a Single Curb Opening (typical value 0.10) C_r (C) = N/A N/A Curb Opening Weir Coefficient (typical value 2.3-3.7) C_w (C) = N/A N/A Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_o (C) = N/A N/A Low Head Performance Reduction (Calculated) $MINOR$ $MJOR$ Depth for Grate Midwidth d_{Carbe} = 0.52 0.77 Grated Inlet Performance Reduction Factor for Long Inlets RF_{Carbe} = 0.94 1.00 Curb Opening Performance Reduction Factor for Long Inlets RF_{Carbe} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{Carbe} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{Carbe} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{Carbe} = N/A N/A Total Inlet Interception Capacity (assumes clogged condition) Q_a = 2.6 4.6 Cfs					
Local Depression (additional to continuous gutter depression 'a' from above) $a_{local} = 2.00$ 2.00inchesNumber of Unit Inlets (Grate or Curb Opening)No =11Water Depth at Flowline (outside of local depression)Ponding Depth =6.09.0inchesGrate InformationLo (G) =3.003.00feetLength of a Unit Grate V_0 = 1.73 1.73 1.73 Open Area Ratio for a Grate (typical value 0.50 - 0.70) A_{rabic} 0.43 0.43 Clogging Factor for a Single Grate (typical value 0.50 - 0.70) C_0 (G) = 0.60 0.60 Grate Orfficient (typical value 0.60 - 0.80) C_0 (G) = 0.60 0.60 Curb Opening Information $MiNOR$ MAIORMAIORLeight of Vertical Curb Opening in Inches H_{thorat} N/A N/A Angle of Throat N/A N/A N/A N/A Side Width for Depression Pan (typically the gutter width of 2 feet) W_0 N/A N/A Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_0 (C) = N/A N/A Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_0 (C) = N/A N/A Low Head Performance Reduction Factor for Long Inlets R_{cath} N/A N/A Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_0 (C) = N/A N/A Low Head Performance Reduction Factor for Long Inlets R_{cath} N/A N/A Curb Opening Weir Equation R_{cath} N/A N/A <td></td> <td>- 1</td> <td></td> <td></td> <td>7</td>		- 1			7
Number of Unit Inlets (Grate or Curb Opening)No11Water Depth at Flowline (outside of local depression) Grate Information Length of a Unit GrateNo11Width of a Unit Grate Width of a Unit GratePonding Depth =6.09.0inchesWidth of a Unit Grate Open Area Ratio for a Grate (typical value $0.15 - 0.90$) Clogging Factor for a Single Grate (typical value $0.50 - 0.70$) Grate Orifice Coefficient (typical value $2.15 - 3.60$) Grate Orifice Coefficient (typical value $0.50 - 0.80$) Curb Opening Information Length of a Unit Curb Opening Inches Height of Vertical Curb Opening Inches Height of Vertical Curb Opening Inches Angle of Throat Side Width for Depression Pan (typical value 0.10) Curb Opening Veir Coefficient (typical value $0.60 - 0.70$) Curb Opening Weir Coefficient (typical value $0.60 - 0.70$) Curb Opening Weir Coefficient (typical value $0.60 - 0.70$) Curb Opening Weir Coefficient (typical value 0.10) Curb Opening Weir Equation Grate Midwidth Depth for Grate Midwidth Curb Opening Weir Equation Grate for Long InletsMiNOR MAJOR MAJOR Curb Opening Weir Equation Grate for Long InletsMiNOR MAJOR Curb Opening Meir Equation Grate Foromance Reduction Factor for Long InletsMiNOR MAJOR MAJOR MAJORMiNOR MAJOR MAJORTotal Inlet Interception Capacity (assumes clogged condition)Qar = 2.6 4.6 Cfs		71			to also a
Water Depth at Flowline (outside of local depression) Grate Linformation Length of a Unit GratePonding Depth = 6.0 9.0 inchesMINORMAOROverride DepthsWidth of a Unit Grate L_0 (G) = 3.00 3.00 feetWidth of a Unit Grate W_0 = 1.73 1.73 feetOpen Area Ratio for a Grate (typical value 0.50 - 0.70) Grate Weir Coefficient (typical value 0.50 - 0.70) Grate Weir Coefficient (typical value 0.60 - 0.80) Curb Opening Information Length of a Unit Curb Opening C_0 (G) = 0.60 0.60 Length of a Unit Curb Opening Height of Vertical Curb Opening Information Length of a Unit Curb Opening Information Length of a Unit Curb Opening Information Length of a Unit Curb Opening (typical value 2.13 - 3.7) Curb Opening Weir Coefficient (typical value 2.13 - 7.7) Curb Opening Weir Coefficient (typical value 0.60 - 0.70) L_0 (C) = N/A N/A Side Width for Depression Pan (typical value 0.10) Curb Opening Weir Coefficient (typical value 0.10) Curb Opening Weir Coefficient (typical value 0.10) Curb Opening Weir Coefficient (typical value 0.60 - 0.70) $MINOR$ $MINOR$ $MINOR$ Low Head Performance Reduction Factor for Long Inlets Combination Inlet Performance Reduction Factor for Long Inlets RF_{Conte} N/A N/A N/A Chall Depth for Curb Opening Weir Capacity (assumes clogged condition) Q_a = 2.6 4.6 C_a				2.00	inches
Grate InformationMINORMAJOROverride DepthsLength of a Unit Grate V_0 (G) = 3.00 3.00 feetWidth of a Unit Grate V_0 = 1.73 1.73 1.73 Cogging Factor for a Single Grate (typical value 0.50 - 0.70) C_r (G) = 0.50 0.50 Grate Orfice Coefficient (typical value 2.15 - 3.60) C_w (G) = 3.30 3.30 Grate Orfice Coefficient (typical value 0.60 - 0.80) C_v (G) = 0.60 0.60 Curb Opening Information V_0 (G) = N/A N/A N/A Length of a Unit Curb OpeningInches H_{eff} N/A N/A N/A Height of Vertical Curb Opening in Inches H_{wroat} N/A N/A N/A Angle of ThroatSide Width for Depression Pan (typical value 0.10) C_r (C) = N/A N/A Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_v (C) = N/A N/A Curb Opening Orifice Coefficient (typical value 0.10) C_r (C) = N/A N/A Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_v (C) = N/A N/A Low Head Performance Reduction Factor for Long Inlets R_{Garde} 0.52 0.77 Curb Opening Weir Equation R_{Garde} 0.94 1.00 Grate Inlet Performance Reduction Factor for Long Inlets $R_{F_{Garde}}$ N/A N/A Curb Opening Weir Equation $R_{Curbination}$ N/A N/A N/A Curb Opening Weir Equation $R_{F_{Garde}}$ N/A <			-	1	
Length of a Unit GrateLo $(G) =$ 3.003.00feetWidth of a Unit GrateWo =1.731.73feetOpen Area Ratio for a Grate (typical value 0.50 - 0.70) C_r (G) =0.430.43Clogging Factor for a Single Grate (typical value 0.50 - 0.70) C_r (G) =0.500.50Grate Weir Coefficient (typical value 2.15 - 3.60) C_r (G) =0.600.60Curb Opening InformationMINORMAJORLength of a Unit Curb OpeningInches $H_{vert} =$ N/AN/AHeight of Vertical Curb Opening in Inches $H_{vert} =$ N/AN/AHeight of Curb Orifice Throat in Inches $H_{vert} =$ N/AN/ASide Width for Depression Pan (typical value 0.10) C_r (C) =N/AN/ACurb Opening Weir Coefficient (typical value 0.10) C_r (C) =N/AN/ACurb Opening Weir Coefficient (typical value 0.60 - 0.70) C_r (C) =N/AN/ACurb Opening Weir Coefficient (typical value 0.60 - 0.70) C_r (C) =N/AN/ACurb Opening Weir Coefficient (typical value 0.60 - 0.70) C_r (C) =N/AN/ALow Head Performance Reduction Factor for Long Inlets $R_{Forste} =$ 0.520.77ftCurb Opening Weir Equation $R_r =$ 0.941.00N/AN/ADepth for Grate Midwidth $R_{Forste} =$ 0.941.00N/AN/ADepth for Grate Midwidth $R_r =$ N/A N/AN/AN/ACurb Opening Weir EquationReforet =		Ponding Depth =			
Width of a Unit Grate $W_o =$ 1.73 1.73 feetOpen Area Ratio for a Grate (typical values 0.15-0.90) C_{r} (G) 0.43 0.43 0.43 Clogging Factor for a Single Grate (typical value 0.50 - 0.70) C_r (G) 0.50 0.50 Grate Orifice Coefficient (typical value 0.60 - 0.80) C_{w} (G) 0.60 0.60 Curb Opening Information C_o (G) 0.60 0.60 Length of a Unit Curb Opening in Inches H_{eff} N/A N/A Height of Curb Orifice Throat in Inches H_{throat} N/A N/A Angle of ThroatSide Width for Depression Pan (typical value 0.10) C_r (C) N/A N/A Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_r (C) N/A N/A Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_r (C) N/A N/A Low Head Performance Reduction Factor for Long Inlets $RF_{Grate} =$ 0.52 0.777 Curb Opening Weir Equation $RF_{Grate} =$ 0.94 1.00 Grated Inlet Performance Reduction Factor for Long Inlets $RF_{Grate} =$ N/A N/A Curb Opening Veir Equation Factor for Long Inlets $RF_{Grate} =$ N/A N/A Combination Inlet Performance Reduction Factor for Long Inlets $RF_{Grate} =$ N/A N/A Curb Opening Veir Capacity (assumes clogged condition) $Q_a =$ 2.6 4.6 Cfs					
Open Area Ratio for a Grate (typical values 0.15-0.90) $A_{ratio} =$ 0.43 0.43 Clogging Factor for a Single Grate (typical value 0.50 - 0.70) $G_r (G) =$ 0.50 0.50 Grate Weir Coefficient (typical value 2.15 - 3.60) $G_v (G) =$ 3.30 3.30 Grate Orifice Coefficient (typical value 0.60 - 0.80) $C_v (G) =$ 0.60 0.60 Curb Opening Information $MINOR$ MAJORLength of a Unit Curb Opening in Inches $H_{vert} =$ N/A N/A Height of Curb Orifice Throat in Inches $H_{treat} =$ N/A N/A Angle of ThroatSide Width for Depression Pan (typical value 0.10) $V_P =$ N/A N/A Curb Opening Weir Coefficient (typical value 0.50 - 0.70) $C_v (C) =$ N/A N/A Curb Opening Weir Coefficient (typical value 0.60 - 0.70) $C_v (C) =$ N/A N/A Low Head Performance Reduction (Calculated) $MINOR$ $MAJOR$ Depth for Grate Midwidth $C_{oth} =$ N/A N/A N/A Depth for Grate Midwidth $R_{carbe} =$ N/A N/A N/A Curb Opening Weir Equation $R_{carbe} =$ N/A N/A N/A Curb Opening Weir Equation $R_{carbe} =$ N/A N/A N/A Curb Opening Weir Equation $R_{carbe} =$ N/A N/A N/A Curb Opening Weir Coefficient (typical value 0.60 - 0.70) $C_o (C) =$ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $R_{carbe} =$ 0.52 0.77	- 5				
Clogging Factor for a Single Grate (typical value 0.50 - 0.70) $C_r (G) =$ 0.50 0.50 Grate Weir Coefficient (typical value 2.15 - 3.60) $C_w (G) =$ 3.30 3.30 Grate Orifice Coefficient (typical value 0.60 - 0.80) $C_o (G) =$ 0.60 0.60 Curb Opening Information $L_o (C) =$ N/A N/A Length of a Unit Curb Opening N/A N/A N/A Height of Vertical Curb Opening in Inches $H_{vert} =$ N/A N/A Angle of Throat N/A N/A N/A Side Width for Depression Pan (typical value 0.10) $C_r (C) =$ N/A N/A Curb Opening Weir Coefficient (typical value 0.3.7) $C_w (C) =$ N/A N/A Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) $C_o (C) =$ N/A N/A Low Head Performance Reduction Factor for Long Inlets $R_{Carbe} =$ 0.94 1.00 Curb Opening Performance Reduction Factor for Long Inlets $R_{Carbe} =$ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $R_{Carbe} =$ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $R_{Carbe} =$ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $R_{Carbe} =$ N/A N/A Curb Opening Veir Equation $R_{Carbe} =$ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $R_{Carbe} =$ N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $R_{Carbe} =$ N/A <td></td> <td>° .</td> <td>-</td> <td>-</td> <td>feet</td>		° .	-	-	feet
Grate Weir Coefficient (typical value 2.15 - 3.60) C_w (G) = 3.30 3.30 Grate Orifice Coefficient (typical value 0.60 - 0.80) C_o (G) = 0.60 0.60 Curb Opening InformationLength of a Unit Curb OpeningMINORMAJORLength of a Unit Curb Opening in Inches H_{vert} = N/A N/A inchesHeight of Curb Orifice Throat in Inches H_{vert} = N/A N/A inchesAngle of ThroatSide Width for Depression Pan (typical value 0.10) C_r (C) = N/A N/A degreesClogging Factor for a Single Curb Opening (typical value 0.10) C_r (C) = N/A N/A feetCurb Opening Weir Coefficient (typical value 0.60 - 0.70) C_r (C) = N/A N/A N/A Low Head Performance Reduction (Calculated)MINOR $MAJOR$ C_{curb} = N/A N/A Depth for Grate Midwidth C_{curb} = N/A N/A N/A N/A Curb Opening Veir EquationGrated Inlet Performance Reduction Factor for Long Inlets RF_{carbe} = 0.94 1.00 Curb Opening Performance Reduction Factor for Long Inlets $RF_{Combination}$ = N/A N/A N/A Total Inlet Interception Capacity (assumes clogged condition) Q_a = 2.6 4.6 Cfs					
Grate Orifice Coefficient (typical value 0.60 - 0.60) C_o (G) = 0.60 0.60 Curb Opening InformationLength of a Unit Curb Opening in InchesMINORMAJORHeight of Vertical Curb Opening in Inches N/A N/A N/A inchesHeight of Curb Orifice Throat in Inches N/A N/A N/A inchesAngle of ThroatSide Width for Depression Pan (typical value 0.10) C_c (C) = N/A N/A N/A Curb Opening Orifice Coefficient (typical value 0.3.7) C_c (C) = N/A N/A feetCurb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_c (C) = N/A N/A feetLow Head Performance Reduction (Calculated) $MINOR$ $MAJOR$ C_{curb} = N/A N/A ftDepth for Grate Midwidth C_{curb} = N/A N/A N/A ftftCurb Opening Veir Equation G_{curb} = N/A N/A N/A ftGrated Inlet Performance Reduction Factor for Long Inlets RF_{curb} = N/A N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{curb} = N/A N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{curb} = N/A N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{curb} = N/A N/A N/A Curb Opening Company Reduction Factor for Long Inlets RF_{curb} = N/A N/A N/A Combination Inlet Performance Reduction Facto					
MINOR MAJOR Length of a Unit Curb Opening Inches Height of Vertical Curb Opening in Inches H_{eff} Height of Curb Orifice Throat in Inches H_{rett} Angle of Throat N/A Side Width for Depression Pan (typically the gutter width of 2 feet) W_p Curb Opening Weir Coefficient (typical value 0.10) C_r (C) Curb Opening Weir Coefficient (typical value 0.50 - 0.70) W_p Low Head Performance Reduction (Calculated) MINOR Depth for Grate Midwidth d_{carb} Grated Inlet Performance Reduction Factor for Long Inlets RF_{Carb} Curb Opening Veir Coefficient for Long Inlets RF_{Carb} Curb Opening Weir Coefficient for Long Inlets RF_{Carb} Depth for Grate Midwidth d_{carb} Depth for Grate Reduction Factor for Long Inlets RF_{Carb} Curb Opening Verir Could for Long Inlets RF_{Carb} Curb Opening Verir Could (assumes clogged condition) Q_a					
Length of a Unit Curb OpeningLoN/AN/AFeetHeight of Vertical Curb Opening in Inches $H_{vert} = N/A$ N/A N/A inchesHeight of Curb Orifice Throat in Inches $H_{vert} = N/A$ N/A N/A inchesSide Width for Depression Pan (typically the gutter width of 2 feet) $H_{vert} = N/A$ N/A N/A inchesClogging Factor for a Single Curb Opening (typical value 0.10) $C_f(C) = N/A$ N/A N/A feetCurb Opening Weir Coefficient (typical value 0.30 - 0.70) $C_o(C) = N/A$ N/A N/A feetLow Head Performance Reduction (Calculated)MINOR $MAJOR$ N/A N/A Depth for Grate Midwidth $d_{curb} = 0.52$ 0.77 ftCurb Opening Performance Reduction Factor for Long Inlets $RF_{carb} = 0.94$ 1.00 Curb Opening Performance Reduction Factor for Long Inlets $RF_{curb} = N/A$ N/A N/A Curb Opening Carbor Inlet Performance Reduction Factor for Long Inlets $RF_{curb} = N/A$ N/A N/A Curb Opening Carbor Carbor (alcond for Long Inlets $RF_{curb} = N/A$ N/A N/A Curb Opening Carbor Carbor for Long Inlets $RF_{curb} = N/A$ N/A N/A Curb Opening Carbor Carbor (assumes clogged condition) $R_{a} = 2.6$ 4.6 C_{a}		$C_o(G) =$		0.60	
Height of Vertical Curb Opening in Inches H_{vert} N/A N/A N/A inches Height of Curb Orifice Throat in Inches H_{vert} N/A N/A N/A inches Angle of Throat N/A N/A N/A N/A N/A inches Side Width for Depression Pan (typically the gutter width of 2 feet) W_p N/A N/A N/A degrees Clogging Factor for a Single Curb Opening (typical value 0.10) C_r (C) N/A N/A N/A Curb Opening Weir Coefficient (typical value 0.60 - 0.70) C_r (C) N/A N/A N/A Low Head Performance Reduction (Calculated) $MINOR$ MAJOR N/A N/A Depth for Grate Midwidth d_{crate} 0.92 0.94 1.00 Curb Opening Veir Equation R_{crate} N/A N/A N/A Curb Opening Performance Reduction Factor for Long Inlets R_{crate} N/A N/A N/A Curb Opening Performance Reduction Factor for Long Inlets R_{crate} N/A N/A N/A Curb Opening Performance Reduction Factor for Long Inlets </td <td></td> <td>_</td> <td></td> <td>MAJOR</td> <td>_</td>		_		MAJOR	_
Height of Curb Orifice Throat in Inches H_{thotal} N/A N/A N/A N/A N/A M_{rhoat} Angle of Throat Side Width for Depression Pan (typically the gutter width of 2 feet) N/A N/A N/A N/A M/A <		$L_{o}(C) =$		1	
Angle of ThroatTheta = N/A N/A degreesSide Width for Depression Pan (typically the gutter width of 2 feet)Theta = N/A N/A feetClogging Factor for a Single Curb Opening (typical value 0.10) C_r (C) = N/A N/A feetCurb Opening Weir Coefficient (typical value 2.3-3.7) C_w (C) = N/A N/A N/A Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_o (C) = N/A N/A N/A Low Head Performance Reduction (Calculated) $MINOR$ $MAJOR$ $MJOR$ Depth for Grate Midwidth d_{Grate} = 0.52 0.77 ftGrated Inlet Performance Reduction Factor for Long Inlets RF_{Grate} = 0.94 1.00 Curb Opening Performance Reduction Factor for Long Inlets RF_{Curb} = N/A N/A Curb Opening Corporance Reduction Factor for Long Inlets RF_{Curb} = N/A N/A Curb Opening Corporance Reduction Factor for Long Inlets RF_{Curb} = N/A N/A Curb Opening Corporance Reduction Factor for Long Inlets RF_{Curb} = N/A N/A Curb Opening Corporance Reduction Factor for Long Inlets RF_{Curb} = N/A N/A Curb Opening Corporance Reduction Factor for Long Inlets RF_{Curb} = N/A N/A Curb Opening Corporance Reduction Factor for Long Inlets RF_{Curb} = N/A N/A Curb Opening Corporation Capacity (assumes clogged condition) Q_a = 2.6 4.6 Cf		H _{vert} =	,	N/A	inches
Side Width for Depression Pan (typically the gutter width of 2 feet) $W_p = \frac{N/A}{N/A}$ N/A N/A Clogging Factor for a Single Curb Opening (typical value 0.10) $C_r (C) = N/A$ N/A N/A Curb Opening Weir Coefficient (typical value 0.50 - 0.70) $C_o (C) = N/A$ N/A N/A Low Head Performance Reduction (Calculated) $MINOR$ MAJOR Depth for Grate Midwidth $d_{Grate} = 0.52$ 0.77 ft Grated Inlet Performance Reduction Factor for Long Inlets $RF_{Grate} = 0.94$ 1.00 Curb Opening Performance Reduction Factor for Long Inlets $RF_{Grate} = 0.94$ 1.00 Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 2.6$ 4.6 Cf_s	- 5	H _{throat} =	,	N/A	inches
Clogging Factor for a Single Curb Opening (typical value 0.10) C_r (C) = N/A N/A Curb Opening Weir Coefficient (typical value 2.3-3.7) C_w (C) = N/A N/A Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_o (C) = N/A N/A Low Head Performance Reduction (Calculated) $MINOR$ $MJOR$ Depth for Grate Midwidth d_{Carbe} = 0.52 0.77 Grated Inlet Performance Reduction Factor for Long Inlets RF_{Carbe} = 0.94 1.00 Curb Opening Performance Reduction Factor for Long Inlets RF_{Carbe} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{Carbe} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{Carbe} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{Carbe} = N/A N/A Total Inlet Interception Capacity (assumes clogged condition) Q_a = 2.6 4.6 Cfs	Angle of Throat	Theta =	N/A	N/A	degrees
Curb Opening Weir Coefficient (typical value 2.3-3.7) C_w (C) = N/A N/A Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) C_o (C) = N/A N/A Low Head Performance Reduction (Calculated) $MINOR$ $MJOR$ Depth for Grate Midwidth d_{carbe} = 0.52 0.77 Grated Inlet Performance Reduction Factor for Long Inlets RF_{Grate} = 0.94 1.00 Curb Opening Performance Reduction Factor for Long Inlets RF_{Carb} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{Carb} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets RF_{Carb} = N/A N/A Curb Opening Performance Reduction Factor for Long Inlets $RF_{combination}$ = N/A N/A Combination Inlet Performance Reduction Factor for Long Inlets $RF_{combination}$ = N/A N/A Total Inlet Interception Capacity (assumes clogged condition) Q_a = 2.6 4.6 Cfs	Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	N/A	N/A	feet
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70) $C_o^{-}(C) = N/A N/A$ Low Head Performance Reduction (Calculated) MINOR MAJOR Depth for Grate Midwidth $d_{Grate} = 0.52 0.77$ Depth for Curb Opening Weir Equation $N/A N/A$ Grated Inlet Performance Reduction Factor for Long Inlets $RF_{Grate} = 0.94 1.00$ Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} = N/A N/A$ Combination Inlet Performance Reduction Factor for Long Inlets $RF_{Curb} = N/A N/A$ Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 2.6 4.6$	Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	N/A	N/A	
Low Head Performance Reduction (Calculated) MINOR MAJOR Depth for Grate Midwidth $d_{Grate} = 0.52$ 0.77 ft Depth for Curb Opening Weir Equation $d_{Curb} = N/A$ N/A N/A Grated Inlet Performance Reduction Factor for Long Inlets RF _{Grate} = 0.94 1.00 Curb Opening Performance Reduction Factor for Long Inlets RF _{Grate} = N/A N/A Combination Inlet Performance Reduction Factor for Long Inlets RF _{Grate} = N/A N/A Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 2.6$ 4.6 cfs		$C_w(C) =$		N/A	
Depth for Grate Midwidth $d_{Grate} =$ 0.52 0.77 ft Depth for Curb Opening Weir Equation $d_{Curb} =$ N/A N/A ft Grated Inlet Performance Reduction Factor for Long Inlets RF _{Grate} = 0.94 1.00 Curb Opening Performance Reduction Factor for Long Inlets RF _{curb} = N/A N/A Combination Inlet Performance Reduction Factor for Long Inlets RF _{combination} = N/A N/A Total Inlet Interception Capacity (assumes clogged condition) Qa = 2.6 4.6 cfs	Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	N/A	N/A	
Depth for Grate Midwidth $d_{Grate} =$ 0.52 0.77 ft Depth for Curb Opening Weir Equation $d_{Curb} =$ N/A N/A ft Grated Inlet Performance Reduction Factor for Long Inlets RF _{Grate} = 0.94 1.00 Curb Opening Performance Reduction Factor for Long Inlets RF _{curb} = N/A N/A Combination Inlet Performance Reduction Factor for Long Inlets RF _{combination} = N/A N/A Total Inlet Interception Capacity (assumes clogged condition) Qa = 2.6 4.6 cfs		-			-
Depth for Curb Opening Weir Equation $d_{Curb} = \frac{N/A}{N/A}$ N/A N/A Grated Inlet Performance Reduction Factor for Long Inlets $RF_{Grate} = 0.94$ 1.00 Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} = N/A$ N/A Combination Inlet Performance Reduction Factor for Long Inlets $RF_{Curb} = N/A$ N/A Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 2.6$ 4.6 Cfs	Low Head Performance Reduction (Calculated)	_	MINOR	MAJOR	_
Grated Inlet Performance Reduction Factor for Long Inlets $RF_{Grate} =$ 0.94 1.00 Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} =$ N/A N/A Combination Inlet Performance Reduction Factor for Long Inlets $RF_{Curb} =$ N/A N/A Total Inlet Interception Capacity (assumes clogged condition) $Q_a =$ 2.6 4.6 cfs	Depth for Grate Midwidth	d _{Grate} =	0.52	0.77	ft
Grated Inlet Performance Reduction Factor for Long Inlets $RF_{Grate} = 0.94$ 1.00 Curb Opening Performance Reduction Factor for Long Inlets $RF_{Curb} = N/A$ N/A Combination Inlet Performance Reduction Factor for Long Inlets $RF_{Curb} = N/A$ N/A Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 2.6$ 4.6 Cfs	Depth for Curb Opening Weir Equation	d _{Curb} =	N/A	N/A	ft
Combination Inlet Performance Reduction Factor for Long Inlets RF _{Combination} = N/A N/A MINOR MAJOR Total Inlet Interception Capacity (assumes clogged condition) Qa = 2.6 4.6 cfs	Grated Inlet Performance Reduction Factor for Long Inlets		0.94	1.00	
Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 2.6 4.6$ cfs	Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	N/A	N/A]
Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 2.6 4.6$ cfs	Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
Total Inlet Interception Capacity (assumes clogged condition) $Q_a = 2.6 4.6$ cfs		-			_
		_	MINOR	MAJOR	_
Inlet Capacity IS GOOD for Minor and Major Storms (>O Peak) Q PEAK REQUIRED = 2.3 4.0 cfs	Total Inlet Interception Capacity (assumes clogged condition)				
	Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{PEAK REQUIRED} =$	2.3	4.0	cfs

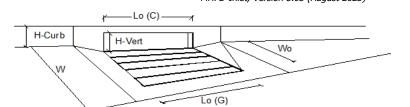
MHFD-Inlet, Version 5.03 (August 2023) AREA INLET IN A SWALE



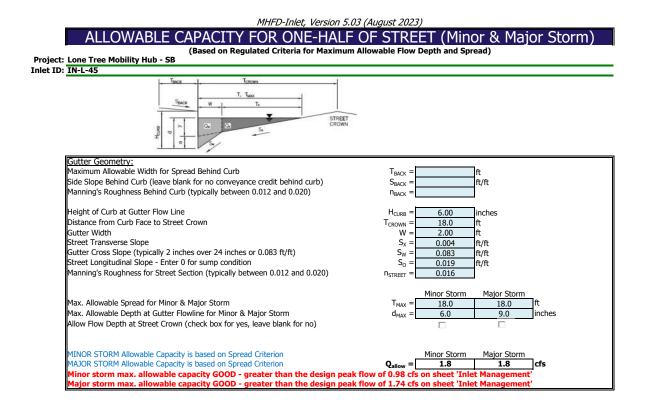
MHFD-Inlet, Version 5.03 (August 2023) AREA INLET IN A SWALE

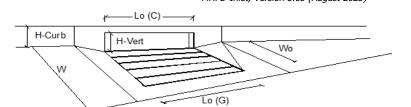
Lone Tree Mobility Hub - SB IN-L-12				
Inlet Design Information (Input) Type of Inlet CDOT Type D (In Series)	Inlet Type =	CDOT Type D	(In Series)	
Angle of Inclined Grate (must be <= 30 degrees) Width of Grate Length of Grate Dpen Area Ratio Height of Inclined Grate Clogging Factor Grate Discharge Coefficient Weir Coefficient Weir Coefficient		$ \begin{array}{c} \theta = \\ W = \\ L = \\ A_{RATIO} = \\ H_B = \\ C_f = \\ C_0 = \\ C_w = \\ \end{array} $	0.00 3.00 6.00 0.70 0.00 0.38 0.78 0.52 1.67	degrees ft ft ft
Water Depth at Inlet (for depressed inlets, 1 foot is added for depression) Fotal Inlet Interception Capacity (assumes clogged condition) Bypassed Flow Capture Percentage = Qa/Qo	d = Q _a = Q _b = C% =	MINOR 0.56 12.4 0.0 100	MAJOR 0.80 21.3 0.0 100	cfs cfs %



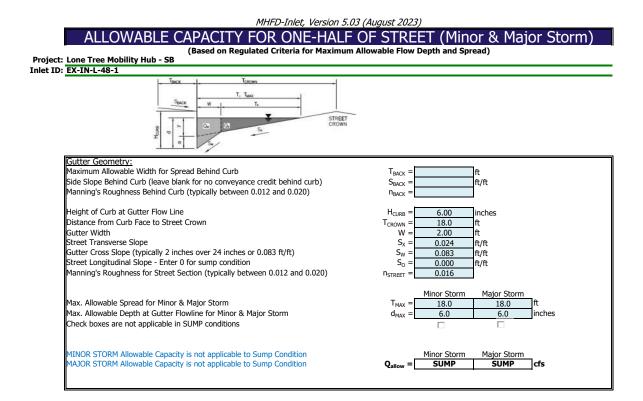


Design Information (Input)	-	MINOR	MAJOR	1
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.9	1.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.1	cfs
Capture Percentage = Q_a/Q_o	C% =	100	93	%

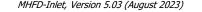


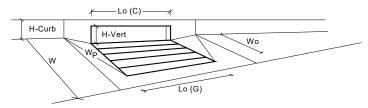


Design Information (Input)	T	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.0	1.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_{b} =$	0.0	0.3	cfs
Capture Percentage = Q_a/Q_o	C% =	100	85	%



INLET IN A SUMP OR SAG LOCATION MHFD-Inlet, Version 5.03 (August 2023)





Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R		1
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	6.0	6.0	inches
Grate Information	· •···································	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{0}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W ₀ =	N/A	N/A	feet
Open Area Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_f(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C_{w} (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{o}(G) =$	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	$L_{o}(C) =$	5.00	5.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	$W_p =$	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Grate} =	0.33	0.33	ft
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	N/A	N/A	
				-
	-	MINOR	MAJOR	-
Total Inlet Interception Capacity (assumes clogged condition)	Qa =	5.4	5.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms (>Q Peak)	$Q_{PEAK REQUIRED} =$	2.0	3.5	cfs

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>EX-IN-L-75</u>	<u>IN-L-76</u>	<u>IN-L-79</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	On Grade	On Grade	On Grade
Inlet Type	Directional Cast Vane Grate	CDOT Type R Curb Opening	CDOT Type R Curb Opening

USER-DEFINED INPUT

User-Defined Design Flows					
Minor Q _{Known} (cfs)	0.8	1.8	3.6		
Major Q _{Known} (cfs)	1.3	2.8	5.9		

Bypass (Carry-Over) Flow from Upstream Inlets must be organized from upstream (left) to downstream (right) in order for bypass flows to be linked.

Receive Bypass Flow from:	No Bypass Flow Received	EX-IN-L-75	IN-L-76
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.1	0.2
Major Bypass Flow Received, Q _b (cfs)	0.0	0.3	0.9

Watershed Characteristics

Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		

Watershed Profile

Overland Slope (ft/ft)					
Overland Length (ft)					
Channel Slope (ft/ft)					
Channel Length (ft)					

Minor Storm Rainfall Input

Design Storm Return Period, Tr (years)			
One-Hour Precipitation, P ₁ (inches)			
One-Hour Precipitation, P_1 (inches)			

Major Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P ₁ (inches)		

Minor Total Design Peak Flow, Q (cfs)	0.8	1.9	3.8
Major Total Design Peak Flow, Q (cfs)	1.3	3.2	6.7
Minor Flow Bypassed Downstream, Q_b (cfs)	0.1	0.2	0.0
Major Flow Bypassed Downstream, Q_b (cfs)	0.3	0.9	0.9

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>IN-L-80</u>	<u>IN-L-83-2</u>	<u>IN-L-83-1</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	On Grade	On Grade	On Grade
Inlet Type	CDOT Type R Curb Opening	CDOT Type R Curb Opening	CDOT Type R Curb Opening

USER-DEFINED INPUT

User-Defined Design Flows					
Minor Q _{Known} (cfs)	0.7	1.0	0.9		
Major Q _{Known} (cfs)	1.1	1.5	1.4		

Bypass (Carry-Over) Flow from Upstream Inlet:

Receive Bypass Flow from:	IN-L-79	IN-L-80	No Bypass Flow Received
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.9	0.2	0.0

Watershed Characteristics

Subcatchment Area (acres)		
Percent Impervious		
NRCS Soil Type		

Watershed Profile

Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		

Minor Storm Rainfall Input

Design Storm Return Period, Tr (years)		
One-Hour Precipitation, P ₁ (inches)		

Major Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P ₁ (inches)		

Minor Total Design Peak Flow, Q (cfs)	0.7	1.0	0.9
Major Total Design Peak Flow, Q (cfs)	2.1	1.7	1.4
Minor Flow Bypassed Downstream, Q_b (cfs)	0.0	0.0	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	0.2	0.1	0.0

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>IN-L-84-1</u>	<u>IN-L-84-2</u>	<u>IN-L-85</u>
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	AREA	STREET
Hydraulic Condition	On Grade	Swale	On Grade
Inlet Type	CDOT Type R Curb Opening	CDOT Type C	CDOT Type R Curb Opening

USER-DEFINED INPUT

User-Defined Design Flows			
Minor Q _{Known} (cfs)	0.7	0.7	0.7
Major Q _{Known} (cfs)	1.1	2.6	1.1

Bypass (Carry-Over) Flow from Upstream Inlets

Receive Bypass Flow from:	IN-L-83-2	No Bypass Flow Received	IN-L-84-1
Minor Bypass Flow Received, Q _b (cfs)	0.0	0.0	0.0
Major Bypass Flow Received, Q _b (cfs)	0.1	0.0	0.0

Watershed Characteristics

S	ubcatchment Area (acres)		
P	ercent Impervious		
Ν	RCS Soil Type		

Watershed Profile

Overland Slope (ft/ft)		
Overland Length (ft)		
Channel Slope (ft/ft)		
Channel Length (ft)		

Minor Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P ₁ (inches)		

Major Storm Rainfall Input

Design Storm Return Period, T _r (years)		
One-Hour Precipitation, P ₁ (inches)		

Minor Total Design Peak Flow, Q (cfs)	0.7	0.7	0.7
Major Total Design Peak Flow, Q (cfs)	1.3	2.6	1.1
Minor Flow Bypassed Downstream, Q_b (cfs)	0.0	0.0	0.0
Major Flow Bypassed Downstream, Q_b (cfs)	0.0	0.0	0.0

INLET MANAGEMENT

Worksheet Protected

INLET NAME	<u>IN-L-87</u>
Site Type (Urban or Rural)	URBAN
Inlet Application (Street or Area)	STREET
Hydraulic Condition	On Grade
Inlet Type	CDOT Type R Curb Opening

USER-DEFINED INPUT

User-Defined Design Flows	
Minor Q _{Known} (cfs)	0.8
Major Q _{Known} (cfs)	1.3

Bypass (Carry-Over) Flow from Upstream	let:
Receive Bypass Flow from:	IN-L-85
Minor Bypass Flow Received, Q _b (cfs)	0.0
Major Bypass Flow Received, Q _b (cfs)	0.0

Watershed Characteristics

Subcatchment Area (acres)	
Percent Impervious	
NRCS Soil Type	

Watershed Profile

Overland Slope (ft/ft)	
Overland Length (ft)	
Channel Slope (ft/ft)	
Channel Length (ft)	

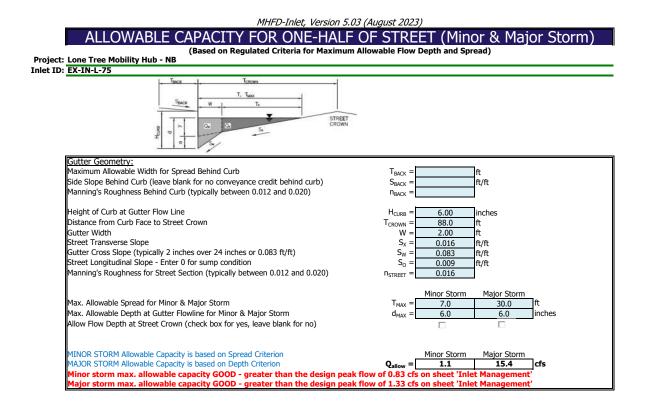
Minor Storm Rainfall Input

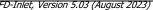
Design Storm Return Period, T _r (years)	
One-Hour Precipitation, P ₁ (inches)	

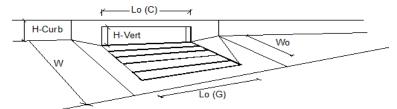
Major Storm Rainfall Input

Design Storm Return Period, T _r (years)	
One-Hour Precipitation, P ₁ (inches)	

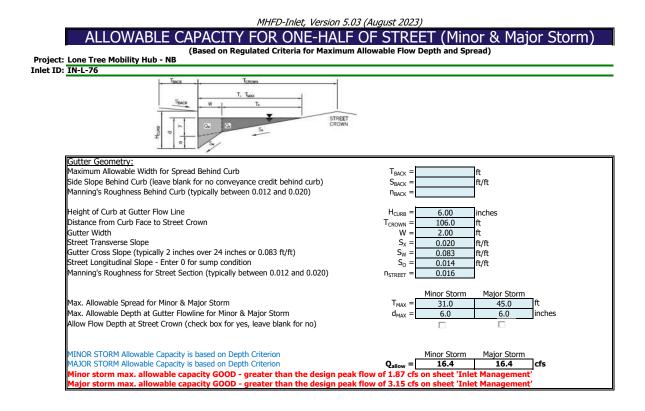
Minor Total Design Peak Flow, Q (cfs)	0.8
Major Total Design Peak Flow, Q (cfs)	1.3
Minor Flow Bypassed Downstream, Q_b (cfs)	0.0
Major Flow Bypassed Downstream, Q _b (cfs)	0.1

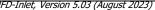


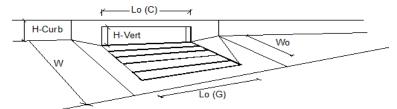




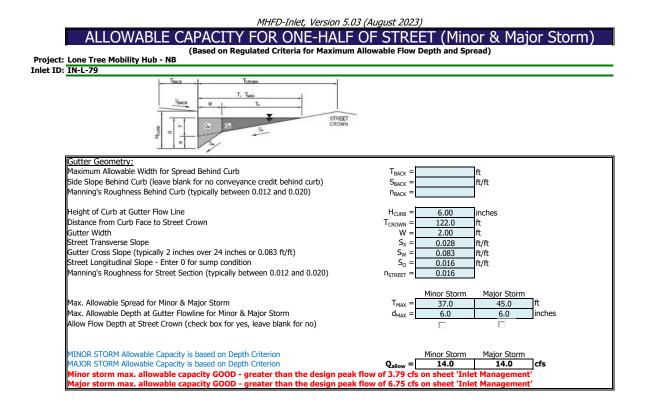
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =		ast Vane Grate	1
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	0.0	0.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	linches
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_0 =$	4.00	4.00	ft
5 5 1 5				
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_{o} =$	2.00	2.00	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	0.50	0.50	-
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	N/A	N/A	
Street Hydraulics: OK - Q < Allowable Street Capacity	- T	MINOR	MAJOR	٦.
Design Discharge for Half of Street (from <i>Inlet Management</i>)	Q _o =	0.8	1.3	cfs
Water Spread Width	T =	5.8	7.8	ft
Water Depth at Flowline (outside of local depression)	d =	2.7	3.1	inches
Water Depth at Street Crown (or at T _{MAX})	d _{CROWN} =	0.0	0.0	inches
Ratio of Gutter Flow to Design Flow	E ₀ =	0.864	0.737	
Discharge outside the Gutter Section W, carried in Section T _x	$Q_x =$	0.1	0.3	cfs
Discharge within the Gutter Section W	Q _w =	0.7	1.0	cfs
Discharge Behind the Curb Face	Q _{BACK} =	0.0	0.0	cfs
Flow Area within the Gutter Section W	A _W =	0.28	0.35	sq ft
Velocity within the Gutter Section W	V _w =	2.5	2.8	fps
Water Depth for Design Condition	d _{LOCAL} =	2.7	3.1	inches
Grate Analysis (Calculated)	110.0	MINOR	MAJOR	
Total Length of Inlet Grate Opening	L =	4.00	4.00	ft
Ratio of Grate Flow to Design Flow	E _{o-GRATE} =	0.864	0.737	
Under No-Clogging Condition	-0-GRATE	MINOR	MAJOR	
Minimum Velocity Where Grate Splash-Over Begins	V ₀ =	8.34	8.34	fps
Interception Rate of Frontal Flow	V ₀ – R _f =	1.00	1.00	ihe
				-
Interception Rate of Side Flow	$R_x =$	0.40	0.38	
Interception Capacity	$Q_i =$	0.8	1.1	cfs
Under Clogging Condition		MINOR	MAJOR	-
Clogging Coefficient for Multiple-unit Grate Inlet	GrateCoeff =	1.00	1.00	_
Clogging Factor for Multiple-unit Grate Inlet	GrateClog =	0.50	0.50	
Effective (unclogged) Length of Multiple-unit Grate Inlet	L _e =	2.00	2.00	ft
Minimum Velocity Where Grate Splash-Over Begins	V _o =	5.96	5.96	fps
Interception Rate of Frontal Flow	$R_{f} =$	1.00	1.00	
Interception Rate of Side Flow	$R_x =$	0.12	0.11	
Actual Interception Capacity	Q _a =	0.7	1.0	cfs
Carry-Over Flow = Q_0 - Q_a (to be applied to curb opening or next d/s inlet)	$Q_{\rm b} =$	0.1	0.3	cfs
Curb Opening or Slotted Inlet Analysis (Calculated)		MINOR	MAJOR	
Equivalent Slope Se	S _e =	N/A	N/A	ft/ft
Required Length L_{T} to Have 100% Interception	L _T =	N/A	N/A	ft
Under No-Clogging Condition	· .	MINOR	MAJOR	
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L_T)	L =	N/A	N/A	ft
Interception Capacity	$Q_i =$	N/A	N/A	cfs
Under Clogging Condition	Qi –	MINOR	MAJOR	0.5
Clogging Coefficient	CurbCoeff =	N/A	MAJOR N/A	7
				-1
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet	CurbClog =	N/A	N/A	
Effective (Unclogged) Length	L _e =	N/A	N/A	ft
Actual Interception Capacity	$Q_a =$	N/A	N/A	cfs
Carry-Over Flow = $Q_{b(GRATF)}$ - Q_a	Q _b =	N/A	N/A	cfs
Summary	F	MINOR	MAJOR	٦.
Total Inlet Interception Capacity	Q =	0.7	1.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.1	0.3	cfs
Capture Percentage = Q_a/Q_a	C% =	88	77	%

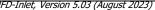


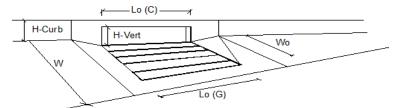




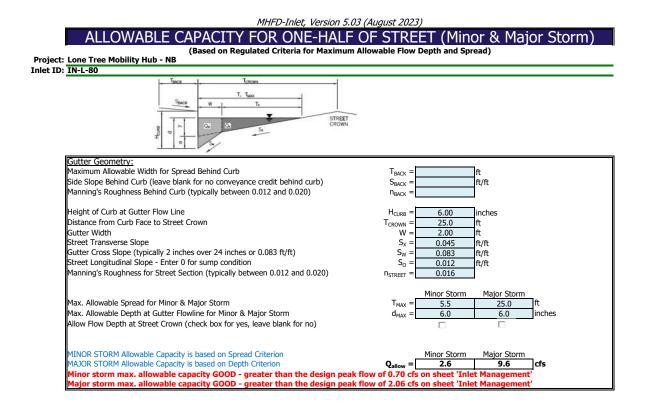
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =		Curb Opening	٦
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	<u> </u>	1	linches
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_0 =$	5.00	5.00	ft
			N/A	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_0 =$	N/A		, it
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	-
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10 MINOR	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	o [MAJOR	-6-
Design Discharge for Half of Street (from <i>Inlet Management</i>)	$Q_0 =$	1.9	3.2	cfs
Water Spread Width	T =	7.1	9.3	ft .
Water Depth at Flowline (outside of local depression)	d =	3.2	3.7	inches
Water Depth at Street Crown (or at T _{MAX})	d _{CROWN} =	0.0	0.0	inches
Ratio of Gutter Flow to Design Flow	$E_0 =$	0.744	0.614	4.
Discharge outside the Gutter Section W, carried in Section T_x	$Q_x =$	0.5	1.2	cfs
Discharge within the Gutter Section W	Q _w =	1.4	1.9	cfs
Discharge Behind the Curb Face	$Q_{BACK} =$	0.0	0.0	cfs
Flow Area within the Gutter Section W	A _W =	0.37	0.46	sq ft
Velocity within the Gutter Section W	V _W =	3.8	4.2	fps
Water Depth for Design Condition	d _{LOCAL} =	6.2	6.7	inches
Grate Analysis (Calculated)	-	MINOR	MAJOR	-
Total Length of Inlet Grate Opening	L =	N/A	N/A	ft
Ratio of Grate Flow to Design Flow	$E_{o-GRATE} =$	N/A	N/A	
Under No-Clogging Condition	_	MINOR	MAJOR	_
Minimum Velocity Where Grate Splash-Over Begins	V _o =	N/A	N/A	fps
Interception Rate of Frontal Flow	$R_f =$	N/A	N/A	
Interception Rate of Side Flow	$R_x =$	N/A	N/A	
Interception Capacity	$Q_i =$	N/A	N/A	cfs
Under Clogging Condition		MINOR	MAJOR	
Clogging Coefficient for Multiple-unit Grate Inlet	GrateCoeff =	N/A	N/A	
Clogging Factor for Multiple-unit Grate Inlet	GrateClog =	N/A	N/A	
Effective (unclogged) Length of Multiple-unit Grate Inlet	L _e =	N/A	N/A	ft
Minimum Velocity Where Grate Splash-Over Begins	V ₀ =	N/A	N/A	fps
Interception Rate of Frontal Flow	$R_f =$	N/A	N/A	1
Interception Rate of Side Flow	R _x =	N/A	N/A	
Actual Interception Capacity	Q _a =	N/A	N/A	cfs
Carry-Over Flow = $Q_0 - Q_a$ (to be applied to curb opening or next d/s inlet)	$Q_{\rm b} =$	N/A	N/A	cfs
Curb Opening or Slotted Inlet Analysis (Calculated)		MINOR	MAJOR	
Equivalent Slope Se	S _e =	0.160	0.136	ft/ft
Required Length L _T to Have 100% Interception	L _T =	6.36	8.96	ft
Under No-Clogging Condition	· <u>·</u>	MINOR	MAJOR	-
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L_T)	L =	5.00	5.00	ft
Interception Capacity	$\overline{Q_i} =$	1.8	2.4	cfs
Under Clogging Condition		MINOR	MAJOR	
Clogging Coefficient	CurbCoeff =	1.00	1.00	٦
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet	CurbClog =	0.10	0.10	4
Effective (Unclogged) Length	L _e =	4.50	4.50	ft
Actual Interception Capacity	$\mathbf{Q}_{\mathbf{a}} =$	1.7	2.3	cfs
Carry-Over Flow = $Q_{b(GRATE)}$ - Q_a	$Q_a = Q_b =$	0.2	0.9	cfs
Summary		MINOR	MAJOR	1010
Total Inlet Interception Capacity	Q =	1.7	2.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q = Q _b =	0.2	0.9	cfs
Capture Percentage = Q_a/Q_o	Qь = С% =	89	72	%
capture rententage = Q_a/Q_0	L% =	69	/2	170

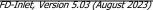


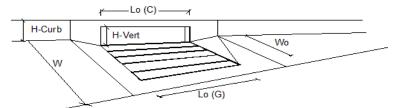




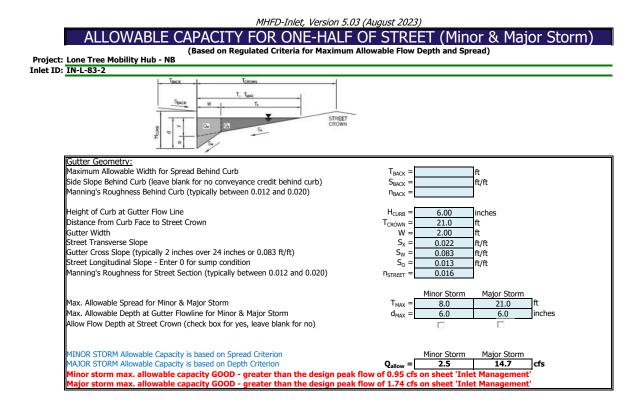
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =		Curb Opening	٦
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	inches
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_0 =$	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W ₀ =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	-
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	- T	MINOR	MAJOR	7.4
Design Discharge for Half of Street (from <i>Inlet Management</i>)	$Q_o =$	3.8	6.7	cfs
Water Spread Width	T =	8.0	10.3	ft
Water Depth at Flowline (outside of local depression)	d =	4.0	4.8	inches
Water Depth at Street Crown (or at T _{MAX})	d _{CROWN} =	0.0	0.0	inches
Ratio of Gutter Flow to Design Flow	E ₀ =	0.637	0.518	
Discharge outside the Gutter Section W, carried in Section T_x	$Q_x =$	1.4	3.2	cfs
Discharge within the Gutter Section W	Q _w =	2.4	3.5	cfs
Discharge Behind the Curb Face	$Q_{BACK} =$	0.0	0.0	cfs
Flow Area within the Gutter Section W	A _W =	0.50	0.63	sq ft
Velocity within the Gutter Section W	V _W =	4.8	5.5	fps
Water Depth for Design Condition	d _{LOCAL} =	7.0	7.8	inches
Grate Analysis (Calculated)		MINOR	MAJOR	
Total Length of Inlet Grate Opening	L =	N/A	N/A	ft
Ratio of Grate Flow to Design Flow	E _{o-GRATE} =	N/A	N/A	
Under No-Clogging Condition		MINOR	MAJOR	
Minimum Velocity Where Grate Splash-Over Begins	V ₀ =	N/A	N/A	fps
Interception Rate of Frontal Flow	R _f =	N/A	N/A	.60
Interception Rate of Side Flow	$R_x =$	N/A	N/A	
Interception Page of Side Flow	$Q_i =$	N/A	N/A	cfs
Under Clogging Condition	Qi =	MINOR	MAJOR	cis
Clogging Coefficient for Multiple-unit Grate Inlet	GrateCoeff =	N/A	N/A	٦
Clogging Factor for Multiple-unit Grate Inlet	GrateClog =	N/A	N/A N/A	-
				ft
Effective (unclogged) Length of Multiple-unit Grate Inlet	$L_e =$	N/A	N/A	
Minimum Velocity Where Grate Splash-Over Begins	V ₀ =	N/A	N/A	fps
Interception Rate of Frontal Flow	$R_{f} =$	N/A	N/A	
Interception Rate of Side Flow	$R_x =$	N/A	N/A	-
Actual Interception Capacity	Q _a =	N/A	N/A	cfs
Carry-Over Flow = $Q_0 - Q_a$ (to be applied to curb opening or next d/s inlet)	Q _b =	N/A	N/A	cfs
Curb Opening or Slotted Inlet Analysis (Calculated)		MINOR	MAJOR	-
Equivalent Slope S _e	S _e =	0.143	0.121	ft/ft
Required Length L_T to Have 100% Interception	L _T =	9.68	13.99	ft
Under No-Clogging Condition	-	MINOR	MAJOR	-
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L_T)	L =	9.68	10.00	ft
Interception Capacity	$Q_i =$	3.8	6.0	cfs
Under Clogging Condition	_	MINOR	MAJOR	
Clogging Coefficient	CurbCoeff =	1.25	1.25	
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet	CurbClog =	0.06	0.06	1
Effective (Unclogged) Length	L _e =	9.38	9.38	ft
Actual Interception Capacity	Q _a =	3.8	5.8	cfs
Carry-Over Flow = $Q_{b/GRATE}$ - Q_a	\tilde{Q}_{b} =	0.0	0.9	cfs
Summary	-20	MINOR	MAJOR	1.51.5
Total Inlet Interception Capacity	Q =	3.8	5.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.9	cfs
Capture Percentage = Q_3/Q_0	Qь – С% =	100	86	%

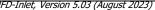


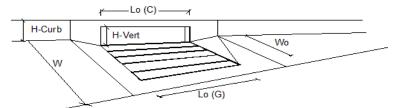




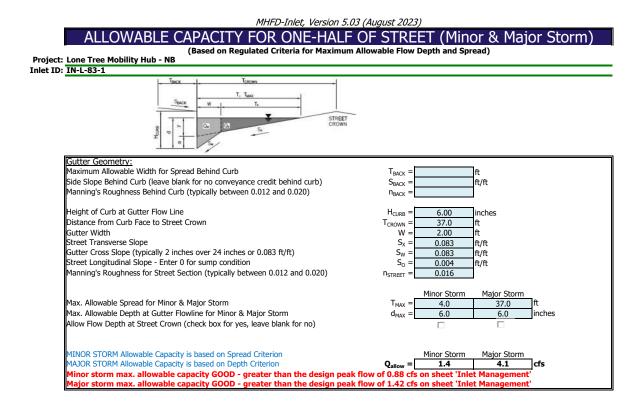
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	inches
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_0 =$	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W ₀ =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f(G) =$	N/A N/A	N/A	ii.
	$C_f(G) = C_f(C) =$	0.10	0.10	-
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1) Street Hydraulics: OK - Q < Allowable Street Capacity'	$C_{f}(C) =$	MINOR	MAJOR	
	o [0.7	MAJOR 2.1	cfs
Design Discharge for Half of Street (from <i>Inlet Management</i>)	$Q_0 =$	-		
Water Spread Width	Τ=	2.9	5.0	ft .
Water Depth at Flowline (outside of local depression)	d =	2.5	3.6	inches
Water Depth at Street Crown (or at T _{MAX})	d _{CROWN} =	0.0	0.0	inches
Ratio of Gutter Flow to Design Flow	E ₀ =	0.977	0.804	-
Discharge outside the Gutter Section W, carried in Section T_x	$Q_x =$	0.0	0.4	cfs
Discharge within the Gutter Section W	Q _w =	0.7	1.7	cfs
Discharge Behind the Curb Face	$Q_{BACK} =$	0.0	0.0	cfs
Flow Area within the Gutter Section W	A _W =	0.25	0.43	sq ft
Velocity within the Gutter Section W	$V_W =$	2.8	3.8	fps
Water Depth for Design Condition	d _{LOCAL} =	5.5	6.6	inches
Grate Analysis (Calculated)	_	MINOR	MAJOR	_
Total Length of Inlet Grate Opening	L =	N/A	N/A	ft
Ratio of Grate Flow to Design Flow	$E_{o-GRATE} =$	N/A	N/A	
Under No-Clogging Condition	-	MINOR	MAJOR	
Minimum Velocity Where Grate Splash-Over Begins	V _o =	N/A	N/A	fps
Interception Rate of Frontal Flow	$R_{f} =$	N/A	N/A	
Interception Rate of Side Flow	R _x =	N/A	N/A	
Interception Capacity	$Q_i =$	N/A	N/A	cfs
Under Clogging Condition		MINOR	MAJOR	
Clogging Coefficient for Multiple-unit Grate Inlet	GrateCoeff =	N/A	N/A	
Clogging Factor for Multiple-unit Grate Inlet	GrateClog =	N/A	N/A	
Effective (unclogged) Length of Multiple-unit Grate Inlet	L _e =	N/A	N/A	ft
Minimum Velocity Where Grate Splash-Over Begins	V _o =	N/A	N/A	fps
Interception Rate of Frontal Flow	$R_{f} =$	N/A	N/A	
Interception Rate of Side Flow	R _x =	N/A	N/A	
Actual Interception Capacity	$Q_a =$	N/A	N/A	cfs
Carry-Over Flow = Q_0 - Q_a (to be applied to curb opening or next d/s inlet)	$\dot{\mathbf{Q}}_{b} =$	N/A	N/A	cfs
Curb Opening or Slotted Inlet Analysis (Calculated)	₹₿ I	MINOR	MAJOR	
Equivalent Slope S _e	S _e =	0.204	0.176	ft/ft
Required Length L_T to Have 100% Interception	L _T =	3.41	6.34	ft
Under No-Clogging Condition		MINOR	MAJOR	ii.
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L _T)	L =	3.41	5.00	ft
Interception Capacity	L = Q _i =	0.7	1.9	cfs
Under Clogging Condition	21-	MINOR	MAJOR	0.5
Clogging Coefficient	CurbCoeff =	1.00	1.00	٦
				-
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet	CurbClog =	0.10	0.10	ft
Effective (Unclogged) Length	L _e =	3.41	4.50	
Actual Interception Capacity	Q _a =	0.7	1.8	cfs
Carry-Over Flow = $Q_{b(GRATE)} - Q_a$	Q _b =	0.0	0.2	cfs
Summary	~ 5	MINOR	MAJOR	٦.
Total Inlet Interception Capacity	Q =	0.7	1.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet) Capture Percentage = Q _a /Q _o	$Q_b =$	0.0	0.2	cfs
	C% =	100	89	%

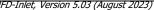


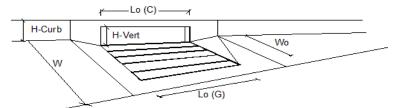




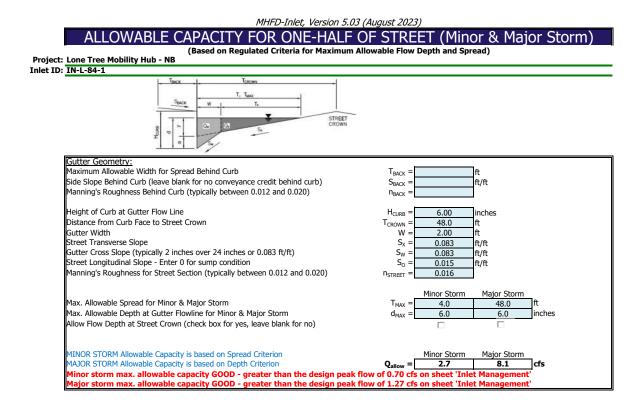
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	a _{LOCAL} = No =	<u> </u>	1	incries
			5.00	ft
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_{o} =$	5.00		
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	-
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	- T	MINOR	MAJOR	٦.
Design Discharge for Half of Street (from Inlet Management)	$Q_0 =$	1.0	1.7	cfs
Water Spread Width	T =	4.6	6.6	ft
Water Depth at Flowline (outside of local depression)	d =	2.7	3.2	inches
Water Depth at Street Crown (or at T _{MAX})	d _{CROWN} =	0.0	0.0	inches
Ratio of Gutter Flow to Design Flow	E ₀ =	0.906	0.763	
Discharge outside the Gutter Section W, carried in Section T_x	$Q_x =$	0.1	0.4	cfs
Discharge within the Gutter Section W	$Q_w =$	0.9	1.3	cfs
Discharge Behind the Curb Face	$Q_{BACK} =$	0.0	0.0	cfs
Flow Area within the Gutter Section W	A _W =	0.28	0.37	sq ft
Velocity within the Gutter Section W	V _W =	3.1	3.6	fps
Water Depth for Design Condition	d _{LOCAL} =	5.7	6.2	inches
Grate Analysis (Calculated)		MINOR	MAJOR	
Total Length of Inlet Grate Opening	L =	N/A	N/A	ft
Ratio of Grate Flow to Design Flow	E _{o-GRATE} =	N/A	N/A	
Under No-Clogging Condition	U-GIGHTE	MINOR	MAJOR	
Minimum Velocity Where Grate Splash-Over Begins	V ₀ =	N/A	N/A	fps
Interception Rate of Frontal Flow	R _f =	N/A	N/A	.60
Interception Rate of Side Flow	$R_x =$	N/A	N/A	
Interception Capacity	$Q_i =$	N/A	N/A	cfs
Under Clogging Condition	Qi -	MINOR	MAJOR	0.3
Clogging Coefficient for Multiple-unit Grate Inlet	GrateCoeff =	N/A	N/A	7
Clogging Factor for Multiple-unit Grate Inlet	GrateClog =	N/A	N/A N/A	-
				ft
Effective (unclogged) Length of Multiple-unit Grate Inlet	$L_e =$	N/A	N/A	
Minimum Velocity Where Grate Splash-Over Begins	V _o =	N/A	N/A	fps
Interception Rate of Frontal Flow	R _f =	N/A	N/A	
Interception Rate of Side Flow	$R_x =$	N/A	N/A	-
Actual Interception Capacity	Q _a =	N/A	N/A	cfs
Carry-Over Flow = Q_0 - Q_a (to be applied to curb opening or next d/s inlet)	Q _b =	N/A	N/A	cfs
Curb Opening or Slotted Inlet Analysis (Calculated)		MINOR	MAJOR	-
Equivalent Slope S _e	S _e =	0.191	0.164	ft/ft
Required Length L_T to Have 100% Interception	$L_T =$	4.14	6.04	ft
Under No-Clogging Condition	-	MINOR	MAJOR	-
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L_T)	L =	4.14	5.00	ft
Interception Capacity	$Q_i =$	1.0	1.7	cfs
Under Clogging Condition	_	MINOR	MAJOR	_
Clogging Coefficient	CurbCoeff =	1.00	1.00	
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet	CurbClog =	0.10	0.10	
Effective (Unclogged) Length	L _e =	4.14	4.50	ft
Actual Interception Capacity	Q _a =	1.0	1.6	cfs
Carry-Over Flow = $Q_{b(GRATE)}$ - Q_a	$Q_b =$	0.0	0.1	cfs
Summary	20	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.0	1.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.1	cfs
		100	91	%
Capture Percentage = Q_a/Q_o	C% =	100	91	%



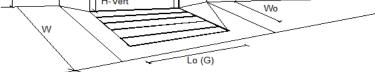




Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	a _{LOCAL} = No =	<u> </u>	1	incries
			5.00	ft
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_o =$	5.00		
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_f(G) =$	N/A	N/A	-
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	- F	MINOR	MAJOR	٦.
Design Discharge for Half of Street (from <i>Inlet Management</i>)	Q _o =	0.9	1.4	cfs
Water Spread Width	T =	3.4	4.0	ft
Water Depth at Flowline (outside of local depression)	d =	3.4	4.0	inches
Water Depth at Street Crown (or at T _{MAX})	d _{CROWN} =	0.0	0.0	inches
Ratio of Gutter Flow to Design Flow	E ₀ =	0.907	0.837	
Discharge outside the Gutter Section W, carried in Section T_x	$Q_x =$	0.1	0.2	cfs
Discharge within the Gutter Section W	Q _w =	0.8	1.2	cfs
Discharge Behind the Curb Face	$Q_{BACK} =$	0.0	0.0	cfs
Flow Area within the Gutter Section W	A _W =	0.40	0.51	sq ft
Velocity within the Gutter Section W	V _w =	2.0	2.3	fps
Water Depth for Design Condition	d _{LOCAL} =	6.4	7.0	inches
Grate Analysis (Calculated)		MINOR	MAJOR	
Total Length of Inlet Grate Opening	L =	N/A	N/A	ft
Ratio of Grate Flow to Design Flow	E _{o-GRATE} =	N/A	N/A	
Under No-Clogging Condition	-0-GRATE	MINOR	MAJOR	
Minimum Velocity Where Grate Splash-Over Begins	V. =	N/A	N/A	fps
Interception Rate of Frontal Flow	R _f =	N/A	N/A	100
Interception Rate of Side Flow	$R_x =$	N/A	N/A	
Interception Capacity	$Q_i =$	N/A	N/A	cfs
Under Clogging Condition	Qi -	MINOR	MAJOR	CI3
Clogging Coefficient for Multiple-unit Grate Inlet	GrateCoeff =	N/A	N/A	7
				-
Clogging Factor for Multiple-unit Grate Inlet	GrateClog =	N/A	N/A	A.
Effective (unclogged) Length of Multiple-unit Grate Inlet	L _e =	N/A	N/A	ft
Minimum Velocity Where Grate Splash-Over Begins	V _o =	N/A	N/A	fps
Interception Rate of Frontal Flow	R _f =	N/A	N/A	_
Interception Rate of Side Flow	R _x =	N/A	N/A	
Actual Interception Capacity	$Q_a =$	N/A	N/A	cfs
Carry-Over Flow = Q_0 - Q_a (to be applied to curb opening or next d/s inlet)	Q _b =	N/A	N/A	cfs
Curb Opening or Slotted Inlet Analysis (Calculated)	F	MINOR	MAJOR	-
Equivalent Slope S _e	S _e =	0.196	0.188	ft/ft
Required Length L_T to Have 100% Interception	$L_T =$	3.65	4.76	ft
Under No-Clogging Condition	_	MINOR	MAJOR	_
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L _T)	L =	3.65	4.76	ft
Interception Capacity	$Q_i =$	0.9	1.4	cfs
Under Clogging Condition	-	MINOR	MAJOR	_
Clogging Coefficient	CurbCoeff =	1.00	1.00	
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet	CurbClog =	0.10	0.10	
Effective (Unclogged) Length	L _e =	3.65	4.50	ft
Actual Interception Capacity	Q _a =	0.9	1.4	cfs
Carry-Over Flow = $Q_{b/GRATE}$ - Q_a	\tilde{Q}_{b} =	0.0	0.0	cfs
Summary	≺ b [−]	MINOR	MAJOR	1010
Total Inlet Interception Capacity	Q =	0.9	1.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q = Q _b =	0.0	0.0	cfs
Capture Percentage = Q_a/Q_o	Qь = С% =	100	99	%



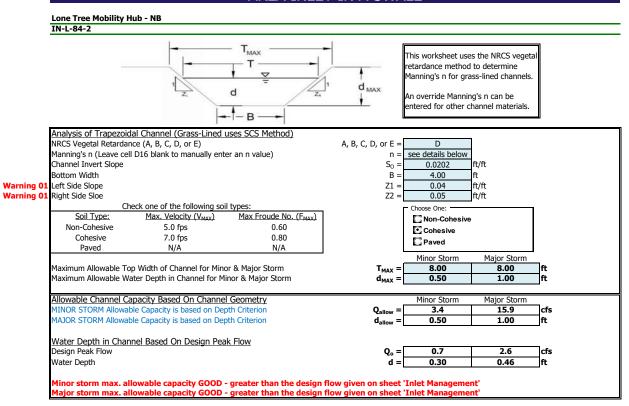


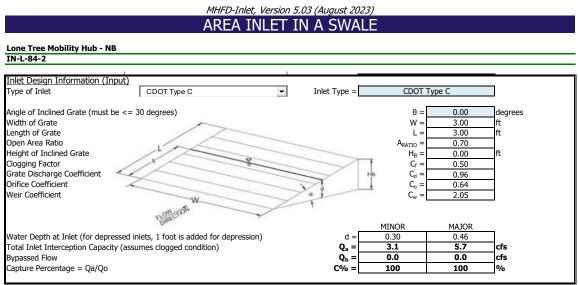


H-Curb

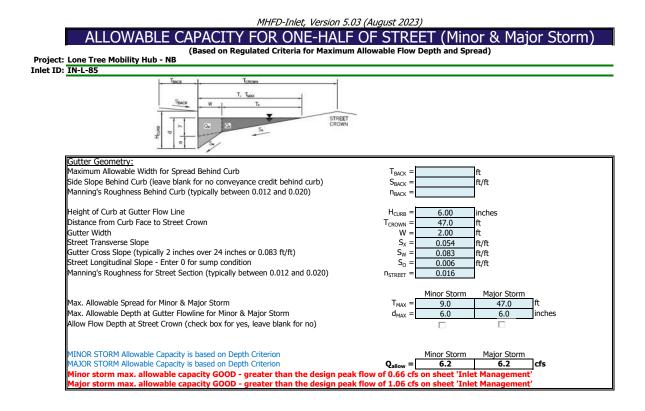
Design Information (Input) CDOT Type R Curb Opening	1	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.7	1.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.0	cfs
Capture Percentage = Q_a/Q_o	C% =	100	100	%

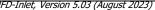
MHFD-Inlet, Version 5.03 (August 2023) AREA INLET IN A SWALE

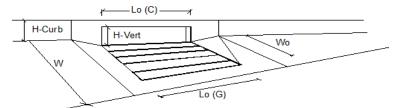




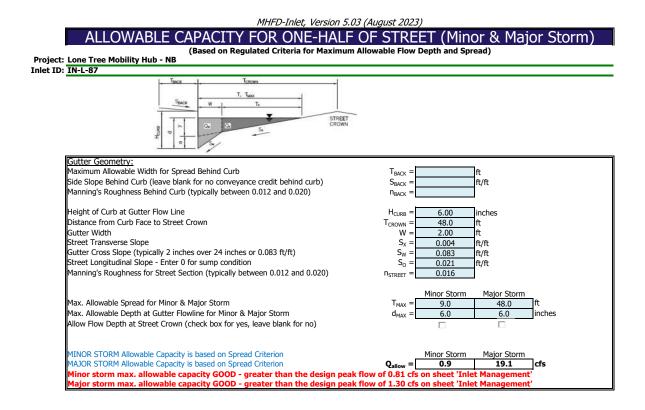
Warning 01: Sideslope steepness exceeds USDCM Volume I recommendation. Warning 02: Depth (d) exceeds USDCM Volume I recommendation.

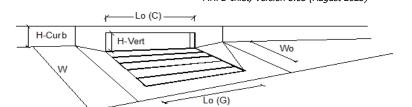






Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =		Curb Opening	
Local Depression (additional to continuous gutter depression 'a')		3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	a _{LOCAL} = No =	<u> </u>	1	incries
	-		5.00	ft
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_0 =$	5.00		
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_0 =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	-
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	- T	MINOR	MAJOR	٦.
Design Discharge for Half of Street (from <i>Inlet Management</i>)	$Q_0 =$	0.7	1.1	cfs
Water Spread Width	Τ=	3.2	4.0	ft
Water Depth at Flowline (outside of local depression)	d =	2.7	3.3	inches
Water Depth at Street Crown (or at T _{MAX})	d _{CROWN} =	0.0	0.0	inches
Ratio of Gutter Flow to Design Flow	E ₀ =	0.951	0.881	
Discharge outside the Gutter Section W, carried in Section T_x	$Q_x =$	0.0	0.1	cfs
Discharge within the Gutter Section W	Q _w =	0.6	0.9	cfs
Discharge Behind the Curb Face	$Q_{BACK} =$	0.0	0.0	cfs
Flow Area within the Gutter Section W	A _W =	0.29	0.38	sq ft
Velocity within the Gutter Section W	V _w =	2.2	2.5	fps
Water Depth for Design Condition	d _{LOCAL} =	5.7	6.3	inches
Grate Analysis (Calculated)		MINOR	MAJOR	
Total Length of Inlet Grate Opening	L =	N/A	N/A	ft
Ratio of Grate Flow to Design Flow	E _{o-GRATE} =	N/A	N/A	
Under No-Clogging Condition	-0-GRATE	MINOR	MAJOR	
Minimum Velocity Where Grate Splash-Over Begins	V ₀ =	N/A	N/A	fps
Interception Rate of Frontal Flow	R _f =	N/A	N/A	105
Interception Rate of Side Flow	$R_x =$	N/A	N/A	-
Interception Capacity	$Q_i =$	N/A	N/A	cfs
Under Clogging Condition	- iv	MINOR	MAJOR	us
Clogging Coefficient for Multiple-unit Grate Inlet	GrateCoeff =	N/A	N/A	7
				-
Clogging Factor for Multiple-unit Grate Inlet	GrateClog =	N/A	N/A	A.
Effective (unclogged) Length of Multiple-unit Grate Inlet	$L_e =$	N/A	N/A	ft
Minimum Velocity Where Grate Splash-Over Begins	V _o =	N/A	N/A	fps
Interception Rate of Frontal Flow	$R_{f} =$	N/A	N/A	_
Interception Rate of Side Flow	$R_x =$	N/A	N/A	
Actual Interception Capacity	$Q_a =$	N/A	N/A	cfs
Carry-Over Flow = Q_0 - Q_a (to be applied to curb opening or next d/s inlet)	Q _b =	N/A	N/A	cfs
Curb Opening or Slotted Inlet Analysis (Calculated)	-	MINOR	MAJOR	-
Equivalent Slope S _e	S _e =	0.200	0.190	ft/ft
Required Length L_T to Have 100% Interception	L _T =	3.21	4.21	ft
Under No-Clogging Condition	_	MINOR	MAJOR	_
Effective Length of Curb Opening or Slotted Inlet (minimum of L, L _T)	L =	3.21	4.21	ft
Interception Capacity	$Q_i =$	0.7	1.1	cfs
Under Clogging Condition	-	MINOR	MAJOR	_
Clogging Coefficient	CurbCoeff =	1.00	1.00	
Clogging Factor for Multiple-unit Curb Opening or Slotted Inlet	CurbClog =	0.10	0.10	
Effective (Unclogged) Length	L _e =	3.21	4.21	ft
Actual Interception Capacity	Q _a =	0.7	1.1	cfs
Carry-Over Flow = $Q_{h(GRATE)} - Q_a$	$\vec{Q}_{b} =$	0.0	0.0	cfs
Summary		MINOR	MAJOR	1010
Total Inlet Interception Capacity	Q =	0.7	1.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_{\rm b} =$	0.0	0.0	cfs
Capture Percentage = Q_a/Q_o	Qь = С% =	100	100	%





Design Information (Input) CDOT Type R Curb Opening	-	MINOR	MAJOR	1
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}(G) =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}(C) =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	0.8	1.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.1	cfs
Capture Percentage = Q_a/Q_o	C% =	100	96	%

Project Description		
Solve For	Efficiency	
Input Data		
Discharge	0.21 cfs	
Slope	0.081 ft/ft	
Gutter Width	3.00 ft	
Gutter Cross Slope	0.015 ft/ft	
Road Cross Slope	0.015 ft/ft	
Roughness Coefficient	0.016	
Grate Width	2.94 ft	
Grate Length	1.1 ft	
Grate Type	P-30 mm (P-1 -7/8")	
Clogging	50.0 %	
Grate Flow Option	Exclude None	
Results		
Efficiency	99.82 %	
Intercepted Flow	0.21 cfs	
Bypass Flow	0.00 cfs	
Spread	3.2 ft	
Depth	0.6 in	
Flow Area	0.1 ft ²	
Gutter Depression	0.0 in	
Total Depression	0.0 in	
Velocity	2.66 ft/s	
Splash Over Velocity	3.31 ft/s	
Frontal Flow Factor	1.000	
Side Flow Factor	0.004	
Grate Flow Ratio	0.998	
Active Grate Length	0.5 ft	

Worksheet for IN-L-103

Project Description		
Solve For	Efficiency	
Input Data		
Discharge	0.35 cfs	
Slope	0.081 ft/ft	
Gutter Width	3.00 ft	
Gutter Cross Slope	0.015 ft/ft	
Road Cross Slope	0.015 ft/ft	
Roughness Coefficient	0.016	
Grate Width	2.94 ft	
Grate Length	1.1 ft	
Grate Type	P-30 mm (P-1 -7/8")	
Clogging	50.0 %	
Grate Flow Option	Exclude None	
Results		
Efficiency	97.48 %	
Intercepted Flow	0.34 cfs	
Bypass Flow	0.01 cfs	
Spread	3.9 ft	
Depth	0.7 in	
Flow Area	0.1 ft ²	
Gutter Depression	0.0 in	
Total Depression	0.0 in	
Velocity	3.02 ft/s	
Splash Over Velocity	3.31 ft/s	
Frontal Flow Factor	1.000	
Side Flow Factor	0.003	
Grate Flow Ratio	0.975	
Active Grate Length	0.5 ft	

Worksheet for IN-L-109

Project Description		
Solve For	Efficiency	
Input Data		
Discharge	0.25 cfs	
Slope	0.017 ft/ft	
Gutter Width	0.00 ft	
Gutter Cross Slope	0.016 ft/ft	
Road Cross Slope	0.016 ft/ft	
Roughness Coefficient	0.016	
Grate Width	2.94 ft	
Grate Length	1.1 ft	
Grate Type	P-30 mm (P-1 -7/8")	
Clogging	50.0 %	
Grate Flow Option	Exclude None	
Results		
Efficiency	94.41 %	
Intercepted Flow	0.24 cfs	
Bypass Flow	0.01 cfs	
Spread	4.5 ft	
Depth	0.9 in	
Flow Area	0.2 ft ²	
Gutter Depression	0.0 in	
Total Depression	0.0 in	
Velocity	1.57 ft/s	
Splash Over Velocity	3.31 ft/s	
Frontal Flow Factor	1.000	
Side Flow Factor	0.011	
Grate Flow Ratio	0.943	
Active Grate Length	0.5 ft	

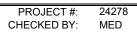
Worksheet for IN-L-111

APPENDIX B.2 – STORM SEWER CAPACITY, HGL AND EGL

B.3A STORM SEWER HYDRAULIC CALCULATIONS (10-YEAR STORM)

PROJECT: DESIGNED BY: DATE: I-25 Mobility Hub (Lone Tree) NAG 12/15/2023

	DESIGN FREQUENCY - 10 YEAR - SYSTEM SB Lanes																		
PIPE ID	UPSTREAM NODE	DOWNSTREAM NODE	SHAPE	MATERIAL	DIAMETER	N VALUE	LENGTH (FT)	SLOPE	INV UPSTREAM (FT)	INV DOWNSTREAM (FT)	Q (CFS)	CRITICAL DEPTH (FT)	ACTUAL DEPTH (FT)	CAPACITY (CFS)	VELOCITY (FT/SEC)	HGL UPSTREAM (FT)	HGL DOWNSTREAM (FT)	EGL UPSTREAM (FT)	EGL DOWNSTREAM (FT)
EX-P-L-21S	EX-IN-L-21-5	EX-FES-L-21S	CIRCULAR	CLASS 7 PIPE	30"	0.013	185.16	1.17%	5978.11	5975.92	19.91	1.05	1.05	88.86	7.30	5979.17	5976.73	5979.56	5977.55
EX-P-L-48-2	EX-IN-L-48-2	EX-IN-L-48-1	CIRCULAR	CLASS 7 PIPE	18"	0.013	36.07	0.67%	5988.87	5988.62	3.35	0.70	1.12	8.59	4.56	5989.99	5989.98	5990.08	5990.04
EX-P-L-48-3	EX-IN-L-48-3	EX-IN-L-48-2	CIRCULAR	CLASS 7 PIPE	18"	0.013	1.39	0.29%	5988.89	5988.88	2.32	0.58	1.20	5.61	3.03	5990.09	5990.09	5990.13	5990.12
P-L-12	IN-L-12	IN-L-14	CIRCULAR	CLASS 7 PIPE	18"	0.010	184.43	0.35%	5991.36	5990.71	4.38	0.80	0.80	8.12	4.68	5992.17	5991.82	5992.49	5991.97
P-L-14	IN-L-14	MH-L-15-1	CIRCULAR	CLASS 7 PIPE	18"	0.010	72.69	1.06%	5990.51	5989.71	5.42	0.90	0.90	14.08	7.45	5991.41	5990.84	5991.78	5991.06
P-L-15	IN-L-15	MH-L-15-1	CIRCULAR	CLASS 7 PIPE	18"	0.010	5.52	3.74%	5991.01	5990.71	0.92	0.36	0.36	26.41	7.01	5991.37	5990.94	5991.50	5991.40
P-L-15-1	MH-L-15-1	IN-L-16	CIRCULAR	CLASS 7 PIPE	18"	0.010	74.58	1.30%	5989.51	5988.51	5.98	0.94	0.94	15.55	8.23	5990.46	5989.85	5990.86	5990.05
P-L-16	IN-L-16	IN-L-17-1	CIRCULAR	CLASS 7 PIPE	18"	0.010	60.54	1.65%	5988.31	5987.31	7.14	1.0	1.04	17.55	9.42	5989.35	5988.02	5989.82	5989.20
P-L-17-1	IN-L-17-1	IN-L-17-3	CIRCULAR	CLASS 7 PIPE	24"	0.010	93.51	2.03%	5986.80	5984.90	8.15	1.0	1.02	41.92	10.34	5987.82	5986.21	5988.22	5986.42
P-L-17-2	IN-L-17-2	IN-L-17-3	CIRCULAR	RCP	18"	0.013	13.76	2.18%	5985.51	5985.21	0.34	0.2	0.91	15.51	3.57	5986.42	5986.42	5986.42	5986.42
P-L-17-3	IN-L-17-3	MH-L-18	CIRCULAR	CLASS 7 PIPE	24"	0.010	90.41	1.99%	5984.71	5982.91	8.99	1.1	1.07	41.49	10.55	5985.78	5983.57	5986.21	5985.12
P-L-18	MH-L-18	MH-L-19	CIRCULAR	RCP	30"	0.013	156.09	1.41%	5982.41	5980.21	9.53	1.03	1.03	48.69	7.70	5983.44	5981.98	5983.83	5982.08
P-L-19	MH-L-19	IN-L-20-3	CIRCULAR	CLASS 7 PIPE	30"	0.010	69.26	0.72%	5980.01	5979.51	14.86	1.30	1.30	45.30	8.27	5981.31	5981.08	5981.83	5981.35
P-L-20	IN-L-20	MH-L-19	CIRCULAR	RCP	24"	0.013	22.42	1.34%	5980.71	5980.41	8.64	1.05	1.05	26.17	7.47	5981.76	5981.90	5982.18	5982.08
P-L-20-1	IN-L-20-1	IN-L-20	CIRCULAR	RCP	24"	0.013	41.3	0.73%	5981.21	5980.91	6.76	0.92	0.92	19.28	5.60	5982.13	5982.24	5982.49	5982.39
P-L-20-2	IN-L-20-2	IN-L-20-1	CIRCULAR	RCP	24"	0.013	36.85	0.81%	5981.71	5981.41	6.18	0.88	0.88	20.41	5.69	5982.59	5982.44	5982.93	5982.67
P-L-20-3	IN-L-20-3	IN-L-21-1	CIRCULAR	CLASS 7 PIPE	30"	0.010	84.35	0.59%	5979.31	5978.81	14.83	1.30	1.30	41.05	7.69	5980.61	5979.88	5981.13	5980.74
P-L-21-1S	IN-L-21-1	EX-IN-L-21-5	CIRCULAR	CLASS 7 PIPE	30"	0.010	56.61	0.53%	5978.51	5978.21	17.60	0.99	0.99	77.63	6.40	5979.50	5979.61	5979.87	5979.76
P-L-21-2	IN-L-21-2	IN-L-21-1		CLASS 7 PIPE	18"	0.010	42.8	1.40%	5980.11	5979.51	3.41	0.70	0.70	16.17	7.25	5980.82	5980.00	5981.09	5980.72
P-L-23	IN-L-23	IN-L-21-2 IN-L-23	CIRCULAR	CLASS 7 PIPE CLASS 7 PIPE	18"	0.010	110.64 128.45	<u>1.72%</u> 1.87%	5982.21	5980.31 5982.41	3.00	0.66	0.66	17.89	7.52 7.16	5982.87 5985.38	5981.01 5983.13	5983.12 5985.59	5981.23 5983.25
P-L-24-1	IN-L-24-1				18"	0.010		-	5984.81		-		0.57	18.66	-				
P-L-24-2	FES-L-24-2U	IN-L-24-1		CLASS 7 PIPE	18"	0.010	18.74	2.00%	5985.39	5985.01	1.48	0.46		19.31	6.46	5985.84	5985.69	5986.01	5985.74
P-L-42	IN-L-42	IN-L-15	CIRCULAR	CLASS 7 PIPE	18"	0.010	36.37	4.40%	5992.81	5991.21	0.45	0.3	0.25	28.64	5.99	5993.06	5991.51	5993.15	5991.56
P-L-45	IN-L-45	IN-L-102 IN-L-20-2	CIRCULAR	CLASS 7 PIPE RCP	18" 18"	0.010	19.91 73.38	5.02% 8.72%	5988.51 5988.61	5987.51 5982.21	0.83	0.34	0.34	30.61 31.02	7.52 13.05	5988.85 5989.49	5987.69 5982.63	5988.97 5989.86	5988.46 5985.28
P-L-48-1 P-L-52	EX-IN-L-48-1 HW-L-52U	FES-L-52D	CIRCULAR	CLASS 7 PIPE	18	0.013	68.42	2.19%	5988.61	5982.21		0.88	0.88	20.22	6.11	5989.49	5982.63	5989.86	5985.28
		-						-			1.10			-	.				
P-L-102	IN-L-102	MH-L-18	CIRCULAR	CLASS 7 PIPE	18"	0.010	50.83	5.90%	5986.51	5983.51	1.00	0.37	0.37	33.17	8.40	5986.88	5983.93	5987.02	5984.02





B.3A STORM SEWER HYDRAULIC CALCULATIONS (10-YEAR STORM)

 PROJECT:
 I-25 Mobility Hub (Lone Tree)

 DESIGNED BY:
 NAG

 DATE:
 6/11/2024

DESIGN FREQUENCY - 10 YEAR - SYSTEM NB Lanes INV INV CRITICAL ACTUAL UPSTREAM DOWNSTREAM LENGTH Q CAPACITY VEL SHAPE MATERIAL DIAMETER N VALUE PIPE ID SLOPE UPSTREAM DOWNSTREAM DEPTH DEPTH NODE NODE (FT) (CFS) (CFS) (F (FT) (FT) (FT) (FT) CIRCULAR EX-P-L-75 EX-IN-L-75 MH-L-76-1 RCP 24" 0.013 161.1 0.90% 5994.71 5993.29 11.17 1.20 1.20 20.94 EX-IN-L-78 CIRCULAR EX-P-L-76-1 MH-L-76-1 RCP 0.013 128.63 0.90% 5993.24 5992.11 24" 11.89 1.24 1.24 20.86 EX-P-L-78 EX-IN-L-78 MH-L-79-1 CIRCULAR RCP 24" 0.013 170.4 1.60% 5991.91 5989.18 11.81 1.23 1.23 28.27 EX-P-L-79-1 MH-L-79-1 EX-IN-L-80 CIRCULAR RCP 24" 0.013 117.05 1.50% 5989.09 5987.21 12.05 1.25 1.25 28.11 EX-P-L-80 EX-IN-L-80 EX-FES-L-80D CIRCULAR RCP 24" 5981.11 0.013 346.04 12.31 1.26 29.48 1.70% 5987.01 1.26 EX-P-L-84-1 CC-L-84-1 EX-FES-L-84-1D CIRCULAR RCP 24" 0.013 5982.01 5981.06 2.02 0.49 0.49 22.40 96.88 1.00% P-L-76 IN-L-76 MH-L-76-1 CIRCULAR RCP 18" 0.013 9.92 3.30% 5993.91 5993.51 1.57 0.47 1.35 18.98 P-L-79 IN-L-79 MH-L-79-1 CIRCULAR CLASS 7 PIPE 18" 0.01 13.49 2.70% 5990.01 5989.61 0.59 0.28 1.12 22.27 15.44 P-L-80 IN-L-80 EX-IN-L-80 CIRCULAR RCP 18" 0.013 5987.21 0.61 25.38 2.20% 5987.81 0.29 1.27 CLASS 7 PIPE P-L-83-1 IN-L-83-1 IN-L-83-2 CIRCULAR 18" 0.01 24.62 1.40% 5986.11 5985.71 0.79 0.33 0.33 16.43 CLASS 7 PIPE P-L-83-2 IN-L-83-2 IN-L-84-1 CIRCULAR 18" 0.01 91.88 3.30% 5985.51 5982.31 1.62 0.48 0.48 24.79 P-L-84-1 IN-L-84-1 CC-L-84-1 CIRCULAR RCP 24" 0.013 5982.11 5982.01 23.93 9.54 1.10% 2.02 0.49 0.49 P-L-84-2 IN-L-84-2 IN-L-84-1 CIRCULAR RCP 18" 0.013 50.36 0.50% 5982.41 5982.11 0.86 0.35 0.44 7.76 CIRCULAR RCP P-L-85 IN-L-85 IN-L-84-2 18" 0.013 63.08 1.50% 5983.41 5982.41 0.59 0.29 0.29 12.76 P-L-87 IN-L-87 FES-L-87D CIRCULAR CLASS 7 PIPE 18" 0.01 162.22 0.80% 5980.81 5979.48 0.69 0.31 12.40 0.31

PR CHE

ROJECT #:	24278
ECKED BY:	MED



LOCITY	HGL UPSTREAM	HGL DOWNSTREAM	EGL UPSTREAM	EGL DOWNSTREAM
T/SEC)	(FT)	(FT)	(FT)	(FT)
6.77	5995.91	5995.04	5996.41	5995.27
6.86	5994.48	5993.56	5995.01	5993.93
8.59	5993.15	5990.85	5993.67	5991.13
8.60	5990.33	5988.75	5990.87	5989.08
8.96	5988.27	5982.01	5988.81	5983.26
4.42	5982.50	5981.47	5982.68	5981.77
6.50	5995.26	5995.26	5995.27	5995.27
5.41	5991.13	5991.13	5991.13	5991.13
4.24	5989.08	5989.08	5989.08	5989.08
4.79	5986.44	5986.22	5986.56	5986.25
7.93	5985.99	5982.57	5986.16	5983.55
4.64	5982.60	5982.43	5982.78	5982.71
2.89	5982.85	5982.85	5982.91	5982.87
3.68	5983.70	5982.92	5983.80	5982.94
3.78	5981.12	5979.72	5981.23	5979.94

B.3B STRUCTURE HYDRAULIC CALCULATIONS (10-YEAR STORM)

PROJECT:	I-25 Mobility Hub (Lone Tree)			
DESIGNED BY:	CAK	PROJECT #:	24278	DCcL
DATE:	12/15/2023	CHECKED BY:	MED	RSCH

	DESIGN FREQ	UENCY - 10 YEAR - SYS	STEM SB Lanes	
STRUCTURE ID	Q (CFS)	RIM/ GRATE ELEVATION (FT)	HGL (FT)	EGL (FT)
EX-IN-L-21-5	19.9	5983.24	5979.36	5979.76
EX-IN-L-48-1	5.2	5991.19	5989.68	5990.04
EX-IN-L-48-2	3.4	5990.44	5990.04	5990.12
EX-IN-L-48-3	2.3	5990.39	5990.11	5990.14
IN-L-12	4.4	5996.37	5992.33	5992.65
IN-L-14	5.4	5995.48	5991.60	5991.97
IN-L-15	0.9	5995.26	5991.43	5991.56
IN-L-16	7.1	5993.10	5989.58	5990.05
IN-L-17-1	8.2	5991.98	5988.02	5988.42
IN-L-17-2	0.3	5988.91	5986.42	5986.42
IN-L-17-3	9.0	5990.10	5986.00	5986.43
IN-L-20	8.6	5985.36	5981.97	5982.39
IN-L-20-1	6.8	5985.29	5982.31	5982.67
IN-L-20-2	6.2	5985.30	5982.76	5983.09
IN-L-20-3	14.8	5985.76	5980.73	5981.24
IN-L-21-1	17.6	5986.09	5979.69	5980.05
IN-L-21-2	3.4	5985.77	5980.95	5981.22
IN-L-23	3.0	5987.66	5983.00	5983.25
IN-L-24-1	2.3	5991.37	5985.51	5985.72
IN-L-42	0.5	6001.67	5993.10	5993.19
IN-L-45	0.8	5995.56	5988.91	5989.03
IN-L-102	1.0	5996.28	5986.88	5987.02
MH-L-15-1	6.0	5994.47	5990.66	5991.06
MH-L-18	9.5	5988.27	5983.64	5984.02
MH-L-19	14.9	5986.07	5981.57	5982.09

B.3B STRUCTURE HYDRAULIC CALCULATIONS (10-YEAR STORM)

PROJECT:	I-25 Mobility Hub (Lone Tree)			
DESIGNED BY:	NAG	PROJECT #:	24278	DCcL
DATE:	6/11/2024	CHECKED BY:	MED	KSCH

	DESIGN FREQ	UENCY - 10 YEAR - SYS	TEM NB Lanes	
STRUCTURE ID	Q (CFS)	RIM/ GRATE ELEVATION (FT)	HGL (FT)	EGL (FT)
EX-IN-L-75	11.2	5999.16	5996.16	5996.66
EX-IN-L-78	11.8	5996.75	5993.41	5993.93
EX-IN-L-80	12.3	5993.13	5988.54	5989.08
IN-L-76	1.6	5997.72	5995.27	5995.28
IN-L-79	0.6	5994.48	5991.13	5991.13
IN-L-80	0.6	5991.81	5989.08	5989.09
IN-L-83-1	0.8	5990.59	5986.50	5986.62
IN-L-83-2	1.6	5989.93	5986.08	5986.25
IN-L-84-1	2.0	5988.14	5982.69	5982.87
IN-L-84-2	0.9	5985.21	5982.88	5982.94
IN-L-85	0.6	5987.89	5983.75	5983.85
IN-L-87	0.7	5984.96	5981.18	5981.28
MH-L-76-1	11.9	5997.92	5994.74	5995.27
MH-L-79-1	12.1	5995.01	5990.60	5991.13

B.3A STORM SEWER HYDRAULIC CALCULATIONS (100-YEAR STORM)

PROJECT: DESIGNED BY: DATE: I-25 Mobility Hub (Lone Tree) NAG 12/15/2023

DESIGN FREQUENCY - 100 YEAR - SYSTEM SB Lanes

							DESIGNT			SYSTEM SB Lanes]
	UPSTREAM	DOWNSTREAM					LENGTH		INV	INV	Q	CRITICAL	ACTUAL	CAPACITY	VELOCITY	HGL	HGL	EGL	EGL
PIPE ID	NODE	NODE	SHAPE	MATERIAL	DIAMETER	N VALUE	(FT)	SLOPE	UPSTREAM	DOWNSTREAM	(CFS)	DEPTH	DEPTH	(CFS)	(FT/SEC)	UPSTREAM	DOWNSTREAM	UPSTREAM	DOWNSTREAM
	_	_					. ,		(FT)	(FT)	、 <i>,</i>	(FT)	(FT)		(- <i>)</i>	(FT)	(FT)	(FT)	(FT)
EX-P-L-21S	EX-IN-L-21-5	EX-FES-L-21S	CIRCULAR	CLASS 7 PIPE	30"	0.013	185.16	1.17%	5978.11	5975.92	42.82	1.57	1.57	88.86	8.97	5979.69	5977.15	5980.36	5978.40
EX-P-L-48-2	EX-IN-L-48-2	EX-IN-L-48-1	CIRCULAR	CLASS 7 PIPE	18"	0.013	36.07	0.67%	5988.87	5988.62	5.90	0.94	1.73	8.59	3.34	5990.60	5990.48	5990.78	5990.66
EX-P-L-48-3	EX-IN-L-48-3	EX-IN-L-48-2	CIRCULAR	CLASS 7 PIPE	18"	0.013	1.39	0.29%	5988.89	5988.88	4.04	0.77	1.55	5.61	2.29	5990.44	5990.44	5990.52	5990.52
P-L-12	IN-L-12	IN-L-14	CIRCULAR	CLASS 7 PIPE	18"	0.010	181.65	0.35%	5991.36	5990.71	12.15	1.32	4.12	8.12	6.87	5995.49	5994.03	5996.22	5994.76
P-L-14	IN-L-14	MH-L-15-1	CIRCULAR	CLASS 7 PIPE	18"	0.010	71.27	1.06%	5990.51	5989.71	13.80	1.4	2.83	14.08	7.81	5993.34	5992.57	5994.29	5993.52
P-L-15	IN-L-15	MH-L-15-1	CIRCULAR	CLASS 7 PIPE	24"	0.010	4.06	3.74%	5991.01	5990.71	2.09	0.6	2.49	26.41	1.18	5993.50	5993.50	5993.52	5993.52
P-L-15-1	MH-L-15-1	IN-L-16	CIRCULAR	RCP	18"	0.010	75.89	1.30%	5989.51	5988.51	15.07	1.4	2.31	15.55	8.53	5991.83	5990.89	5992.96	5992.02
P-L-16	IN-L-16	IN-L-17-1	CIRCULAR	CLASS 7 PIPE	24"	0.010	60.54	1.65%	5988.31	5987.31	17.20	1.4	1.44	17.55	11.32	5989.75	5988.58	5991.26	5990.39
P-L-17-1	IN-L-17-1	IN-L-17-3	CIRCULAR	RCP	30"	0.010	93.55	2.03%	5986.80	5984.90	19.08	1.57	1.57	41.92	13.03	5988.37	5987.12	5989.18	5987.70
P-L-17-2	IN-L-17-2	IN-L-17-3	CIRCULAR	CLASS 7 PIPE	30"	0.013	12.9	2.18%	5985.51	5985.21	0.89	0.35	2.18	15.51	0.50	5987.69	5987.69	5987.70	5987.70
P-L-17-3	IN-L-17-3	MH-L-18	CIRCULAR	RCP	24"	0.010	89.07	1.99%	5984.71	5982.91	20.94	1.64	1.64	41.49	13.23	5986.35	5984.00	5987.25	5986.22
P-L-18	MH-L-18	MH-L-19	CIRCULAR	RCP	24"	0.013	156.09	1.41%	5982.41	5980.21	21.84	1.59	1.59	48.69	9.65	5984.00	5983.08	5984.69	5983.39
P-L-19	MH-L-19	IN-L-20-3	CIRCULAR	RCP	24"	0.010	66.78	0.72%	5980.01	5979.51	31.83	1.92	2.35	45.30	10.00	5982.36	5982.16	5983.05	5982.81
P-L-20	IN-L-20	MH-L-19	CIRCULAR	CLASS 7 PIPE	30"	0.013	23.44	1.34%	5980.71	5980.41	15.94	1.44	2.39	26.17	5.07	5983.10	5982.99	5983.50	5983.39
P-L-20-1	IN-L-20-1	IN-L-20	CIRCULAR	CLASS 7 PIPE	30"	0.013	41.27	0.73%	5981.21	5980.91	12.11	1.25	2.38	19.28	3.86	5983.59	5983.47	5983.82	5983.70
P-L-20-2	IN-L-20-2	IN-L-20-1	CIRCULAR	CLASS 7 PIPE	18"	0.013	36.92	0.81%	5981.71	5981.41	11.09	1.19	2.12	20.41	3.53	5983.83	5983.75	5984.03	5983.94
P-L-20-3	IN-L-20-3	IN-L-21-1	CIRCULAR	CLASS 7 PIPE	18"	0.010	74.33	0.59%	5979.31	5978.81	32.09	1.93	1.93	41.05	9.25	5981.24	5980.51	5982.21	5981.78
P-L-21-1S	IN-L-21-1	EX-IN-L-21-5	CIRCULAR	CLASS 7 PIPE	18"	0.010	55.3	0.53%	5978.51	5978.21	38.73	1.49	1.89	77.63	7.90	5980.40	5980.42	5980.77	5980.69
P-L-21-2	IN-L-21-2	IN-L-21-1	CIRCULAR	CLASS 7 PIPE	18"	0.010	35.29	1.40%	5980.11	5979.51	8.58	1.13	1.13	16.17	9.28	5981.25	5980.36	5981.80	5981.44
P-L-23	IN-L-23	IN-L-21-2	CIRCULAR	CLASS 7 PIPE	18"	0.010	100.68	1.72%	5982.21	5980.31	7.80	1.1	1.08	17.89	9.78	5983.29	5981.77	5983.80	5982.08
P-L-24-1	IN-L-24-1	IN-L-23	CIRCULAR	CLASS 7 PIPE	18"	0.010	130.95	1.87%	5984.81	5982.41	6.66	1.00	1.00	18.66	9.68	5985.81	5983.82	5986.25	5984.05
P-L-24-2	FES-L-24-2U	IN-L-24-1	CIRCULAR	RCP	18"	0.010	15.07	2.00%	5985.39	5985.01	5.41	0.90	1.33	19.31	9.38	5986.72	5986.71	5986.88	5986.86
P-L-42	IN-L-42	IN-L-15	CIRCULAR	CLASS 7 PIPE	18"	0.010	34.24	4.40%	5992.81	5991.21	0.89	0.35	0.71	28.64	7.31	5993.52	5993.53	5993.54	5993.53
P-L-45	IN-L-45	IN-L-102	CIRCULAR	CLASS 7 PIPE	18"	0.010	19.24	5.02%	5988.51	5987.51	1.39	0.44	0.44	30.61	8.77	5988.95	5987.75	5989.11	5988.68
P-L-48-1	EX-IN-L-48-1	IN-L-20-2	CIRCULAR	RCP	18"	0.013	67.79	8.72%	5988.61	5982.21	9.05	1.16	1.16	31.02	15.22	5989.78	5983.72	5990.36	5984.13
P-L-52	HW-L-52U	FES-L-52D	CIRCULAR	CLASS 7 PIPE	18"	0.010	68.42	2.19%	5987.61	5986.11	3.86	0.75	0.75	20.22	8.82	5988.36	5987.15	5988.66	5987.28
P-L-102	IN-L-102	MH-L-18	CIRCULAR	CLASS 7 PIPE	18"	0.010	50.83	5.90%	5986.51	5983.51	1.65	0.48	0.48	33.17	9.76	5986.99	5985.01	5987.17	5985.03

PROJECT #: 24278 CHECKED BY: MED



B.3A STORM SEWER HYDRAULIC CALCULATIONS (100-YEAR STORM)

PROJECT: I-25 Mobility Hub (Lone Tree) DESIGNED BY: NAG DATE: 6/11/2023

DESIGN FREQUENCY - 100 YEAR - SYSTEM SB Lanes INV INV CRITICAL ACTUAL UPSTREAM DOWNSTREAM LENGTH Q CAPACITY VEL PIPE ID SHAPE MATERIAL DIAMETER N VALUE SLOPE UPSTREAM DOWNSTREAM DEPTH DEPTH NODE NODE (FT) (CFS) (CFS) (F (FT) (FT) (FT) (FT) MH-L-76-1 CIRCULAR EX-P-L-75 EX-IN-L-75 RCP 24" 0.013 161.1 0.90% 5994.71 5993.29 22.33 1.69 3.39 20.94 EX-IN-L-78 CIRCULAR EX-P-L-76-1 MH-L-76-1 RCP 0.013 128.63 0.90% 5993.24 5992.11 24" 23.56 1.72 2.72 20.86 EX-P-L-78 EX-IN-L-78 MH-L-79-1 CIRCULAR RCP 24" 0.013 170.4 1.60% 5991.91 5989.18 23.40 1.72 2.19 28.27 EX-P-L-79-1 MH-L-79-1 EX-IN-L-80 CIRCULAR RCP 24" 0.013 117.05 1.50% 5989.09 5987.21 27.04 1.81 2.28 28.11 EX-P-L-80 EX-IN-L-80 EX-FES-L-80D CIRCULAR RCP 24" 5981.11 0.013 346.04 27.46 1.82 1.82 29.48 1.70% 5987.01 EX-P-L-84-1 CC-L-84-1 EX-FES-L-84-1D CIRCULAR RCP 24" 0.013 96.88 5982.01 5981.06 5.05 0.79 0.79 22.40 1.00% P-L-76 IN-L-76 MH-L-76-1 CIRCULAR RCP 18" 0.013 9.92 3.30% 5993.91 5993.51 2.72 0.6 3.33 18.98 P-L-79 IN-L-79 MH-L-79-1 CIRCULAR CLASS 7 PIPE 18" 0.01 13.49 2.70% 5990.01 5989.61 6.84 1.0 2.89 22.27 15.44 P-L-80 IN-L-80 EX-IN-L-80 CIRCULAR RCP 18" 0.013 5987.21 0.38 25.38 2.20% 5987.81 1.05 2.97 CLASS 7 PIPE P-L-83-1 IN-L-83-1 IN-L-83-2 CIRCULAR 18" 0.01 24.62 1.40% 5986.11 5985.71 1.37 0.44 0.44 16.43 CLASS 7 PIPE P-L-83-2 IN-L-83-2 IN-L-84-1 CIRCULAR 18" 0.01 91.88 3.30% 5985.51 5982.31 2.81 0.64 0.64 24.79 P-L-84-1 IN-L-84-1 CC-L-84-1 CIRCULAR RCP 24" 0.013 5982.11 5982.01 0.79 23.93 9.54 1.10% 5.05 0.79 P-L-84-2 IN-L-84-2 IN-L-84-1 CIRCULAR RCP 18" 0.013 50.36 0.50% 5982.41 5982.11 2.87 0.64 0.89 7.76 CIRCULAR RCP P-L-85 IN-L-85 IN-L-84-2 18" 0.013 63.08 1.50% 5983.41 5982.41 1.02 0.38 0.38 12.76 P-L-87 IN-L-87 FES-L-87D CIRCULAR CLASS 7 PIPE 18" 0.01 162.22 0.80% 5980.81 5979.48 1.28 0.4 0.42 12.40

PR CHE

ROJECT #:	24278
ECKED BY:	MED



LOCITY	HGL	HGL	EGL	EGL
T/SEC)	UPSTREAM	DOWNSTREAM	UPSTREAM	DOWNSTREAM
1/320)	(FT)	(FT)	(FT)	(FT)
7.11	5998.10	5996.49	5998.88	5997.27
7.50	5995.96	5994.52	5996.84	5995.39
7.45	5994.10	5992.23	5994.96	5993.09
8.61	5991.37	5989.63	5992.52	5990.78
10.66	5988.83	5982.64	5990.13	5984.41
5.76	5982.80	5981.71	5983.10	5982.22
1.54	5997.24	5997.24	5997.28	5997.27
3.87	5992.90	5992.86	5993.13	5993.09
0.59	5990.78	5990.78	5990.79	5990.78
5.63	5986.55	5986.47	5986.71	5986.51
9.30	5986.15	5983.26	5986.39	5983.35
6.04	5982.90	5982.69	5983.20	5983.14
4.06	5983.30	5983.29	5983.41	5983.35
4.33	5983.79	5983.45	5983.92	5983.46
4.53	5981.24	5979.80	5981.39	5980.12

B.3B STRUCTURE HYDRAULIC CALCULATIONS (100-YEAR STORM)

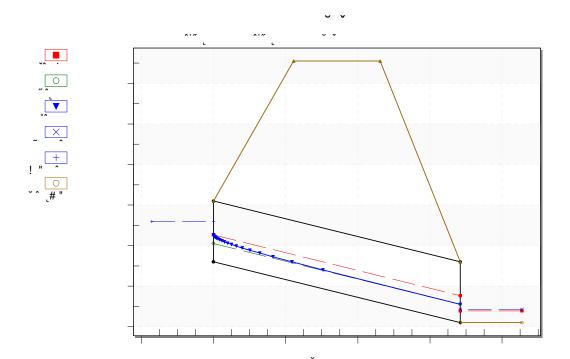
PROJECT:	I-25 Mobility Hub (Lone Tree)			
DESIGNED BY:	CAK	PROJECT #:	24278	DCcL
DATE:	12/15/2023	CHECKED BY:	MED	RSCH

	DESIGN FREQU	JENCY - 100 YEAR - SYS	TEM SB Lanes	
STRUCTURE ID	Q (CFS)	RIM/ GRATE ELEVATION (FT)	HGL (FT)	EGL (FT)
EX-IN-L-21-5	42.8	5983.24	5980.02	5980.69
EX-IN-L-48-1	9.1	5991.19	5990.07	5990.66
EX-IN-L-48-2	5.9	5990.44	5990.52	5990.70
EX-IN-L-48-3	4.0	5990.39	5990.44	5990.52
IN-L-12	12.2	5996.37	5995.85	5,996.59
IN-L-14	13.8	5995.48	5993.82	5994.76
IN-L-15	2.1	5995.26	5993.51	5993.53
IN-L-16	17.2	5993.10	5990.51	5,992.02
IN-L-17-1	19.1	5991.98	5988.77	5989.58
IN-L-17-2	0.9	5988.91	5987.69	5987.70
IN-L-17-3	20.9	5990.10	5986.80	5987.70
IN-L-20	15.9	5985.36	5983.30	5983.70
IN-L-20-1	12.1	5985.29	5983.71	5983.94
IN-L-20-2	11.1	5985.30	5983.93	5984.12
IN-L-20-3	32.1	5985.76	5981.58	5982.55
IN-L-21-1	38.7	5986.09	5980.59	5980.95
IN-L-21-2	8.6	5985.77	5981.52	5982.08
IN-L-23	7.8	5987.66	5983.55	5984.05
IN-L-24-1	6.7	5991.37	5986.36	5986.80
IN-L-42	0.9	6001.67	5993.53	5993.55
IN-L-45	1.4	5995.56	5989.03	5989.19
IN-L-102	1.7	5996.28	5986.99	5987.17
MH-L-15-1	15.1	5994.47	5992.39	5993.52
MH-L-18	21.8	5988.27	5984.34	5985.03
MH-L-19	31.8	5986.07	5982.70	5983.39

B.3B STRUCTURE HYDRAULIC CALCULATIONS (100-YEAR STORM)

PROJECT:	I-25 Mobility Hub (Lone Tree)			The second second second second
DESIGNED BY:	NAG	PROJECT #:	24278	DCcL
DATE:	6/11/2023	CHECKED BY:	MED	RSCH

	DESIGN FREQU	JENCY - 100 YEAR - SYS	TEM SB Lanes	
STRUCTURE ID	Q (CFS)	RIM/ GRATE ELEVATION (FT)	HGL (FT)	EGL (FT)
EX-IN-L-75	22.3	5999.16	5998.49	5999.28
EX-IN-L-78	23.4	5996.75	5994.53	5995.39
EX-IN-L-80	27.5	5993.13	5989.48	5990.78
IN-L-76	2.7	5997.72	5997.26	5997.30
IN-L-79	6.8	5994.48	5993.02	5993.25
IN-L-80	1.1	5991.81	5990.78	5990.79
IN-L-83-1	1.4	5990.59	5986.63	5986.79
IN-L-83-2	2.8	5989.93	5986.27	5986.51
IN-L-84-1	5.1	5988.14	5983.05	5983.35
IN-L-84-2	2.9	5985.21	5983.36	5983.46
IN-L-85	1.0	5987.89	5983.86	5983.99
IN-L-87	1.3	5984.96	5981.31	5981.46
MH-L-76-1	23.6	5997.92	5996.40	5997.27
MH-L-79-1	27.0	5995.01	5991.94	5993.09



Parameter	Value		Units		
OISCHARGE DATA					
Discharge Method	Recurrence	-			-
Discharge List	Define			Parameter	V
7 TAILWATER DATA				CULVERT DATA	
Channel Type	Triangular Channel	-		Name	G
Side Slope (H:V)	17.000		_:1	Shape	C
Channel Slope	0.0173	1	ft/ft	2 Material	c
Manning's n (channel)	0.035			Diameter	1
Channel Invert Elevation	5986.100	1	ft	Embedment Depth	0
Rating Curve	View			Manning's n	0
ROADWAY DATA				Culvert Type	s
Roadway Profile Shape	Constant Roadway Elevation	-		Inlet Configuration	N
First Roadway Station	0.000	1	ft	Inlet Depression?	N
Crest Length	24.000	1	ft	SITE DATA	
Crest Elevation	5992.550		ft	Site Data Input Option	C
Roadway Surface	Paved	-		Inlet Station	0
Top Width	24.000		ft	Inlet Elevation	5
				Outlet Station	6
				Outlet Elevation	5
				Number of Barrels	1
				Computed Culvert Slope	0

FES-L-25D	Add Culvert		
	Duplicate Culvert		
	Delete Culvert		
Parameter	Value		Unit
OULVERT DATA			
Name	FES-L-25D		
Shape	Circular	•	
Ø Material	Concrete	•	
Diameter	1.500		ft
② Embedment Depth	0.000		in
Manning's n	0.013		
Oulvert Type	Straight	-	
Inlet Configuration	Mitered to Conform to Slope (Ke=0.7)	-	
Inlet Depression?	No	-	
SITE DATA			
Site Data Input Option	Culvert Invert Data	-	
Inlet Station	0.000		ft
Inlet Elevation	5987.600		ft
Outlet Station	68.400		ft
Outlet Elevation	5986.100		ft
Number of Barrels	1		
Computed Culvert Slope	0.021930		ft/ft

Culvert Summary Table - FES-L-25D

Discharge Names	Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth(ft)	Outlet Control Depth(ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
10 year	0.89	0.89	5988.11	0.51	-1.14	1-52n	0.24	0.35	0.24	0.21	4.79	1.23
50 year	2.27	2.27	5988.44	0.84	-0.86	1-S2n	0.39	0.57	0.39	0.29	6.29	1.55
100 year	3.05	3.05	5988.59	0.99	-0.70	1-52n	0.45	0.66	0.45	0.33	6.85	1.67

APPENDIX B.3 – CHANNEL CALCUATIONS

Worksheet for Bridge Gutter

. ۲۳۳۳ ۵۵ ر	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	
" # <i>"</i>	`!^ ° `\$ °″	
	~%	
'(#)	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	
+, · <i>"</i> - #	₩ * ∀ 1 ^ °	
π ι	:	
, / , / .+	· ~~% °~~~ ~ 0 °	
°1,	ں *** ۲!**	
2 '-,	2	
ı <i>«</i>	u u	
3 2 4° ″	v 0	
- ″		
5″)°″)°+″″	~(~	
, , , , , , , , , , , , , , , , , , ,	u 0 ~~~	
5″/,	~~%	
ι ι	• • • • • • • • • • • • • • • • • • •	
i		

B.2 ROADSIDE DITCH CALCULATIONS (10-YEAR STORM)

PROJECT:Lone Tree Mobility HubDESIGNED BY:NAGDATE:6/11/2024

PROJECT #: 24278 CHECKED BY: MED

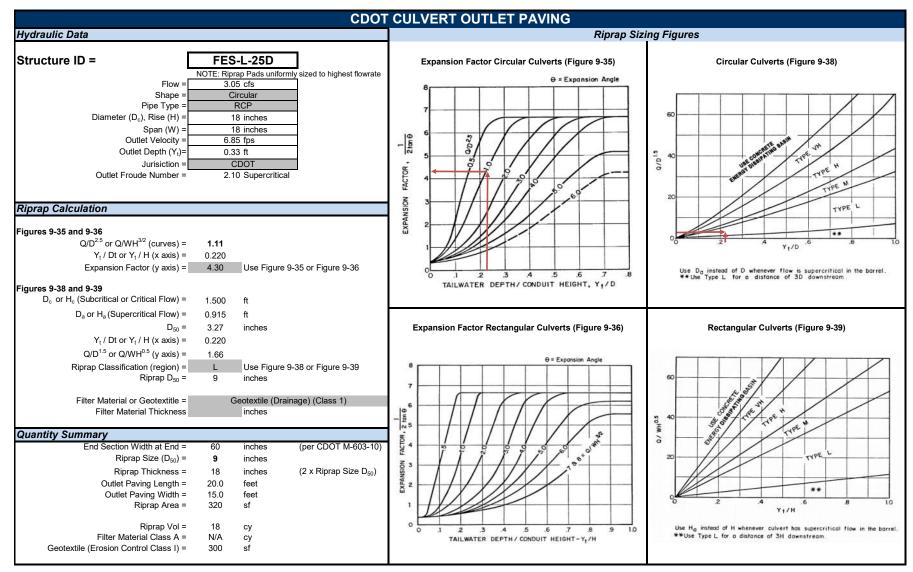
	DESIGN FREQUENCY - 10 YEAR - SYSTEM L																	
DITCH ID	SECTION	BEGIN STATION	OFFSET	BEGIN INV ELEV (FT)	END STATION	OFFSET	END INV ELEV (FT)	ALIGNMENT	B (FT)	Z (LT)	Z (RT)	LONG. SLOPE	N VALUE	Q (CFS)	FLOW DEPTH (FT)	SHEAR STRESS (LB/SF)	MINIMUM LINING	COMMENTS
CH-L-12N-A	Triangular	13+31.47	20.88' LT	5996.58	12+61.09	16.77' LT	5996.35	SB I-25 ON RAMP	0.00	16.67%	33.33%	0.33%	0.064	12.0	1.55	0.319	VEGETATED	
CH-L-12N-B	Triangular	13+78.25	18.97' LT	5997.00	13+31.47	20.88' LT	5996.58	SB I-25 ON RAMP	0.00	16.67%	33.33%	0.90%	0.048	12.0	1.15	0.648	VEGETATED	
CH-L-12S	Triangular	10+80.01	20.00' LT	5997.63	12+61.09	16.77' LT	5996.35	SB I-25 ON RAMP	0.00	40.00%	16.67%	0.71%	0.051	12.1	1.26	0.560	VEGETATED	
CH-L-15	Triangular	13+81.41	18.89' LT	5997.00	15+20.35	18.75' LT	5995.25	SB I-25 ON RAMP	0.00	33.33%	16.67%	1.27%	0.066	0.5	0.37	0.293	VEGETATED	
CH-L-17-2-A	Triangular	16+80.22	24.65' LT	5990.44	17+50.47	32.85' LT	5988.90	SB I-25 ON RAMP	0.00	33.33%	25.00%	2.23%	0.049	1.2	0.46	0.640	VEGETATED	
CH-L-17-2-B	Triangular	15+82.93	20.36' LT	5993.70	16+80.22	24.65' LT	5990.44	SB I-25 ON RAMP	0.00	33.33%	25.00%	3.34%	0.043	1.2	0.41	0.851	VEGETATED	
CH-L-24-2N	Trapezoidal	25+36.65	20.53' LT	5994.24	24+25.35	59.38' LT	5985.65	SB I-25 ON RAMP	2.00	25.00%	33.33%	7.29%	0.040	1.6	0.00	0.000	VEGETATED	
CH-L-24-2S	Trapezoidal	22+69.14	66.53' LT	5986.59	24+25.35	59.38' LT	5985.65	SB I-25 ON RAMP	2.00	33.33%	25.00%	0.61%	0.069	1.6	0.51	0.196	VEGETATED	
CH-L-52N	Triangular	54+78.68	36.77' LT	5990.00	52+51.51	9.94' LT	5987.60	MULTI-USE TRAIL	0.00	33.33%	33.33%	1.12%	0.052	3.1	0.80	0.557	VEGETATED	
CH-L-52S-A	Triangular	52+48.91	16.30' LT	5987.82	52+51.51	9.94' LT	5987.60	MULTI-USE TRAIL	0.00	25.00%	25.00%	3.20%	0.040	3.1	0.53	1.057	VEGETATED	
CH-L-52S-B	Triangular	52+01.69	4.83' LT	5989.00	52+48.91	16.30' LT	5987.82	MULTI-USE TRAIL	0.00	25.00%	25.00%	2.44%	0.043	3.1	0.57	0.873	VEGETATED	
CH-L-82-2E-A	Trapezoidal	83+86.97	58.10' RT	5985.45	84+49.72	29.59' RT	5985.20	NB I-25 OFF RAMP	2.00	33.33%	33.33%	0.56%	0.064	2.8	0.69	0.241	VEGETATED	
CH-L-82-2E-B	Triangular	82+70.71	86.56' RT	5988.65	83+86.97	58.10' RT	5985.45	NB I-25 OFF RAMP	0.00	5.00%	5.00%	2.53%	0.052	2.8	0.32	0.512	VEGETATED	
CH-L-82-2W-A	Triangular	84+09.57	10.92' RT	5983.01	84+49.72	29.59' RT	5981.21	NB I-25 OFF RAMP	0.00	33.33%	33.33%	4.39%	0.041	0.9	0.36	0.997	VEGETATED	
CH-L-82-2W-B	Triangular	83+49.94	13.80' RT	5983.78	84+09.57	10.92' RT	5983.01	NB I-25 OFF RAMP	0.00	33.33%	33.33%	1.33%	0.057	0.9	0.52	0.428	VEGETATED	



APPENDIX B.4 – EROSION CONTROL

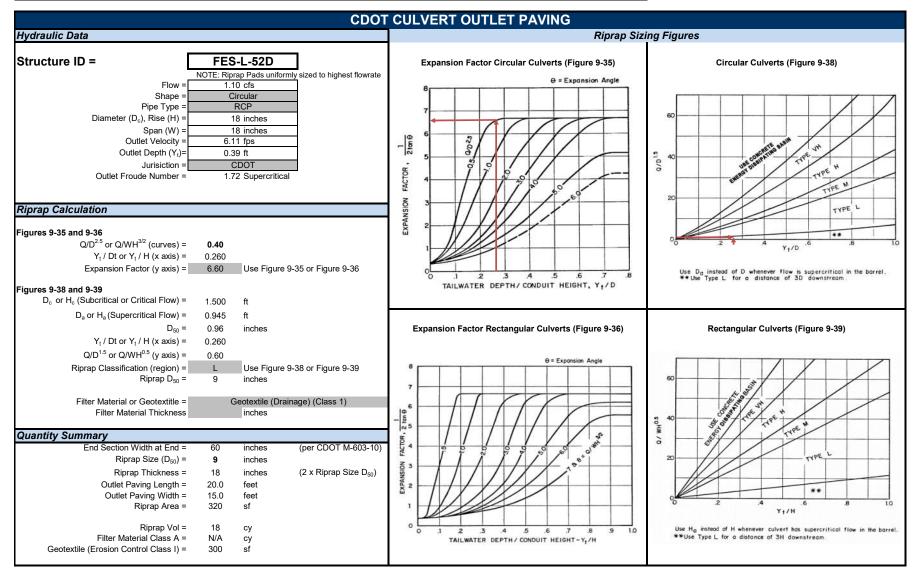
Project Name:	I-25 Mobility Hub (Lone Tree) FOR
Job No.:	24278
Date:	6/11/2024
Designed By:	JMM
Checked by:	MED





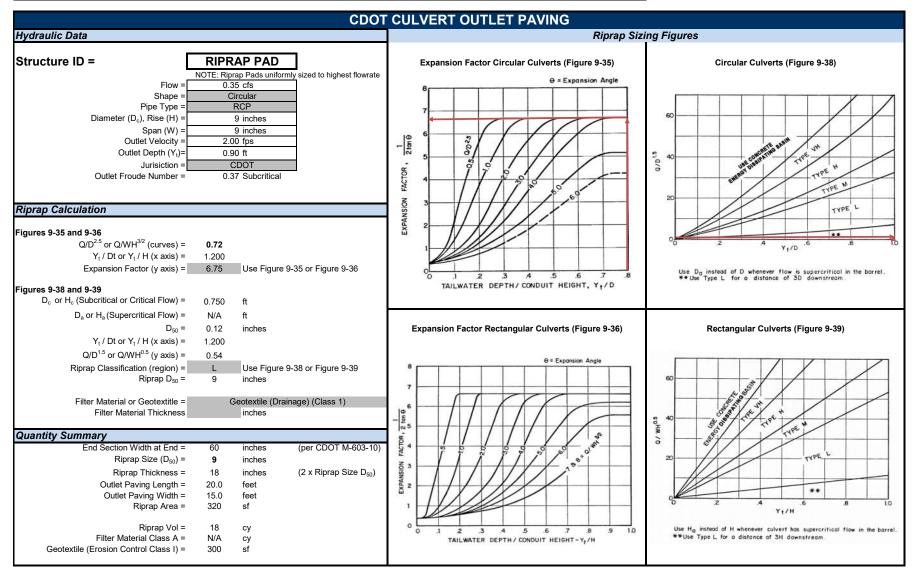
Project Name:	I-25 Mobility Hub (Lone Tree) FOR
Job No.:	24278
Date:	6/11/2024
Designed By:	JMM
Checked by:	MED





Project Name:	I-25 Mobility Hub (Lone Tree) FOR
Job No.:	24278
Date:	6/11/2024
Designed By:	JMM
Checked by:	MED



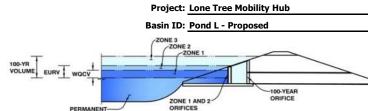


APPENDIX C – WATER QUALITY ENHANCEMENT BMPS

APPENDIX C.1 – DESIGN AND SIZING

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



Depth Increment =	ft

ZONE	1 AND 2	ORIFIC		Depth Increment =		ft		1	1	Ontional	г
PERMANENT ORIFI		on (Retentio	on Pond)	Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	
	oomgalaale		in rona)	Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft ²)	L
Watershed Information		1		Top of Micropool		0.00				227	Ļ
Selected BMP Type =	EDB	-	Note: L / W Ratio > 8	5965		0.50				301	L
Watershed Area =		acres	L / W Ratio = 9.29			1.50				4,083	L
Watershed Length =		ft				2.50				14,138	Ļ
Watershed Length to Centroid =		ft				3.50				31,084	L
Watershed Slope =		ft/ft		5050 0 5		4.50				53,250	┝
Watershed Imperviousness =	71.22%	percent		5970 - Overflow		5.50				76,918	┝
Percentage Hydrologic Soil Group A = Percentage Hydrologic Soil Group B =		percent percent				6.50 7.50				99,884 117,749	┝
Percentage Hydrologic Soil Groups C/D =		percent				8.50				131,701	ŀ
Target WQCV Drain Time =		hours				0.50				151,701	ŀ
Location for 1-hr Rainfall Depths =			t								F
After providing required inputs above inc		·									ľ
depths, click 'Run CUHP' to generate run											Γ
the embedded Colorado Urban Hydro	ograph Procedu	re.	Optional User Overrides								ſ
Water Quality Capture Volume (WQCV) =	0.737	acre-feet	acre-feet								ſ
Excess Urban Runoff Volume (EURV) =	2.183	acre-feet	acre-feet								ſ
2-yr Runoff Volume (P1 = 0.84 in.) =	1.458	acre-feet	inches								
5-yr Runoff Volume (P1 = 1.1 in.) =	2.067	acre-feet	inches								
10-yr Runoff Volume (P1 = 1.33 in.) =	2.650	acre-feet	inches								Ĺ
25-yr Runoff Volume (P1 = 1.68 in.) =	3.661	acre-feet	inches								L
50-yr Runoff Volume (P1 = 1.97 in.) =	4.452	acre-feet	inches								L
100-yr Runoff Volume (P1 = 2.28 in.) =		acre-feet	inches								L
500-yr Runoff Volume (P1 = 3.07 in.) =		acre-feet	inches								L
Approximate 2-yr Detention Volume =		acre-feet									L
Approximate 5-yr Detention Volume =	2.003	acre-feet									┝
Approximate 10-yr Detention Volume =		acre-feet									ŀ
Approximate 25-yr Detention Volume =	2.798	acre-feet									┝
Approximate 50-yr Detention Volume = Approximate 100-yr Detention Volume =		acre-feet acre-feet									┝
	5.552	aciellect									ŀ
Define Zones and Basin Geometry											F
Zone 1 Volume (WQCV) =	0.737	acre-feet									r
Zone 2 Volume (EURV - Zone 1) =		acre-feet									Γ
Zone 3 Volume (100-year - Zones 1 & 2) =	1.149	acre-feet									Γ
Total Detention Basin Volume =	3.332	acre-feet									ſ
Initial Surcharge Volume (ISV) =	user	ft ³									ſ
Initial Surcharge Depth (ISD) =	user	ft									
Total Available Detention Depth $(H_{total}) =$	user	ft									
Depth of Trickle Channel $(H_{TC}) =$	user	ft									L
Slope of Trickle Channel (S_{TC}) =	user	ft/ft									L
Slopes of Main Basin Sides $(S_{main}) =$		H:V									L
Basin Length-to-Width Ratio $(R_{L/W}) =$	user										L
		1									┝
Initial Surcharge Area $(A_{ISV}) =$	-	ft ²									ŀ
Surcharge Volume Length (L_{ISV}) =		ft									┝
Surcharge Volume Width (W_{ISV}) = Depth of Basin Floor (H_{FLOOR}) =	-	ft ft									┝
Length of Basin Floor $(L_{FLOOR}) =$		ft									┝
Width of Basin Floor (W_{FLOOR}) =		ft									ŀ
Area of Basin Floor (A_{FLOOR}) =		ft ²									┝
Volume of Basin Floor (V_{FLOOR}) =		ft ³									F
Depth of Main Basin (V_{HOOR}) =		ft									F
Length of Main Basin (L_{MAIN}) =		ft									ŀ
Width of Main Basin (W_{MAIN}) =		ft									ſ
Area of Main Basin $(A_{MAIN}) =$		ft ²									ľ
Volume of Main Basin (V _{MAIN}) =		ft ³									ſ
Calculated Total Basin Volume (V_{total}) =	user	acre-feet									Γ
		-									ſ

--

--

--

_

Volume

(ft ³)

132

2,324

11,434

34,045

76,212

141,296

229,697

338,514

463,239

Area

(acre) 0.005

0.007

0.094

0.325

0.714

1.222

1.766

2.293

2.703

3.023

Volume (ac-ft)

0.003

0.053

0.262

0.782

1.750

3.244

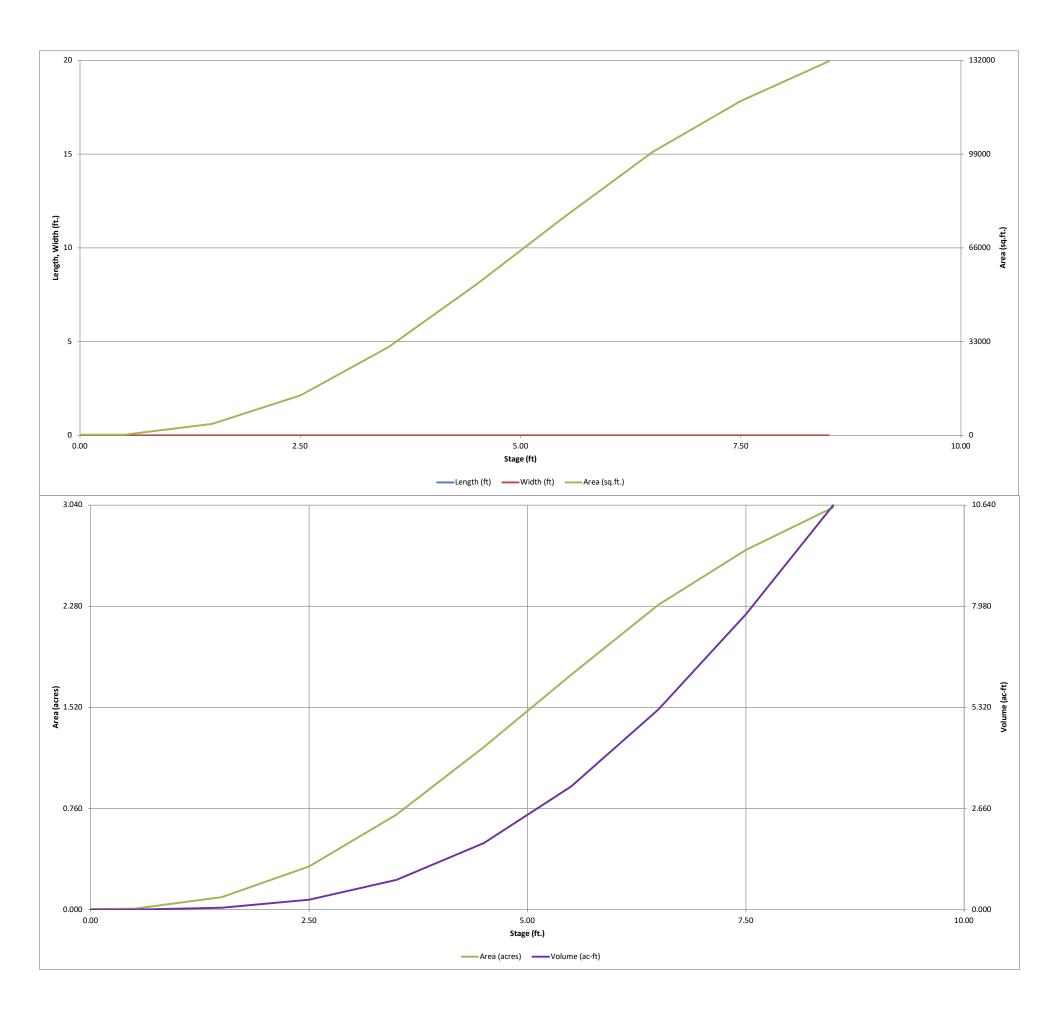
5.273

7.771

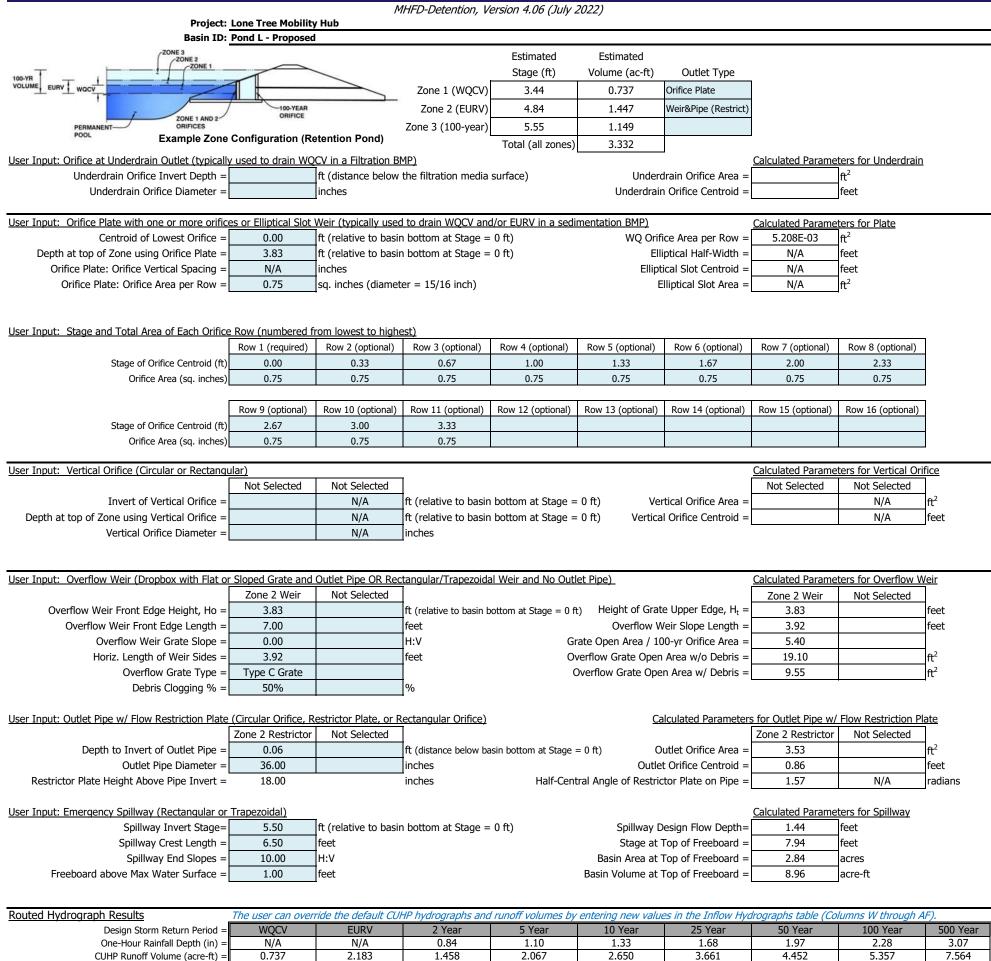
10.634

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

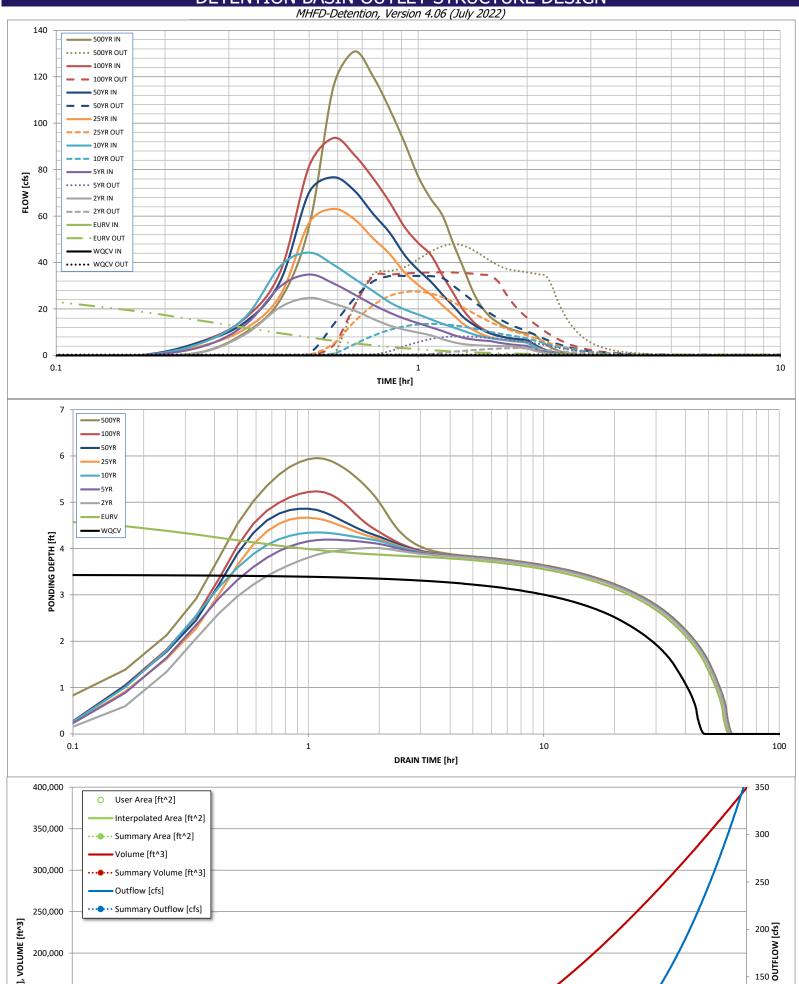
MHFD-Detention, Version 4.06 (July 2022)



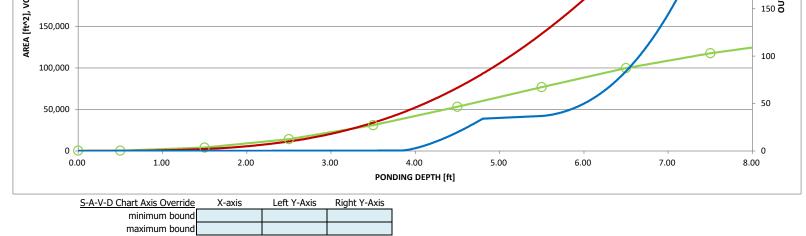
DETENTION BASIN OUTLET STRUCTURE DESIGN



Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.458	2.067	2.650	3.661	4.452	5.357	7.564
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.3	2.9	7.7	19.8	27.1	36.7	57.4
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.09	0.25	0.63	0.86	1.17	1.82
Peak Inflow Q (cfs) =	N/A	N/A	24.8	34.9	44.3	63.1	76.8	93.7	130.9
Peak Outflow Q (cfs) =	0.3	31.6	3.2	8.2	13.6	27.5	34.3	35.8	48.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.8	1.8	1.4	1.3	1.0	0.8
Structure Controlling Flow =	Plate	Outlet Plate 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	1.76	0.14	0.4	0.7	1.4	1.8	1.8	2.0
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	40	48	51	49	48	45	43	41	38
Time to Drain 99% of Inflow Volume (hours) =	43	53	56	55	54	52	52	51	49
Maximum Ponding Depth (ft) =	3.44	4.84	4.01	4.20	4.35	4.67	4.86	5.24	5.96
Area at Maximum Ponding Depth (acres) =	0.69	1.41	0.97	1.06	1.15	1.31	1.42	1.62	2.00
Maximum Volume Stored (acre-ft) =	0.739	2.197	1.212	1.395	1.572	1.952	2.225	2.787	4.092



DETENTION BASIN OUTLET STRUCTURE DESIGN



DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

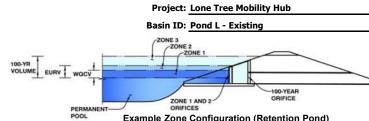
Inflow Hydrographs

								d in a separate pr	-	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.41
	0:15:00	0.00	0.00	1.24	3.58	5.21	3.98	5.73	5.92	9.89
	0:20:00	0.00	0.00	9.20	13.31	16.61	11.59	14.49	16.19	24.10
	0:25:00	0.00	0.00	20.87	29.82	38.58	26.12	32.24	36.32	55.67
	0:30:00	0.00	0.00	24.83	34.87	44.29	57.18	70.30	81.55	115.86
	0:35:00	0.00	0.00	22.35	31.03	39.05	63.10	76.78	93.66	130.91
	0:40:00	0.00	0.00	19.34	26.26	33.00	58.66	70.99	86.35	120.26
	0:45:00	0.00	0.00	15.75	21.88	27.80	50.46	61.04	76.41	106.26
	0:50:00	0.00	0.00	12.93	18.45	22.93	43.85	52.99	66.05	91.70
	0:55:00	0.00	0.00	11.12	15.83	19.85	35.75	43.24	55.35	77.03
	1:00:00	0.00	0.00	9.85	13.90	17.64	30.35	36.78	48.46	67.48
	1:10:00	0.00	0.00	8.68	12.16	15.58	26.25	31.84	43.32	60.31
	1:15:00	0.00	0.00	7.07 5.73	10.56 8.84	13.67 12.12	21.57 17.45	26.21 21.24	34.48 26.84	48.18 37.68
	1:20:00	0.00	0.00	4.92	7.58	10.61	13.53	16.45	19.51	27.49
	1:25:00	0.00	0.00	4.50	6.88	9.14	11.05	13.43	19.51	20.73
	1:30:00	0.00	0.00	4.26	6.46	8.13	9.11	11.04	11.67	16.55
	1:35:00	0.00	0.00	4.15	6.18	7.43	7.85	9.48	9.83	13.96
	1:40:00	0.00	0.00	4.06	5.53	6.94	7.00	8.42	8.55	12.14
	1:45:00	0.00	0.00	4.00	5.02	6.61	6.46	7.74	7.70	10.95
	1:50:00	0.00	0.00	3.95	4.65	6.37	6.08	7.26	7.09	10.09
	1:55:00	0.00	0.00	3.42	4.38	6.02	5.83	6.95	6.71	9.55
	2:00:00	0.00	0.00	2.98	4.06	5.42	5.68	6.76	6.56	9.32
	2:05:00	0.00	0.00	2.17	2.95	3.91	4.14	4.92	4.79	6.79
	2:10:00	0.00	0.00	1.52	2.06	2.72	2.89	3.42	3.36	4.76
	2:15:00	0.00	0.00	1.05	1.42	1.90	2.01	2.38	2.35	3.34
	2:20:00	0.00	0.00	0.72	0.96	1.29	1.38	1.63	1.61	2.28
	2:25:00	0.00	0.00	0.47	0.62	0.86	0.91	1.08	1.07	1.51
	2:30:00	0.00	0.00	0.30	0.42	0.57	0.62	0.73	0.72	1.02
	2:35:00 2:40:00	0.00	0.00	0.17	0.26	0.34	0.38	0.45	0.45	0.63
	2:40:00	0.00	0.00	0.08	0.13	0.17	0.20	0.24	0.24	0.33
	2:50:00	0.00	0.00	0.03	0.05	0.06	0.08	0.09	0.09	0.13
	2:55:00	0.00	0.00	0.00	0.01	0.00	0.00	0.01	0.00	0.02
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00 4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00 4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.06 (July 2022)



Example Zone Configuration (Retention Pond)

Watershed Information		
Selected BMP Type =	EDB	Note: L / W Ratio
Watershed Area =	29.92	acres L / W Ratio = 12.2
Watershed Length =	4,000	ft
Watershed Length to Centroid =	1,400	ft
Watershed Slope =	0.028	ft/ft
Watershed Imperviousness =	68.38%	percent
Percentage Hydrologic Soil Group A =	0.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	100.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	Lone Tree - M	unicipal Court

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

	5	
Water Quality Capture Volume (WQCV) =	0.668	acre-feet
Excess Urban Runoff Volume (EURV) =	1.985	acre-feet
2-yr Runoff Volume (P1 = 0.84 in.) =	1.338	acre-feet
5-yr Runoff Volume (P1 = 1.1 in.) =	1.908	acre-feet
10-yr Runoff Volume (P1 = 1.33 in.) =	2.462	acre-feet
25-yr Runoff Volume (P1 = 1.68 in.) =	3.434	acre-feet
50-yr Runoff Volume (P1 = 1.97 in.) =	4.190	acre-feet
100-yr Runoff Volume (P1 = 2.28 in.) =	5.063	acre-feet
500-yr Runoff Volume (P1 = 3.07 in.) =	7.179	acre-feet
Approximate 2-yr Detention Volume =	1.250	acre-feet
Approximate 5-yr Detention Volume =	1.831	acre-feet
Approximate 10-yr Detention Volume =	2.173	acre-feet
Approximate 25-yr Detention Volume =	2.557	acre-feet
Approximate 50-yr Detention Volume =	2.740	acre-feet
Approximate 100-yr Detention Volume =	3.068	acre-feet

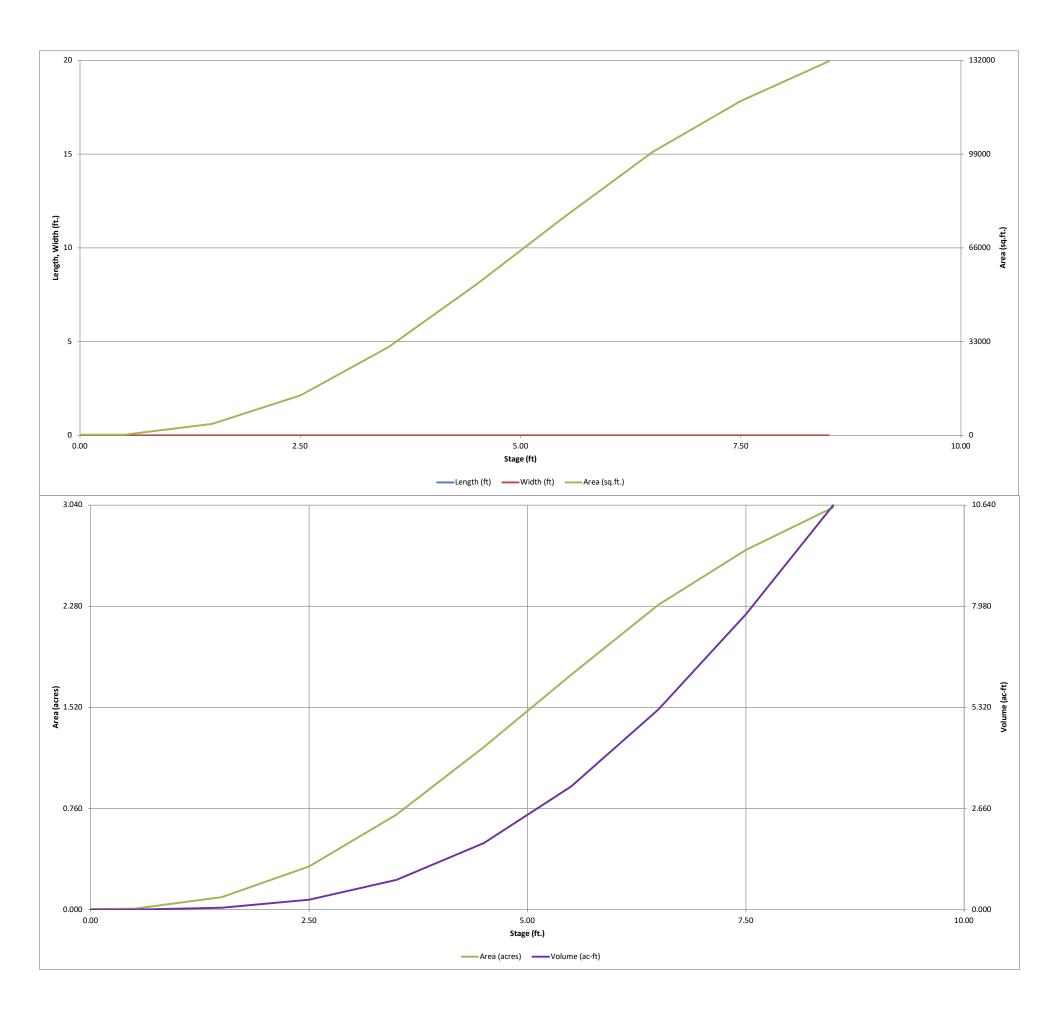
Define Zones and Basin Geometry

ine zones and basin Geometry		
Zone 1 Volume (WQCV) =	0.668	acre-feet
Zone 2 Volume (EURV - Zone 1) =	1.317	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	1.084	acre-feet
Total Detention Basin Volume =	3.068	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel $(H_{TC}) =$	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S_{main}) =	user	H:V
Basin Length-to-Width Ratio ($R_{L/W}$) =	user	
Initial Surcharge Area $(A_{ISV}) =$	user	ft ²
Surcharge Volume Length (L_{ISV}) =	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor (L_{FLOOR}) =	user	ft
Width of Basin Floor (W_{FLOOR}) =	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft ²
Volume of Basin Floor (V_{FLOOR}) =	user	ft ³
Depth of Main Basin (H_{MAIN}) =	user	ft
Length of Main Basin (L_{MAIN}) =	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A_{MAIN}) =	user	ft ²
Volume of Main Basin (V_{MAIN}) =	user	ft ³
Calculated Total Basin Volume (V_{total}) =	user	acre-feet
		•

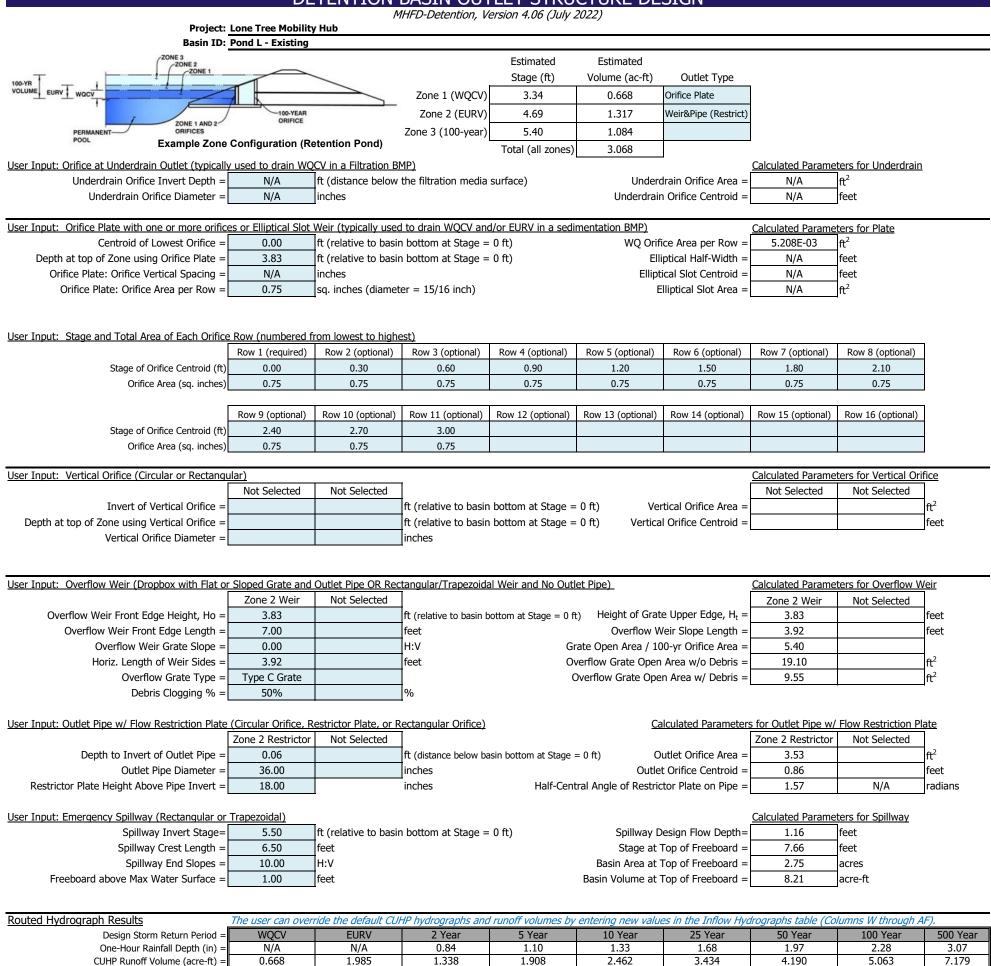
AR E	Denth Increment =		ft							
on Pond)	Depth Increment = Stage - Storage Description	Stage (ft)	Optional Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	Optional Override Area (ft ²)	Area (acre)	Volume (ft ³)	Volume (ac-ft)
	Top of Micropool		0.00				227	0.005		
Note: L / W Ratio > 8	5965		0.50				301	0.007	132	0.003
L / W Ratio = 12.28			1.50				4,083	0.094	2,324	0.053
			2.50				14,138	0.325	11,434	0.262
			3.50				31,084	0.714	34,045	0.782
			4.50				53,250	1.222	76,212	1.750
	5970 - Overflow		5.50				76,918	1.766	141,296	3.244
			6.50				99,884	2.293	229,697	5.273
			7.50				117,749	2.703	338,514	7.771
			8.50				131,701	3.023	463,239	10.634
t										
Optional User Overrides										
acre-feet										
acre-feet										
inches										
inches										
inches										
inches										
inches										
inches								<u> </u>		
inches										
								<u> </u>		
										<u> </u>
									L	
									-	
								<u> </u>		
									+	
									L	
									[
									1	ł

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

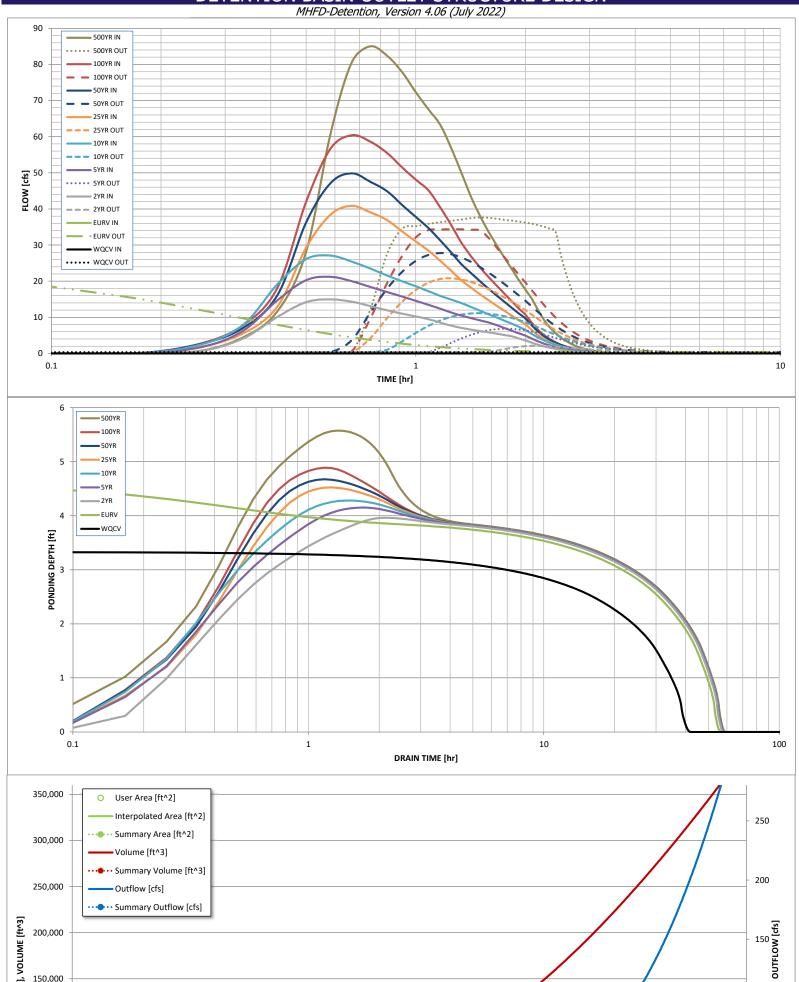
MHFD-Detention, Version 4.06 (July 2022)



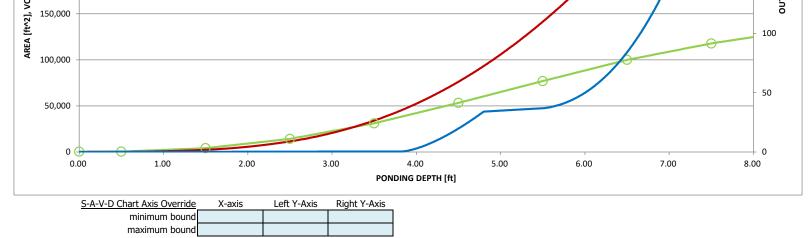
DETENTION BASIN OUTLET STRUCTURE DESIGN



Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	1.338	1.908	2.462	3.434	4.190	5.063	7.179
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.2	1.6	4.4	11.9	16.4	22.6	35.6
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0.05	0.15	0.40	0.55	0.76	1.19
Peak Inflow Q (cfs) =	N/A	N/A	15.0	21.2	27.1	40.9	49.9	60.4	85.0
Peak Outflow Q (cfs) =	0.4	25.1	2.1	6.9	11.2	20.8	27.8	34.4	37.6
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	4.2	2.5	1.7	1.7	1.5	1.1
Structure Controlling Flow =	Plate	Overflow Weir 1	Outlet Plate 1	Spillway					
Max Velocity through Grate 1 (fps) =	N/A	1.47	0.09	0.3	0.6	1.1	1.4	1.8	1.9
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	34	44	48	46	45	43	41	39	36
Time to Drain 99% of Inflow Volume (hours) =	37	49	52	51	50	49	48	47	46
Maximum Ponding Depth (ft) =	3.34	4.69	3.96	4.15	4.28	4.52	4.68	4.89	5.58
Area at Maximum Ponding Depth (acres) =	0.65	1.33	0.95	1.04	1.11	1.23	1.31	1.43	1.80
Maximum Volume Stored (acre-ft) =	0.672	1.992	1.164	1.353	1.493	1.774	1.965	2.253	3.369



DETENTION BASIN OUTLET STRUCTURE DESIGN



DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

	The user can o	verride the calcu	lated inflow hyd	lrographs from t	his workbook w	ith inflow hydrog	graphs develope	d in a separate pr	rogram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.58
	0:15:00	0.00	0.00	0.51	1.48	2.16	1.65	2.38	2.46	4.32
	0:20:00	0.00	0.00	3.99	6.06	7.68	5.42	6.89	7.63	11.64
	0:25:00	0.00	0.00	10.13	14.72	19.13	12.94	16.11	18.15	28.16
	0:30:00	0.00	0.00	14.23	20.31	26.13	29.33	36.28	42.00	60.89
	0:35:00	0.00	0.00	14.98	21.21	27.10	38.44	47.17	56.75	80.55
	0:40:00	0.00	0.00	14.35	20.01	25.45	40.87	49.87	60.40	85.04
	0:45:00	0.00	0.00	13.11	18.41	23.54	39.05	47.55	58.66	82.41
	0:50:00	0.00	0.00	11.95	17.02	21.57	36.93	44.93	55.52	77.90
	0:55:00	0.00	0.00	11.03	15.76	19.99	33.78	41.11	51.49	72.29
	1:00:00	0.00	0.00	10.26	14.60	18.60	31.02	37.78	48.12	67.55
	1:05:00	0.00	0.00	9.50	13.46	17.24	28.49	34.72	45.13	63.35
	1:10:00	0.00	0.00	8.55	12.39	15.96	25.67	31.31	40.44	56.84
	1:15:00	0.00	0.00	7.70	11.34	14.91	22.89	27.95	35.53	50.08
	1:20:00	0.00	0.00	7.08	10.49	13.97	20.25	24.74	30.70	43.39
	1:25:00	0.00	0.00	6.63	9.79	12.90	18.25	22.28	26.94	38.10
	1:30:00	0.00	0.00	6.23	9.17	11.84	16.39	19.99	23.83	33.69
	1:35:00	0.00	0.00	5.86	8.59	10.86	14.74	17.94	21.19	29.94
	1:40:00	0.00	0.00	5.49	7.83	9.96	13.21	16.05	18.78	26.52
	1:45:00	0.00	0.00	5.12	7.05	9.10	11.82	14.32	16.56	23.36
	1:50:00	0.00	0.00	4.76	6.29	8.27	10.48	12.65	14.44	20.36
	1:55:00 2:00:00	0.00	0.00	4.18	5.59	7.41	9.21	11.09	12.47	17.58
	2:05:00	0.00	0.00	3.61	4.93	6.51	8.04	9.66	10.70	15.07
	2:10:00	0.00	0.00	2.96	4.08	5.38	6.43 5.03	7.71	8.44	9.23
	2:15:00	0.00	0.00	2.40	3.32 2.70	4.39 3.59	3.96	6.02 4.75	6.51 5.07	7.20
	2:20:00	0.00	0.00	1.90	2.70	2.94	3.16	3.79	3.97	5.65
	2:25:00	0.00	0.00	1.31	1.80	2.40	2.52	3.02	3.10	4.42
	2:30:00	0.00	0.00	1.07	1.46	1.94	2.02	2.41	2.42	3.45
	2:35:00	0.00	0.00	0.86	1.18	1.55	1.60	1.91	1.86	2.66
	2:40:00	0.00	0.00	0.69	0.93	1.23	1.25	1.49	1.43	2.04
	2:45:00	0.00	0.00	0.55	0.73	0.96	0.98	1.16	1.11	1.58
	2:50:00	0.00	0.00	0.44	0.57	0.75	0.77	0.91	0.87	1.24
	2:55:00	0.00	0.00	0.35	0.45	0.59	0.61	0.72	0.70	1.00
	3:00:00	0.00	0.00	0.27	0.35	0.46	0.47	0.56	0.55	0.78
	3:05:00	0.00	0.00	0.20	0.26	0.35	0.36	0.42	0.42	0.59
	3:10:00	0.00	0.00	0.14	0.18	0.25	0.26	0.31	0.31	0.43
	3:15:00	0.00	0.00	0.09	0.12	0.17	0.18	0.21	0.21	0.30
	3:20:00	0.00	0.00	0.05	0.08	0.10	0.11	0.13	0.13	0.18
	3:25:00	0.00	0.00	0.03	0.04	0.05	0.06	0.07	0.07	0.10
	3:30:00	0.00	0.00	0.01	0.02	0.02	0.03	0.03	0.03	0.04
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00 4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00 4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

APPENDIX C.2 – PERMANENT WATER QUALITY FORM

Permanent Water Quality Form

Please complete this form for every transportation and Property Management project in your Region to assess PWQ requirements per CDOT's MS4 permit. Information about number of projects reviewed for PWQ requirements and projects that install PWQ is reported to CDPHE in annual reports. Please email the completed Form and any changes to PWQ Program Manager <u>Rachel.hansgen@state.co.us</u>. Thank you!

Date 6/12/2024

Region _____ Completed by ____Mary Duke

Subaccount # & Project Description <u>24278 - I-25 - Mobility Hub (Lone Tree)</u>

Please circle Y or N for the Primary Criteria

	Primary Criteria	
1. Inside or partially inside CDOT MS4 area	2. Disturb more than 1 acre or disturb less than 1 acre but is part of a larger common plan of	3. Increases impervious surface by 20% or more
	development	
(Y) br N	Y br N	(Y) or N

Is/Does the project:

1. Inside or partially inside CDOT's MS4 area?

Use C-Plan
https://cdot.maps.arcgis.com/apps/webappviewer/index.html?id=129bef3793774ade8
1cfca5ec9baff7d

- 2. Disturb more than 1 acre or disturb less than 1 acre but is part of a larger common plan of development¹?
- 3. Increase impervious surface by 20% or more?

Use formula: New Impervious Surface / Existing Impervious Surface X 100

New <u>1.67 ac</u> Existing <u>3.10 ac</u> Percent Increase <u>54%</u>

If the answer to one or more of questions 1-3 is NO, PWQ is NOT required on the project.

If the answer to ALL questions above is YES, answer the following 3 questions:

¹ Common Plan of Development A "common plan of development or sale" is a contiguous area where multiple separate and distinct construction activities may be taking place at different times on different schedules, but remain related. Consistent with EPA guidance, "contiguous" is interpreted to mean construction activities located in close proximity to each other (within ¼ mile). Construction activities are considered to be "related" if they share the same development plan, builder or contractor, equipment, storage areas, etc. (CDOT MS4 Permit)

Please circle Y or N for the Secondary Criteria

Secondary Criteria				
4. Discharges to a 303(d)	5. Discharges to the Cherry	6. Is part of an EA or EIS		
listed stream for a CDOT	Creek Reservoir drainage			
Roadway Pollutant of	basin			
Concern				
(Y) or N	(Y)or N	(Y) or N		

Is/Does the project:

4. Discharge to a 303(d) listed stream for a CDOT pollutant of concern?

Use CDPHE map and identify 303 (d) list pollutants https://cdphe.maps.arcgis.com/apps/Viewer/index.html?appid=f1541d2f21834642ba1 551c674fd4a79

Use table of CDOT "Roadway pollutants of concern" and check the "Yes only" column if the stream is listed on the 303(d) list:

Roadway pollutant and (form)	Chemical Formula	YES only
Total Suspended Solids	TSS	
Cadmium (total & potentially dissolved)	Cd	
Chromium (total & potentially dissolved)	Cr	
Copper (total & potentially dissolved)	Cu	X
Iron (total & potentially dissolved)	Fe	X
Lead (total & potentially dissolved)	Pb	
Magnesium (total & potentially dissolved)	Mg	
Manganese (total & potentially dissolved)	Mn	
Nickel (total & potentially dissolved)	Ni	
Zinc	Zn	
Total Inorganic Nitrogen	$TKN + NO_2 + NO_3$	
Total Phosphorus	TP	
Chloride	Cl ⁻	
Sodium	Na	
Oil		
Grease		

5. Discharge to the Cherry Creek Reservoir Basin?

Use Environmental Scoping Tool - sign on using your CDOT login: https://dtdinternalapps.dot.state.co.us/environmentalscoping/

Or view Cherry Creek Drainage Basin Map here: https://www.cherrycreekbasin.org/maps

6. Part of an Environmental Assessment or Environmental Impact Statement?

Check with Region NEPA or Environmental staff

<u>If answer to any question 4-6 is YES, PWQ is REQUIRED on the project.</u> Please access the PWQ Program Manual and <u>website</u> for information about next steps or contact PWQ Program Manager <u>Rachel.hansgen@state.co.us</u>.

APPENDIX D – PIPE SELECTION MEMO



DATE:	June 12, 2024
FROM:	Mary Duke, P.E. (RS&H)
TO:	Samer AlHaj, P.E. (CDOT), Jiovanna Toppi, P.E. (CDOT)
CC:	David Woolfall, P.E. (RS&H)
SUBJECT: Pipe Selection Report	

BACKGROUND

This memorandum is to summarize pipe material selected for the project based upon the Colorado Department of Transportation's (CDOT) *CDOT Pipe Material Selection Guide* dated April 30. 2015 for the I-25 Mobility Hub (Sky Ridge @ Lone Tree) Project.

The *CDOT Pipe Material Selection Guide's* purpose is to enable Project Managers (PM) to select the allowable pipe material options based on a myriad of site specifications that are important to the longevity of the material due to exterior influences. By meeting the corrosion and abrasion criteria defined by the guide and installing the pipe per plans and specifications is assumed to have a 50-year service life. There are a few exemptions to the policy, the only one applicable to this project is the utilization of subsurface drains.

DISCUSSION

A Pipe Selection Report was completed regarding the type of pipe material to be utilized in order to allow a contractor to select the most cost-effective materials. CDOT has five primary steps in determining the pipe materials permitted to be utilized:

- 1. Determine Drainage Application
- 2. Determine Abrasion Level
- 3. Determine Corrosion Level
- 4. Pipe Selection, and
- 5. Verify Fill Height.

Based upon the location of the pipe CDOT has defined 3 types of applications: cross drains, side drains, and storm drains. Definitions for each type of pipe applications are found in the CDOT Drainage Design Manual (DDM) in Chapter 9 Appendix C. This project is utilizing side drains and storm drains for the drainage design.

The second step in determining pipe material is the abrasion level the pipe will encounter. Four levels of abrasion are discussed in the memorandum and after consideration an Abrasion Level 2 will best reflect the pipe's bed load and velocities. Abrasion Level 2 applies where low abrasive conditions exist. Low

abrasive conditions exist in areas of minor bed loads of sand and velocities of 5 fps or less. Though minor bed loads are more likely, Abrasion Level 2 was selected due to the propensity of lower velocities. Velocities are based upon a 2-year storm-event.

Determining the corrosion level requires the use of borings. A draft geotechnical report titled *Draft Subsurface Exploration Report for* Lone Tree Mobility Hub – Pedestrian Bridge dated May 2024 written by Geocal. This report includes information about the chloride and sulfate levels within each of the borings. These were compared to the values in Table 1 from the *CDOT Pipe Selection Guide* to determine a CR 1 level.

Using Figure 1 in the CDOT Pipe Selection Guide for cross drains and side drains materials permitted are all materials for class 1. Figure 2, which is used for storm drains, permits RCP, PP, SRPE, or PVC for Class 7. For simplicity, all pipes within the project shall adhere to the more conservative pipe material and shall meet the requirements of Class 7 pipe. Pipe shall have a minimum Class 3 pipe strength.

Depth of pipe will need to be considered to ensure strength of pipe is adequate in locations where the pipe has minimal cover, in these locations, concrete pipe is specified.